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RESEARCH MEMORANDUM

SUMMARY OF SPIN AND RECOVERY CHARACTERISTICS OF 12 MODELS
OF FLYING-WING AND UNCONVENTIONAL-TYPE AIRPLANES

By Ralph W. Stone, Jr. and Burton E. Hultz

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SUMMARY OF SPIN AND RECOVERY CHARACTERISTICS OF 12 MODELS
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SUMMARY

A compilation is presented of free-spinning model results of investigations of the spin and recovery characteristics of 12 flying-wing and unconventional-type designs. The results were obtained from dynamic tests in the Langley 15-foot free-spinning tunnel and in the Langley 20-foot free-spinning tunnel which replaced it. Dimensional data, mass data, and three-view drawings of the free-spinning models which correspond to each of the 12 airplane designs are presented. The model test results presented include the spin and recovery characteristics of each model for various combinations of control deflections and for various loadings and dimensional configurations.

The results of the spin-tunnel investigations indicated that the effects of control setting and control movement on the spin and spin-recovery characteristics of the flying-wing and unconventional-type models were affected by changes in mass distribution in the same manner as for models of conventional configurations. For mass distributed chiefly along the fuselage, aileron-with and elevator-up settings were conducive of the best recovery; whereas elevator-down and aileron-against settings were conducive of the slowest recovery; for mass distributed chiefly along the wings, the converse was true. The influence of mass distribution on the effect of directional controls was dependent not only on the yawing moment produced but also on the accompanying rolling moment if the rolling moment was appreciable. Recovery techniques required were similar to those of conventional configurations except where unconventional-type control surfaces set up unusual moments when moved for recovery. The models generally recovered from inverted spins as readily as from erect spins and it was indicated that wing-tip parachutes are an effective means of terminating spins in an emergency. Although the results were not sufficiently extensive for evaluation in the form of a design criterion for satisfactory recovery, the data presented should help designers of flying-wing and unconventional-type airplanes anticipate probable spin and recovery characteristics.

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INTRODUCTION

The results of investigations of the spin and recovery characteristics of numerous models tested in the Langley 15-foot free-spinning tunnel and the Langley 20-foot free-spinning tunnel during the years 1935 to 1946 have been used to establish empirical criterions for satisfactory spin recovery (references 1 and 2) which are generally applicable to airplanes having mass distributions typical of this time period and which are considered of conventional design (that is, having both horizontal and vertical surfaces at the tail end of the airplane). The results of several designs which may be generally termed unconventional or flying-wing-type configurations were also available and, because of increased interest in unconventional high-speed airplane configurations, it appeared desirable to evaluate these available results to determine criterions for satisfactory spin recovery similar to those evolved for conventional airplanes. Because the flying-wing and unconventional-type designs often utilized unusual and different methods of obtaining directional control, it was not possible to evaluate their spin-recovery characteristics in terms of a vertical-tail design parameter (tail-damping power factor) in the manner used for conventional designs (reference 1). Also, because of rather limited data available for these configurations, an alternate effective parameter could not be developed at this time. Results available for 12 designs of unconventional and flying-wing-type configurations have been summarized, however, and the more important spin and recovery characteristics are presented in this paper.

The effects of mass distribution and center-of-gravity location were determined for many of the models as were the effects of geometric modifications designed in an attempt to improve the spin-recovery characteristics. The investigations included the determination of the effectiveness for spin recovery of several types of controls which are peculiar to flying-wing and unconventional-type airplanes.

The spin and recovery characteristics of each model are presented for the various control configurations, mass distributions, and dimensional configurations tested. Dimensional data, mass data, and a three-view drawing of each of the various free-spinning models are included. The data presented are intended to help designers of unconventional and flying-wing-type airplanes anticipate probable spin and recovery characteristics.

SYMBOLS

b wing span, feet
S wing area, square feet

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\bar{c}	mean aerodynamic chord, inches
c	wing local chord, inches
x/\bar{c}	ratio of distance of center of gravity rearward of leading edge of mean aerodynamic chord to mean aerodynamic chord; positive when center-of-gravity position is rearward of leading edge of \bar{c}
z/\bar{c}	ratio of distance between center of gravity and thrust line or fuselage reference line to length of mean aerodynamic chord; positive when center of gravity is below thrust line
m	mass of airplane, slugs
ρ	air density, slug per cubic foot
μ	airplane relative density ($m/\rho S b$)
I_X, I_Y, I_Z	moments of inertia about X, Y, Z body axes, respectively, slug-feet ²
$\frac{I_X - I_Y}{mb^2}$	inertia yawing-moment parameter
$\frac{I_Y - I_Z}{mb^2}$	inertia rolling-moment parameter
$\frac{I_Z - I_X}{mb^2}$	inertia pitching-moment parameter
α	angle between thrust line or fuselage reference line and vertical, degrees, approximately equal to absolute value of angle of attack at plane of symmetry
ϕ	angle between span axis and horizontal, degrees; on the charts U or D means inboard wing (right wing in a right spin) up or down, respectively, with relation to the horizontal
V	full-scale true rate of descent, feet per second
Ω	full-scale angular velocity about spin axis, revolutions per second

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δ_r	deflection of rudder, degrees
δ_e	deflection of elevator, degrees
δ_a	deflection of ailerons, degrees
U	elevator up
N	elevator neutral
D	elevator down
ΔC_l	rolling-moment coefficient due to control deflection (Rolling moment / $\frac{1}{2}\rho V^2 b S$)
ΔC_n	yawing-moment coefficient due to control deflection (Yawing moment / $\frac{1}{2}\rho V^2 b S$)

MODELS

The dimensional and mass characteristics of the airplanes simulated by the models are presented in tables I and II, respectively. Three-view drawings of the models are presented in figure 1. The models were constructed as described in reference 3. Briefly, each model was constructed primarily of balsa to be dimensionally similar and was ballasted with lead weights to be dynamically similar to the particular airplane it represented at a given test altitude. A remote-control mechanism was installed in the model to actuate the controls for recovery tests. Sufficient moments were exerted on the control surfaces during recovery tests to move the controls rapidly to the desired positions without regard to the actual forces required to move the controls of the airplane. Parachutes used for spin-recovery parachute tests were of the flat circular type, made of silk, and had drag coefficients of approximately 0.7 based on the surface area of the canopy when spread out flat.

The lateral and longitudinal controls for some of the models presented herein are combined in one pair of control surfaces designated as elevons. Longitudinal control is obtained by deflection of the elevons together and lateral control is obtained by differential deflection of the elevons. In this paper, elevon deflections for longitudinal and lateral control will be referred to, generally, as elevator and aileron deflections, respectively.

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Wind Tunnel and Testing Techniques

The model tests were performed in the Langley 15-foot free-spinning tunnel and in the Langley 20-foot free-spinning tunnel which replaced it. The operation of the Langley 15-foot free-spinning tunnel is described in reference 3 and operation of the Langley 20-foot free-spinning tunnel is generally similar. In brief, models are launched with rotation into the vertically rising air stream of the tunnel and the airspeed is varied by the operator until it equals the rate of descent of the model. The model is thus maintained at approximately eye level in the test section. With the model spinning freely, observations of its general behavior are made, and motion-picture records are obtained. Figure 2 shows a typical model spinning in the Langley 20-foot free-spinning tunnel. After observation of the fully developed spin, recoveries are attempted. The turns for recovery are measured from the time the controls are moved to the time the spin rotation ceases.

Spin tests generally are made to determine the spin and recovery characteristics of the model for the normal spinning control configuration (elevator full up, ailerons neutral, and rudder full with the spin) and at various other aileron-elevator combinations including neutral and maximum deflections. The control deflections used were measured perpendicular to the hinge lines. Recoveries are generally attempted by rapid full rudder reversal, although for the investigations presented herein, some recoveries were attempted by other control manipulations which are specifically noted on the charts. For spins which had rates of descent in excess of that which could be readily attained in the tunnel, the rate of descent was recorded as greater than the velocity at the time the model hit the safety net, as >300 . For recovery attempts in which the model struck the safety net before recovery could be effected, because of the wandering or oscillatory nature of the spin or because of an unusually high rate of descent, the number of turns from the time the controls were moved to the time the model struck the safety net was recorded. This number indicates that the model required more turns to recover from the spin than shown, as, for example, >3 . A >3 -turn recovery, however, does not necessarily indicate an improvement over a >7 -turn recovery. The symbol ∞ is used on the charts to indicate that recovery required more than 10 turns. For a condition in which the model recovered without movement of the controls after having been launched in a spinning attitude with the controls set for a spin, the result is recorded on the charts as "no spin."

The recovery characteristics of a model have been considered satisfactory if recovery from the spin at the normal spinning control configuration (rudder full with, elevator full up, and ailerons neutral) requires 2 turns or less and if small deviations from this control configuration do not cause recovery to exceed $2\frac{1}{4}$ turns. Small deviations are considered to be those which allow for a variation in the deflection of any given control

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setting by as much as one-third from its intended position. This criterion for satisfactory spin recovery has been adopted on the basis of full-scale-airplane spin-recovery data and corresponding model test results (reference 4). The full-scale results available in reference 4 were generally for conventional-type airplanes with horizontal tails, but unless actual full-scale spins of unconventional or flying-wing type airplanes subsequently prove otherwise, it is felt that the criterion for satisfactory recovery specified may be generally applicable to all types of airplane designs. Unpublished observation of airplane motions for some of the unconventional and flying-wing-type configurations presented herein have indicated that the model results give qualitative agreement, at least, with the motions obtained on the airplanes.

The spin-recovery parachute tests were performed in the manner described in reference 5. In brief, recoveries were generally attempted by parachute action alone, the rudder being maintained with the spin. The parachutes were opened by use of a remote-control mechanism.

PRECISION

The results of the free-spinning-tunnel tests presented are believed to be the true values given by the model within the following limits:

α , deg	± 1
ϕ , deg	± 1
V, percent	± 5
Ω , percent	± 2
Turns for recovery:	
From motion-picture records	$\pm \frac{1}{4}$
From visual estimate	$\pm \frac{1}{2}$

All recoveries presented herein were obtained from motion-picture records except where otherwise specifically noted on the charts.

The preceding limits may have been exceeded for certain spins in which it was difficult to control the model in the tunnel because of the high rate of descent or because of the wandering or oscillatory nature of the spin. Comparison between model and airplane spin results (reference 4) indicates that spin-tunnel results are not always in complete agreement with airplane results. In general, when the model spun at an angle of attack less than 45° the corresponding airplane spun at a larger angle

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of attack, and when the model spun at an angle of attack greater than 45° , the corresponding airplane spun at a smaller angle of attack. Generally, the spin at the lower angle of attack (either model or airplane) was associated with the higher rate of descent. The airplane generally spun with its inner wing down more than the inner wing of the corresponding model. The comparison made in reference 4 for 60 different designs indicated that approximately 90 percent of the models satisfactorily predicted full-scale recovery characteristics and that the remaining 10 percent of the models were of some value in predicting details of the full-scale results such as proper recovery technique, aileron effects, and the motion in the developed spin. The designs compared in reference 4 were, in general, for conventional airplanes.

The accuracy of measuring the weight and mass distribution of the models is believed to be within the following limits:

Weight, percent	± 1
Center-of-gravity location, percent \bar{c}	± 1
Moments of inertia, percent	± 5

The controls were set with an accuracy of $\pm 1^\circ$.

TEST CONDITIONS

The variations of the mass-distribution parameters for the various loadings investigated for each model are presented in figure 3. Figure 4 shows the variations of the control-surface deflections with stick positions for the models which combined the longitudinal and lateral controls in one control surface. The dimensional modifications tested during the investigations summarized in this paper are presented in figure 5. Figure 6 shows the original rudders tested on models 1 to 4, these rudders are of the drag type and are mounted at the wing tips. The control configurations tested on each specific model for each model configuration are indicated in charts 1 to 14 with the results.

RESULTS AND DISCUSSION

The erect spin and recovery data for the 12 models summarized herein are presented in charts 1 to 12. Inverted spin data and spin-recovery parachute data available for some of the 12 models are presented in

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charts 13 and 14, respectively. The results of tests with dimensional modifications on the various models are listed with their indicated effectiveness in table III and in general are presented in the corresponding charts 1 to 12.

Erect Spins

The spin and recovery characteristics of models 1 to 6 (charts 1 to 6) were found to be in general agreement with references 1 and 6 as regards the influence of the mass distribution on the effectiveness of the controls during the spin and the recovery. When the mass of the models was distributed primarily along the wings, for example, aileron settings against the spin (stick left in a right spin) and down-elevator settings (stick forward) were generally favorable. For these control settings, steeper spins with more rapid recoveries were generally obtained than were obtained for other control settings. These control settings were also conducive of no-spin conditions. For this mass distribution, reversal of rudders which primarily gave a yawing moment only were ineffective; whereas movement of the elevator down appeared to be the most effective method of obtaining recovery. Such control movement for recovery is consistent with that indicated for conventional airplanes for similar loadings. When the mass of the models was distributed primarily along the fuselage, aileron-with settings and elevator-up settings were generally most effective in causing steep spins from which recovery was most easily obtained. For this mass distribution, movement of the rudder against the spin, when the rudder primarily gave a yawing moment only, generally appeared to be the most effective method of obtaining recovery. These results of control effectiveness are also consistent with those indicated for conventional airplanes for similar loadings (references 1 and 6).

Some exceptions to the general effects of control settings and movements on the spin and recovery were obtained, however. When, for example, model 6 had its loading distributed mainly along the wings (chart 6) full-down elevator and full ailerons against the spin sometimes caused a relatively flat spin from which recovery was unsatisfactory. For this model and other similar models, combination of the longitudinal and lateral controls in a single surface caused unusually large deflections of the surfaces when both full elevator and aileron controls were applied. When the elevator was full down and the ailerons were full against the spin, the inboard control surface (that on the right wing in a right spin) had a large downward deflection; whereas the outboard control surface was nearly neutral. It is believed that this large downward deflection of the inboard control caused unusually large pro-spin yawing moments which overcame the possible favorable effect of the rolling moment due to the aileron-against setting. For loadings for which the mass was distributed primarily along the fuselage, control settings of the elevator

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full up and the ailerons full with the spin tended to be similarly detrimental.

Models 1 to 4 (charts 1 to 4) had rudders which did not primarily provide yawing moments only but also provided appreciable rolling moments. The rudders for models 1 to 4 are shown in figure 6. Typical of these rudders are those of models 2 and 3, similar models with different rudders. The rudder of model 2 is a spoiler-like surface which on the airplane protruded downward and forward through the lower surface of the wing; a pitch flap moved upward in conjunction with downward movement of the spoiler surface. On model 3 two split flap-like surfaces, one on the upper surface and one on the lower surface of the wing, were both deflected for rudder movement. For both models, the rudders on the right wing functioned and those on the left wing remained neutral for a right turn. These rudders may generally be termed scoop-type and split-type rudders, respectively.

A comparison of the aerodynamic yawing- and rolling-moment characteristics of the two general types of rudders (measured on the free-flight-tunnel balance, described in reference 7) is shown in figure 7. The results indicate that, for angles of attack above 34° , setting the rudder against the spin (left rudder pedal forward in a right spin) for the scoop-type rudder produced a rolling-moment increment in the same direction as would be obtained by setting the ailerons against the spin (left stick in a right spin); whereas for the split-type rudder, a rolling-moment increment in the same direction as would be obtained by setting the ailerons with the spin was produced. The yawing moments contributed by both types of rudders were approximately the same. The results are consistent with those indicated in reference 6 for conventional designs with loadings with the mass distributed primarily along the wings in that rolling moments caused by aileron-against settings were favorable and rolling moments caused by aileron-with settings were unfavorable to spin recovery. Thus for wing-heavy loadings, the scoop-type rudders when moved against the spin gave favorable rolling moments for spin recovery and the split-type rudders when moved against the spin produced unfavorable rolling moments. Conversely, it was indicated that maintaining the split-type rudders with the spin was favorable for spin recovery; whereas maintaining the scoop-type rudders with the spin was unfavorable. As is further indicated in reference 6, for loadings in which the mass is distributed primarily along the fuselage, aileron-with settings are favorable. It appears probable that, for designs with the loading primarily along the fuselage, scoop-type rudders when set against the spin would have produced unfavorable rolling moments for spin recovery; whereas split-type rudders would have produced favorable rolling moments.

Models 5 and 6 had rudder control surfaces that primarily provided a yawing moment only. Model 5 had dual rudders and model 6 was tested both with single and dual rudders. For models 5 and 6 (charts 5 and 6),

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when the mass distribution was primarily along the fuselage, rudder reversal was generally effective in producing recovery; whereas for model 6, rudder reversal was ineffective in producing recovery when the mass distribution was primarily along the wings. These results are in accord with the results of reference 1 for conventional airplane designs. Thus rudders which primarily provided yawing moment only appear to be similarly effective in producing recovery for airplanes of the flying-wing type as for airplanes of conventional designs, depending primarily on mass distribution. It has been noted for one model (model 6) that single or dual vertical tails appeared equally as effective provided they had equivalent vertical-tail volume (reference 8).

Model 7 had a delta-wing plan form and a loading for which the weight was very heavily distributed along the fuselage. The results of an extensive investigation on model 7 (reference 9) indicate that spins may not be obtained for values of the inertia yawing-moment parameter $(I_x - I_y/mb^2)$ between approximately -450×10^{-4} to -750×10^{-4} and that flat spins will generally be obtained for larger or smaller values of the inertia yawing-moment parameter. Reversal of the rudder was generally ineffective in stopping the spin rotation except when sufficiently large dual vertical tails and rudders were used (reference 9). These large vertical tails are shown in figure 5 and the results are noted in table III. Movement of the ailerons with the spin, however, was generally effective for terminating the spin rotation. This effect is in agreement with the results obtained during an extensive investigation on a swept-wing model having a horizontal tail. This model was tested at fuselage heavy mass distributions (reference 10) beyond the mass range of references 1 and 6. For all loading conditions tested on model 7 after spin rotation had ceased, the model tended to glide at a flat attitude (very high angle of attack) decreasing its angle of attack relatively slowly except when the elevator was full down.

Model 8 had a sweptforward wing and generally tended to spin flat with a wide radius, very slow rotation, and large oscillations in roll, pitch, and yaw (chart 8). Rudder reversal generally stopped the rotation but the model tended to glide at very large angles of attack above the stall and the oscillations continued after the rotation ceased. When the elevator was reversed to full down following rudder reversal, however, the model tended to dive after the spin rotation ceased. Unpublished full-scale results on this design indicated that accurately timed movement of the stick forward during the oscillations was required to regain unstalled flight. The results of an extensive investigation of modifications to this design and a brief comparison with flying-wing types with sweptback wings indicate that major modifications would be needed to improve the characteristics of this design and that in this instance the sweptforward wing appeared to cause the unsatisfactory trim characteristics. Installation of a large horizontal tail and increased

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vertical-tail length made the model's trim and spin characteristics satisfactory. The results with the horizontal tail installed are noted in table III and the modification is shown in figure 5.

Models 9 and 10 were similar designs having approximately circular plan form, dual vertical tails mounted on the upper surface of the wing, and horizontal surfaces with control surfaces extending from the nearly circular plan form for longitudinal and lateral control. The spin and recovery characteristics of model 9 (chart 9) were not appreciably affected by changes in mass distribution for the range of values of inertia yawing-moment parameter tested ($I_X - I_Y/mb^2$ from -208×10^{-4} to 590×10^{-4}). Increasing the relative density for model 9, however, had an adverse effect upon spin recovery. The results for the largest relative density for model 9 and the results for model 10 (chart 10) which were for a similarly large relative density, indicated poor recovery characteristics. Satisfactory spin recoveries were obtained for model 9 by a special technique for which the leading edges of the horizontal surfaces were moved down and the stick was held back and moved against the spin (left in a right spin) while the rudder was reversed. Satisfactory recoveries were obtained on model 10 only with the installation of modifications and following a recovery technique in which the stick was held full back and moved against the spin while the rudder was reversed, a technique similar to that used for model 9. The satisfactory modifications used for model 10 were a supplementary vertical tail (supplementary tail 2, fig. 5(g)) behind the trailing edge, a large semispan spoiler (spoiler no. 4, fig. 5(g)) beneath the outer wing in a spin (left wing in a right spin), or two large vertical fins (vertical fin 7, fig. 5(g)) mounted on the horizontal control surfaces.

Models 11 and 12 were tail-first or canard-type designs. The spinning characteristics of these models (charts 11 and 12) were not affected by small variations in mass distribution or by small movements of the center of gravity. After recovery from the spin, model 11 trimmed at a high angle of attack (approx. 80°) even when the elevator was set to simulate a stick position of full forward. Modifications which caused model 11 to trim in a normal flight attitude after the spinning rotation had been stopped were the addition of large fillets or drooping enlarged ailerons 22° . Prior to spin tests, model 12 was designed so that it would not trim at high angles of attack by installing a large elevator with increased deflections over those of model 11, and by installing large wing-tip trimmers. The configuration for model 12 with these changes is shown in figure 1(1). Satisfactory spin recoveries in which the model recovered in a dive were obtained for model 12 by application of full rudder reversal when the elevator was set to simulate a stick position of full forward.

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Inverted Spins

Inverted spin and recovery characteristics were available for 10 of the 12 models presented herein. These results are presented in chart 13. A brief analysis of the results based on reference 11, a summary of inverted spin results, is presented.

When the ailerons were set with the spin, for the fully developed inverted spins presented, the ailerons were set to simulate a stick position to the pilot's left when spinning to the pilot's right with the rudder to the pilot's right (controls crossed). When the ailerons were set against the inverted spin, the controls were together. Elevator-up simulated stick forward and elevator-down simulated stick back. In chart 13, the angle of wing tilt is given as up or down relative to the ground.

Model 1 would spin inverted only when the ailerons were neutral or with the spin. Recoveries from these spins were generally unsatisfactory. The inverted spin results were generally similar to those for erect spins. This is probably an indication that exposed area which tended to damp the rotation was approximately the same for both erect and inverted spins.

Model 2 would spin inverted only when the ailerons were with the spin with the stick neutral or forward longitudinally. The inverted spin characteristics were considered somewhat improved over the erect spin characteristics in that spins were obtained for fewer control settings (that is, more no-spin conditions were obtained).

Model 4 would generally not spin inverted when the rudders were set with the spin (right rudder pedal forward in an inverted spin to the pilot's right); whereas it did spin erect. Model 4, however, would spin inverted, when the rudders were set against the spin (data not presented).

Model 5 would spin inverted for most control configurations; recovery by rudder reversal was, however, satisfactory. These results are somewhat better than those obtained erect, probably because more vertical fin and rudder area were unshielded in the inverted spin than in the erect spin.

Model 6 would spin inverted only with ailerons and rudder with the spin. Satisfactory recoveries were obtained by neutralizing all of the controls.

Model 7 would spin inverted for a loading condition for which it would not spin erect. The model spun inverted, however, only when the ailerons were against the spin and the stick was neutral or forward longitudinally. The rudder of this model was above the wing and shielded in erect spins, whereas it was relatively unshielded in inverted spins. Thus for this

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design it appears that in an erect attitude the rudder which was shielded did not supply sufficient pro-spin yawing moment to cause the model to rotate; whereas in an inverted attitude the pro-spin yawing moment of the unshielded rudder was apparently sufficient to cause the model to spin. Satisfactory recovery by rapid rudder reversal was obtained and it appears that, on a corresponding airplane, neutralization of the stick laterally and longitudinally also would be desirable.

Model 8 would generally not spin inverted but tended to become erect and, as in the case of erect spins, tended to remain at a flat erect attitude. The vertical fin and rudder of this design, which had a relatively large aspect ratio and was mounted well above the fuselage center line, was unshielded in the inverted attitudes and may have contributed a rolling moment which caused the model to roll erect following launching into the tunnel inverted.

Model 10 had inverted spins which were similar to the erect spins, recoveries from which were unsatisfactory.

Models 11 and 12 would spin inverted generally when the ailerons were neutral or with the spin. Reversal of the rudder caused the spinning rotation to stop quickly for both models. Model 11 remained in an inverted stalled attitude after the rotation had ceased, for all elevator settings. Model 12, however, dived into a normal flight attitude when the elevator was set to cause a nose-down pitching moment from the inverted attitude. These results are similar to those for erect spins.

The results of the inverted spin tests of the various models are in general accord with inverted spin and recovery results for conventional designs as indicated in reference 11, in that rearward movement of the stick, and aileron-against settings generally tended to be beneficial.

Spin-Recovery Parachutes

The results of investigations made to determine the effect of spin-recovery parachutes were available for six of the models. The results (chart 14) indicate that, in general, parachutes attached to the outer wing tip in a spin (left wing in a right spin) will generally cause satisfactory spin recovery by parachute action alone for emergency purposes. The primary disadvantage of wing-tip spin-recovery parachutes is the danger of opening the parachute on the inboard wing tip (right tip in a right spin) rather than the outboard wing tip. Under such circumstances, the spin may be flattened and recovery made impossible. The results of tests for conventional designs (reference 12) and for one model reported herein indicated that use of parachutes on both wing tips when opened simultaneously required parachutes of approximately twice the diameter of a single wing-tip parachute used only on the outer wing tip.

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Opening two parachutes simultaneously has the advantage of eliminating the danger of opening the wrong wing-tip parachute. The experimental results indicated that a towline length equal to approximately the semispan of the wing should be used.

Model 8 was tested only with a parachute attached to the tail cone for which satisfactory recoveries were obtained. On model 10 a single wing-tip parachute, required for satisfactory recovery, was excessively large but satisfactory recoveries were obtained by simultaneously opening moderate sized tail and wing-tip parachutes. The tail parachute was mounted on the arresting gear mast shown in figure 8.

Reference 12 presents a method whereby the size wing-tip parachute required for satisfactory spin recovery may be calculated. As is indicated in reference 12, calculations by this method correlate satisfactorily with experimental data for flying-wing-type configurations.

CONCLUSIONS

Based on the spin and recovery characteristics of models of 12 flying-wing and unconventional-type designs investigated in the Langley 15-foot free-spinning tunnel and the Langley 20-foot free-spinning tunnel, the following conclusions are made.

1. The effect of aileron and elevator control settings on spin and recovery characteristics was generally dependent upon mass distribution in the same manner as for conventional configurations: that is, for mass distributed chiefly along the fuselage, aileron-with and elevator-up settings were conducive of the best recovery, whereas elevator-down and aileron-against settings were conducive of the slowest recovery; for mass distributed chiefly along the wings, the converse was true. The influence of mass distribution on the effect of directional controls was dependent not only on the yawing moment produced but also on the accompanying rolling moment if the rolling moment was appreciable.
2. Recovery from inverted spins generally was obtained as readily as from erect spins. It appears that the most rapid recoveries from inverted spins would have been obtained by movement of the stick back longitudinally and against the spin laterally and of the rudder against the spin.
3. A single wing-tip parachute on the outer wing tip in a spin generally was an effective spin-recovery device for emergency recovery of unconventional and flying-wing-type designs.

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TABLE I.- DIMENSIONAL CHARACTERISTICS OF MODELS TESTED
 [Model values are presented in terms of corresponding airplane values.]

Model	1	2	3	4	5	6	7	8	9	10	11	12
Model scale	1/16	1/20	1/17.33	1/16	1/17.34	1/20	1/20	1/17.8	1/16	1/16	1/16	1/16.99
Over-all length, ft	23.58	17.78	50.90	14.25	36.44	20.45	41.37	29.40	26.64	28.13	27.40	29.58
Wings:												
Span, ft	40.59	60.00	172.00	39.00	38.67	26.83	29.42	54.0	23.33	23.33	36.98	40.57
Area, sq ft	309.32	490.0	4020.0	293.31	496.00	200.00	375.0	356.0	427.5	427.0	191.0	208.3
Aspect ratio	5.33	7.36	7.36	5.19	3.01	3.60	2.31	8.20	1.27	1.27	7.00	7.91
Root chord, in.	148.48	157.00	450.00	141.65	194.00	123.00	305.80	116.40	280.16	280.16	92.00	92.00
Tip chord, in.	24.80	39.00	112.00	35.92	116.00	4.28	0	44.00	---	---	35.50	33.55
Taper ratio	0.167	0.248	0.249	0.253	0.600	0.420	0	0.376	---	---	0.386	0.364
M.A.C., (C), in.	103.04	109.80	315.00	102.33	157.0	93.68	203.89	85.82	238.00	238.00	67.71	67.69
L.E. rearward L.E. root chord	53.28	69.70	200.00	49.30	83.56	62.48	101.91	-30.00	10.5	10.02	57.0	61.08
Twist, deg	3.0	4.0	4.0	0	0	---	0	0	0	0	2.0 to -0.25	3.0 to -0.5
Dihedral, deg	Tip -43.0 Center 8.0	2.0	2.0	1.0	0	0	0	2.0	0	0	4.5	4.5
Sweepback, deg	29.3 LEW	21.9 c/4	25.8 LEW	27.8 LEW	35 c/4	38.1 c/4	60 LEW	-15 c/4	0 c/4	0 c/4	28.5 c/4	28.8 c/4
Airfoil section, root	NACA 66,2-018	NACA 65,3-019	NACA 65,3-019	NACA 66,2-018	CVA 4-(00) -(12)(40) -(1.1)(1.0)	NACA 0010-64 (normal to 40-percent chord line)	NACA 65(06)-006.5	NACA 23018	NACA 0016	NACA 0016	C-W 6500-0015	C-W 6500-0015
Airfoil section, tip	NACA 66,2x-012	NACA 65,3-018	NACA 65,3-018	NACA 66,2-018	CVA 4-(00) -(12)(40) -(1.1)(1.0)	---do---	NACA 65(06)-006.5	NACA 23012	NACA 0016	NACA 0016	C-W 6500-0015	C-W 6500-0015
Horizontal tail:												
Span, percent b/2	None	None	None	None	None	None	None	None	64.90	80.35	44.60	55.20
Area, sq ft	---do---	---do---	---do---	---do---	---do---	---do---	---do---	---do---	46.0	48.0	15.56	21.92
Longitudinal control:												
Type	Elevons	Elevons	Elevons	Elevons	Elevons	Elevons	Elevons	Elevons	Elevons	Elevons	Elevons	Elevons
Area, sq ft	36.06	31.85	273.36	32.67	54.40	16.98	33.30	36.31	25.00	47.99	15.56	18.62
Distance to c.g., ft ^b	5.76	4.55	16.85	5.03	12.76	---	10.53	5.42	10.42	11.45	15.73	16.05
Vertical tail:												
Area, sq ft	31.82	0	0	37.15	122.40	20.10	67.00	43.50	28.30	28.42	25.20	27.80
Rudders:												
Type	Frisee	Drag	Drag	Drag	Conventional	Conventional	Conventional	Conventional	Conventional	Conventional	Conventional	Conventional
Area, sq ft	13.88	14.63	120.00	21.68	32.00	4.10	13.40	19.40	13.20	11.28	11.44	13.00
Dist. to c.g., ft ^b	7.18	7.68	22.05	5.65	15.15	9.33	11.86	12.31	15.00	12.53	5.00	7.92
Lateral control:												
Type	Elevons	Elevons	Elevons	Elevons ^d	Elevons	Elevons	Elevons	Conventional	Elevons	Elevons	Conventional	Conventional
Span, percent b/2	56.66	33.67	40.00	58.30	47.20	45.40	72.15	52.85	64.90	80.35	38.01	39.11
Area, sq ft	36.06	31.85	273.36	32.67	54.40	16.98	33.30	31.60	25.00	47.99	13.20	15.16
Maximum control deflections:												
Right δ_r , deg up ^e	90	^f 26	60	45	25 R	30	30 R	25 R	30 R	25 R	30 R	40 R
Right δ_r , deg down ^e	20	69	60	45	25 L	30	30 L	25 L	30 L	25 L	30 L	11 L
Left δ_r , deg up ^e	90	^f 26	60	45	25 R	30			30 R	25 R		11 R
Left δ_r , deg down ^e	20	69	60	45	25 L	30			30 L	25 L		40 L
δ_a , deg up ^e	30	24	20	^g 10.5, ^h 21	30	20	20	30	15	45	30	60
δ_a , deg down ^e	20	11	10	^g 10.5, ^h 7	20	10	20	20	15	15	15	60
δ_a , deg up ^e	30	17	15	^g 10.5, ^h 10	15	15	15	20	30	10	20	38
δ_a , deg down ^e	15	13	15	^g 10.5, ^h 10	15	15	15	15	30	10	14 1/2	9

^aAll movable elevator.

^bDistances measured rearward to midpoint of control hinge line.

^cArea of both rudders.

^dElevon balancers were used in conjunction with elevon, deflections 120° (14° up and 42° down revised).

^eDeflections measured from chord plane and perpendicular to hinge line.

^fDeflection of pitch flap which moved up in conjunction with downward movement of drag rudder.

^gOriginal deflections.

^hRevised deflections.

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TABLE II.- MASS CHARACTERISTICS OF MODELS TESTED

[Model values are presented in terms of full-scale values]

Loading	Weight (lbs)	Center-of-gravity location		Relative airplane density, μ		Moments of inertia (slug-feet ²)			Mass parameters			Remarks
		x/c	z/c	Sea level	Test altitude	I _X	I _Y	I _Z	$\frac{I_X - I_Y}{mb^2}$	$\frac{I_Y - I_Z}{mb^2}$	$\frac{I_Z - I_X}{mb^2}$	
Model 1												
A	10,194	0.128	-0.003	10.59	12.62	9,313	6,834	15,635	48×10^{-4}	-169×10^{-4}	121×10^{-4}	Loading primarily along wings
B	10,194	.128	-.003	10.59	12.62	7,264	6,834	13,586	8	-129	121	Do.
C	10,194	.128	-.003	10.59	12.62	11,828	6,834	18,150	96	-217	121	Do.
D	10,194	.128	-.003	10.59	12.62	9,313	5,604	14,405	71	-169	98	Do.
E	10,194	.128	-.003	10.59	12.62	9,313	9,226	18,027	2	-169	167	Do.
F	10,194	.188	-.003	10.59	12.62	9,313	6,834	15,635	48	-169	121	Do.
G	10,194	.078	-.003	10.59	12.62	9,313	6,834	15,635	48	-169	121	Do.
H	9,755	.179	-.023	10.14	12.01	8,417	12,417	20,667	-80	-165	245	Loading primarily along fuselage
Model 2												
A	6,526	0.290	-0.040	2.91	4.62	19,138	2,274	21,298	231×10^{-4}	-260×10^{-4}	29×10^{-4}	Loading primarily along wings
B	6,526	.290	-.040	2.91	4.62	22,951	2,274	25,111	283	-312	29	Do.
C	6,526	.290	-.040	2.91	4.62	19,138	1,999	21,023	235	-261	26	Do.
D	6,768	.290	-.040	3.01	4.78	19,132	2,967	21,997	214	-251	37	Do.
E	6,694	.240	-.040	2.98	4.73	19,132	2,679	21,709	221	-254	33	Do.
F	6,675	.320	-.040	2.96	4.71	19,132	2,059	21,089	229	-255	26	Do.
G	6,538	.350	-.040	2.91	4.62	19,132	1,729	20,758	238	-260	22	Do.
H	6,914	.250	-.040	3.08	4.89	19,131	2,919	21,949	210	-246	36	Do.
Model 3												
A	155,000	0.275	-0.014	2.93	5.50	3,380,000	433,500	3,769,000	207×10^{-4}	-234×10^{-4}	27×10^{-4}	Loading primarily along wings
B	155,000	.275	-.014	2.93	5.50	3,380,000	563,550	3,899,050	198	-234	36	Do.
C	155,000	.333	-.014	2.93	5.50	3,380,000	433,500	3,769,000	207	-234	27	Do.
D	155,000	.391	-.014	2.93	5.50	3,380,000	433,500	3,769,000	207	-234	27	Do.
E	155,000	.200	-.014	2.93	5.50	3,380,000	433,500	3,769,000	207	-234	27	Do.
Model 4												
A	4,642	0.251	0.049	5.29	8.42	6,074	1,030	7,102	230×10^{-4}	-280×10^{-4}	50×10^{-4}	Loading primarily along wings
B	4,642	.383	.049	5.29	8.42	6,074	1,030	7,102	230	-280	50	Do.
C	4,642	.184	.049	5.29	8.42	6,074	1,030	7,102	230	-280	50	Do.
D	13,291	.268	.011	15.18	24.14	19,151	1,925	20,902	270	-297	27	Do.
E	9,000	.268	.011	10.29	16.36	9,590	1,520	11,120	189	-226	37	Do.
Model 5												
A	14,517	0.167	0.004	9.89	15.72	13,250	22,943	35,021	-144×10^{-4}	-179×10^{-4}	323×10^{-4}	Loading primarily along fuselage
B	14,485	.240	.003	9.87	15.68	13,338	23,618	35,994	-153	-184	337	Do.
C	14,485	.163	.003	9.87	15.68	13,338	17,449	29,825	-61	-184	245	Do.
Model 6												
A	6,815	0.199	0.035	16.59	23.36	3,910	2,749	6,534	76×10^{-4}	-249×10^{-4}	173×10^{-4}	Loading primarily along wings
B	6,260	.178	.038	15.23	24.21	3,050	2,694	5,616	25	-208	183	Do.
C	5,820	.159	.041	14.18	22.54	2,360	2,640	4,821	-22	-168	190	Loading primarily along fuselage
D	6,815	.199	.035	16.59	23.36	2,381	3,787	6,041	-92	-148	240	Do.

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TABLE II.- MASS CHARACTERISTICS OF MODELS TESTED - Concluded

Loading	Weight (lbs)	Center-of-gravity location		Relative airplane density, μ		Moments of inertia (slug-feet ²)			Mass parameters			Remarks
		x/c	z/c	Sea level	Test altitude	I_x	I_y	I_z	$\frac{I_x - I_y}{mb^2}$	$\frac{I_y - I_z}{mb^2}$	$\frac{I_z - I_x}{mb^2}$	
Model 7												
A	11,648	0.240	0.014	13.80	21.93	3,989	27,619	29,557	-754×10^{-4}	-62×10^{-4}	816×10^{-4}	Loading primarily along fuselage
B	11,598	.241	.002	18.10	28.79	4,713	27,078	30,560	-1192	-186	1378	Do.
Model 8												
A	3,846	0.140	-0.052	2.61	4.13	5,084	4,369	9,365	21×10^{-4}	-144×10^{-4}	123×10^{-4}	Loading primarily along wings
B	3,507	.120	-.035	2.36	3.79	4,789	4,275	9,096	16	-152	136	Do.
C	3,890	.140	-.052	2.65	4.20	4,060	4,369	8,340	-9	-115	124	Loading primarily along fuselage
D	4,004	.140	-.052	2.71	4.30	5,941	4,369	10,222	43	-161	118	Loading primarily along wings
E	3,846	.190	-.052	2.61	4.13	5,084	3,844	8,840	36	-144	108	Do.
F	3,846	.090	-.052	2.61	4.13	5,084	4,864	9,860	6	-144	138	Do.
G	7,886	.140	-.010	5.35	8.51	5,664	4,738	10,204	13	-77	64	Do.
H	7,547	.120	-.023	5.11	8.13	5,384	4,655	9,930	10	-77	67	Do.
I	7,886	.090	-.010	5.35	8.51	5,664	5,738	11,203	-1	-77	78	Do.
Model 9												
A	4,615	0.225	0.006	6.05	8.19	8,090	4,915	12,780	405×10^{-4}	-1006×10^{-4}	601×10^{-4}	Loading primarily along wings
B	5,287	.225	.006	6.92	9.36	10,193	4,915	14,883	590	-1115	525	Do.
C	4,615	.225	.006	6.05	8.19	4,126	5,750	9,651	-208	-500	708	Loading primarily along fuselage
D	4,615	.250	.006	6.05	8.19	4,126	5,750	9,651	-208	-500	708	Do.
E	4,615	.200	.006	6.05	8.19	4,126	5,750	9,651	-208	-500	708	Do.
F	6,283	.225	.006	8.24	11.16	8,053	4,765	12,056	309	-686	377	Loading primarily along wings
G	6,947	.225	.006	9.09	12.30	10,122	4,765	14,243	456	-807	351	Do.
H	7,320	.225	.006	9.58	12.96	8,053	10,578	17,527	-204	-563	767	Loading primarily along fuselage
I	11,890	.218	.017	15.59	21.11	17,178	6,900	23,571	511	-803	281	Loading primarily along wings
Model 10												
A	16,850	0.263	0.005	22.1	35.1	18,296	15,367	33,703	103×10^{-4}	-646×10^{-4}	543×10^{-4}	Loading primarily along wings
Model 11												
A	3,241	0.120	0.182	6.07	8.22	1,409	4,062	5,041	-197×10^{-4}	-72×10^{-4}	269×10^{-4}	Loading primarily along fuselage
B	3,241	.120	.182	6.07	8.22	1,973	4,062	5,605	-155	-114	269	Do.
C	3,241	.120	.182	6.07	8.22	1,409	3,453	4,432	-151	-73	224	Do.
D	3,241	.120	.182	6.07	8.22	1,409	5,687	6,666	-317	-72	389	Do.
E	3,241	.220	.182	6.07	8.22	1,409	4,062	5,041	-197	-72	269	Do.
F	3,241	.070	.182	6.07	8.22	1,409	4,062	5,041	-197	-72	269	Do.
G	3,241	.08	.182	6.07	8.22	1,409	4,062	5,041	-197	-72	269	Do.
H	3,241	.37	.182	6.07	8.22	1,409	4,062	5,041	-197	-72	269	Do.
Model 12												
A	7,717	0.118	-0.019	11.52	15.61	4,120	10,896	14,712	-168×10^{-4}	-95×10^{-4}	263×10^{-4}	Loading primarily along fuselage
B	7,906	.099	-.008	11.80	15.99	6,592	11,916	17,184	-114	-116	230	Do.
C	7,851	.109	-.008	11.72	15.88	5,657	8,717	14,270	-68	-123	191	Do.
D	7,811	.048	-.012	11.66	15.80	5,063	12,672	17,718	-186	-124	310	Do.
E	7,835	.202	-.016	11.79	15.84	4,542	9,860	14,255	-130	-107	237	Do.

^aForward of leading edge of M.A.C.

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TABLE III.- MODIFICATIONS TESTED ON MODELS

Modification	Modification made to				Effect on spin and recovery characteristics	Modification shown in figure	Data presented in chart
	Wing	Wing-tip rudders	Vertical fin	Other part			
Model 1							
A	-----	Split rudder	-----	-----	Detrimental	5(a)	1
Model 2							
A	-----	-----	-----	Equivalent propeller fin area added	Slightly detrimental	5(b)	2
B	20-percent semispan slats	-----	-----	-----	Detrimental	5(b)	2
C	35-percent semispan slats	-----	-----	-----	-----do-----	5(b)	2
D	-----	-----	Horizontal area	-----	Ineffective	5(b)	2
Model 4							
A	40-percent semispan slats	-----	-----	-----	Slightly detrimental	5(c)	4
B	25-percent semispan slats	-----	-----	-----	Ineffective	5(c)	4
C	60-percent semispan slats	-----	-----	-----	Detrimental	5(c)	4
D	25-percent semispan auxiliary airfoil	-----	-----	-----	Slightly detrimental	5(c)	4
E	25-percent semispan slats	-----	Vertical fins removed	-----	Detrimental	5(c)	4
F	25-percent semispan slats	Neutral	Surface made movable aft of 50-percent-chord line	-----	Beneficial	5(c)	4
G	25-percent semispan slats	Neutral	Surface made movable aft of 50-percent-chord line plus area A	-----	Very beneficial	5(c)	4
H	25-percent semispan slats	Neutral; Area B added to trailing edge of wing	Surface made movable aft of 50-percent-chord line	-----	Beneficial	5(c)	4
I	25-percent semispan slats	Area C added, doubling chord of rudders	-----	-----	Somewhat beneficial	5(c)	4
J	25-percent semispan slats	Area C added and hinge line moved to trailing edge of wing	-----	-----	Beneficial	5(c)	4
K	25-percent semispan slats	Area D added and hinge line moved to trailing edge of wing	-----	-----	Very beneficial	5(c)	4
L	Area F added	Neutral	Fins moved outboard, area E added, surface made movable aft of 50-percent-chord line	-----	Beneficial	5(c)	4
M	-----	Neutral	Fins moved outboard; area E added; area G used as rudders	-----	Beneficial	5(c)	Not presented
Model 5							
A	55.4-percent semispan slats	-----	-----	-----	Slightly detrimental	1(e)	5
Model 6							
A	-----	-----	Single vertical tail moved rearward 1.7 inches	-----	Ineffective for loading A, beneficial for loading D	5(d)	6
B	-----	-----	Dual vertical tails added with same tail volume as original single vertical tail	-----	Ineffective for loading A, ineffective for loading D	5(d)	6
C	-----	-----	Dual vertical tails moved rearward 1.0 inch to have same tail volume as mod. A	-----	Ineffective for loading A, beneficial for loading D	5(d)	6
Model 7							
A	Wing fillets added	-----	-----	-----	Detrimental	1(g)	7
B	-----	-----	Dual vertical tails	-----	Ineffective	1(g)	7
C	-----	-----	Large dual vertical tails	-----	Beneficial	5(e)	Not presented

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TABLE III.- MODIFICATIONS TESTED ON MODELS - Concluded

Modification	Modification made to				Effect on spin and recovery characteristics	Modification shown in figure	Data presented in chart
	Wing	Wing-tip rudders	Vertical fin	Other part			
Model 8							
A	Spoilers				Slightly beneficial	5(r)	8
B	Increase dihedral to 8°				Ineffective	-----	8
C			Moved rearward	Large horizontal tail added	Beneficial in improving trim condition	5(r)	Not presented
Model 10							
A			Ventral fin 1		Ineffective	5(g)	Not presented
B			Ventral fin 2		-----do-----	5(g)	Do.
C			Vertical fin 1		-----do-----	5(g)	Do.
D			Vertical fin 2		-----do-----	5(g)	Do.
E			Vertical fin 3		-----do-----	5(g)	Do.
F			Vertical fin 4		-----do-----	5(g)	Do.
G			Vertical fin 5		-----do-----	5(g)	Do.
H			Vertical fin 6		-----do-----	5(g)	Do.
I	Spoiler 1		Vertical fin 2		-----do-----	5(g)	Do.
J	Spoiler 2				-----do-----	5(g)	Do.
K	Spoiler 3				-----do-----	5(g)	Do.
L	Longitudinal fence 1				-----do-----	5(g)	Do.
M	Longitudinal fences 1 and 2				-----do-----	5(g)	Do.
N	Longitudinal fences 1 and 2		Vertical fin 5		-----do-----	5(g)	Do.
O	Elevon spoilers		Vertical fin 5		-----do-----	5(g)	Do.
P	Slotted elevon; slats 1				-----do-----	5(g)	Do.
Q	Slotted elevon; slats 2				-----do-----	5(g)	Do.
R			Vertical fin 7; dorsal fin 1		-----do-----	5(g)	Do.
S			Vertical fin 7; dorsal fin 2		-----do-----	5(g)	Do.
T				Supplementary tail 1	Very slightly beneficial	5(g)	Do.
U	Spoiler 5				-----do-----	5(g)	Do.
V	Spoiler 6				-----do-----	5(g)	Do.
W	Spoiler 7				-----do-----	5(g)	Do.
X	Spoiler 7		Vertical fin 2		-----do-----	5(g)	Do.
Y				Supplementary tail 2	Beneficial	5(g)	Do.
Z	Spoiler 4				-----do-----	5(g)	Do.
A'			Vertical fin 7; rearward portion movable as rudder		-----do-----	5(g)	Do.
Model 11							
A	Ailerons drooped 22°				Ineffective	-----	11
B	Aileron chord and area double; ailerons drooped 22°				Slightly beneficial in improving trim condition	-----	11
C	Fin A				Ineffective	5(h)	11
D	Fin B				Slightly beneficial in improving trim condition	5(h)	11
E	Spoilers				Ineffective	5(h)	11
F		Fins and rudder moved to wing tip			Ineffective	5(h)	11
G				Fin C	Ineffective	5(h)	11
H				Fin D	Ineffective	5(h)	11

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CHART 2.- SPIN DATA OBTAINED WITH MODEL 2

Unless otherwise indicated, steady-spin data are for rudder-with spina of the model in clean condition and recoveries were attempted by rapid full rudder reversal; right erect spin.

Loading A													Loading A rudder controls neutral														
Ailerons	Against						Neutral						With						Against			Neutral			With		
	Full			1/2			1/2			Full			Against			Neutral			With								
Elevators	U (a)	U (b)	N	D	N	D	U (c)	N	D	U (b)	N	D	U (c)	N	D	U	N	D	U	N	D	U (c)	N	D			
α , deg	---	---	N	N	N	N	44,37	34,21	27,20	N	N	N	33,26	38	49,41	39,32	32	N	N	N	N	N	32,22	35,25	---		
β , deg	---	---	s	s	s	s	30,40	20,10	30,20	s	s	s	10,20	20,20	10,20	10,10	20,10	s	s	s	s	s	30,40	30,20	---		
δ , rps	---	0.21	p	p	p	p	0.21	0.37	0.38	p	p	p	0.37	0.31	0.34	0.35	0.39	p	p	p	p	p	0.23	0.40	---		
V , fps	---	213	n	n	n	n	188	220	204	n	n	n	201	176	163	179	188	n	n	n	n	n	213	204	---		
Turns for recovery	$\frac{1}{2}$	$\frac{1}{2}$					$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$						$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$										

Loading A rudder controls against the spin													Loading B													Loading C												
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With													
	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
Elevators	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
α , deg	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N	N														
β , deg	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---														
δ , rps	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s	s														
V , fps	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p	p														
Turns for recovery	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$															

Loading D													Loading E													Loading F												
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With													
	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
Elevators	U <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th>	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
α , deg	44,36	N	N	51,41	43,35	---	23,45	30,38	46,37	38,23	N	N	43,37	N	N	51,40	43,27	N	34	36,27	N	43,22	N	46,40														
β , deg	30,30	N	N	70,30	20,10	---	10,30	30,40	10,20	70,10	N	N	70,10	N	N	40,0	30,10	N	30,20	40,10	N	30,20	N	30,20														
δ , rps	0.20	s	s	0.22	0.28	0.35	0.29	0.32	0.32	0.44	s	s	---	s	s	0.39	0.51	s	0.13	0.15	s	---	s	0.28														
V , fps	191	p	p	176	194	201	160	176	188	213	p	p	---	p	p	185	182	p	185	185	p	---	p	185														
Turns for recovery	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$															

Loading G													Loading H													Loading A - Modification A												
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With													
	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
Elevators	U <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th>	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
α , deg	54,40	52,43	N	55,41	51,40	63,53	53,42	54,40	56,22	N	N	43,33	38,16	N	N	49,41	43,35	40,24	38,33	N	N	49,30	41,23															
β , deg	50,20	50,10	N	30,20	20,10	---	20,10	30,20	30,10	N	N	20,20	30,20	N	N	10,20	20,20	20,20	20,20	N	N	10,20	20,20															
δ , rps	0.19	0.24	s	0.23	0.26	0.26	0.27	0.27	0.33	s	s	0.27	---	s	s	0.35	0.39	0.45	0.18	s	s	0.22	0.33															
V , fps	166	166	p	170	166	150	157	163	209	p	p	197	---	p	p	176	195	195	201	p	p	186	201															
Turns for recovery	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$																

Loading A - Modification B													Loading A - Modification C													Loading A - Modification D												
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With													
	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
Elevators	U <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th> <th>U</th> <th>N</th> <th>D</th>	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D														
α , deg	36	N	N	48,41	34	N	48	55,41	35	38	34	N	44	38	47,37	49,42	48,38	38	46,23	N	N	49,34	38,21															
β , deg	30,10	N	N	10	20,20	---	20,10	30,10	10	30,10	30,10	N	10,30	10,20	30,20	20,20	10,10	20	60,20	N	N	10,20	20,20															
δ , rps	0.33	0.41	s	0.33	0.44	0.44	0.33	---	---	s	s	0.31	0.41	0.44	0.42	0.43	0.45	0.32	---	s	s	0.22	0.43															
V , fps	184	p	p	161	157	p	151	157	163	174	213	p	164	170	170	146	151	154	220	p	p	207	207															
Turns for recovery	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{2}$																

Radius of spin too great to permit testing completely.

Two types of spin.

Oscillatory spin; range of values or average value given.

Visual estimate.

CHART 3.- SPIN DATA OBTAINED WITH MODEL 3

[Unless otherwise indicated, steady-spin data are for rudder-with spins of the model in the clean condition and recoveries were attempted by rapid full rudder reversal, right erect spins]

	Loading A, rudders against spin									Loading A, rudder neutral spins									Loading A											
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With					
Elevators	U (ab)	N	D	U (ab)	N (ac)	D	U (d)	N	D	U	N	D	U	N (g)	D (hd)	U	N	D	U	N	D	U	N	D	U	N (dg)	D			
α , deg	---	---	---	---	---	---	36	26	25	---	---	---	---	---	---	44	32	28	---	---	---	---	---	---	44	---	---			
ϕ , deg	---	N	O	---	---	---	30	30	30	N	O	N	N	---	---	0	0	10	N	O	N	N	O	N	---	20	---	N		
Ω , rps	---	---	---	---	---	---	0.10	0.21	0.21	---	---	---	---	---	---	0.18	0.21	0.24	---	---	---	---	---	---	0.20	---	---			
V, fps	377	---	---	366	---	350	319	350	361	---	---	---	---	---	---	>350	319	350	363	---	---	---	---	---	298	---	---			
Turns for recovery	---	---	---	---	---	---	e ₂	ef ₁	ef ₁ 2	---	---	---	---	---	---	e ₂	ea >8	ef ₁ >8	---	---	---	---	---	---	h ₂	---	---			
Loading A, slots open, rudders against spin									Loading A, slots open						Loading B, rudders against spin						Loading B									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With					
Elevators	U	N	D	U (a)	N	D	U	N (i)	D (i)	U	N	D	U	N (i)	D (i)	U	N	D	U	N (a)	D (i)	U	N	D	U (a)	N (i)	D (i)	U	N (i)	D (i)
α , deg	---	---	---	29	---	---	44	30	26	---	---	---	57	---	---	---	---	---	38	33	25	---	---	---	---	---	41	29	25	
ϕ , deg	N	O	N	110	N	O	40	40	50	N	O	N	N	O	N	N	O	N	50	80	70	N	O	N	---	---	30	10	10	
Ω , rps	---	---	---	0.11	---	---	0.22	0.24	0.23	---	---	---	0.26	---	---	---	---	0.15	0.19	0.13	---	---	---	---	---	0.22	0.15	0.24		
V, fps	---	---	---	377	---	---	318	329	350	---	---	---	377	---	---	---	---	320	350	350	---	---	---	383	---	266	372	378		
Turns for recovery	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	
Loading C rudders against spin									Loading C						Loading D rudders against spin						Loading D									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With					
Elevators	U	N	D	U	N	D	U	N	D	U (j)	N (j)	D (j)	U	N	D	U	N	D	U	N	D	U	N (i)	D	U	N	D	U	N	D
α , deg	---	---	---	---	---	---	47	36	34	---	---	---	53	34	25	---	---	---	56	---	---	---	---	---	71	66	---	74	73	60
ϕ , deg	N	O	N	---	---	---	60	80	70	N	O	N	10	10	10	N	O	N	30	---	---	N	O	N	---	---	10	10	10	
Ω , rps	---	---	---	0.13	0.12	0.15	---	---	---	0.13	0.12	0.18	0.23	0.18	0.15	---	---	---	0.17	---	---	---	---	---	0.21	0.19	0.23	0.21	0.19	
V, fps	---	---	---	298	320	320	---	---	---	288	329	298	253	282	329	---	---	---	255	---	---	---	---	---	234	249	239	234	244	
Turns for recovery	---	---	---	---	---	---	---	---	---	1	2 4	1 2	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	
Loading E rudders against spin									Loading E						Loading A, pitch flap deflected down 15°, rudders against spin						Loading A, pitch flap deflected down 15°									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With					
Elevators	U (g)	N	D	U (g)	N	D	U (g)	N	D	U (g)	N	D	U	N	D	U	N	D	U (d)	N	D	U	N	D	U	N	D	U	N (d)	D
α , deg	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	25	---	---	---	---	---	---	---	---	---	---
ϕ , deg	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	40	---	---	---	---	---	---	---	---	---	---
Ω , rps	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	0.26	---	---	---	---	---	---	---	---	---	---
V, fps	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	360	---	---	---	---	---	---	---	---	---	---
Turns for recovery	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---

*Large radius oscillatory spin, average values given.

^bWandering spin.

^cSteep wandering spin.

^dOscillatory in pitch.

^eRecovery attempted by moving rudder to full with the spin.

^fVisual observation.

^gSteep spin.

^hRecovery attempted by moving rudder to full against the spin.

ⁱOscillatory spin.

^jOccasionally oscillated out of spin.

UNCLASSIFIED

CHART 3.- SPIN DATA OBTAINED WITH MODEL 3-CONCLUDED


	Loading A, landing condition, rudders against spin									Loading A, landing condition									Loading A, landing condition, slots closed, rudders against spin									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With			
Elevators	U	N (1)	D (1)	U	N (1)	D (1)	U	N	D	U	N	D	U	N	D	U	N	D	U	N (1)	D	U	N	D	U	N	D	
α , deg	27	---	35	31	22	26	47	28	33	N	O	N	O	N	O	---	N	O	---	26	---	33	30	29	29	40	35	30
ϕ , deg	80	---	60	40	60	40	30	40	20	N	O	N	O	N	O	---	N	O	---	30	---	20	30	30	20	20	40	40
\dot{n} , rps	0.13	---	0.16	0.15	0.17	0.18	0.21	0.20	0.21	s	s	s	s	s	s	---	s	s	---	0.14	---	0.19	0.16	0.20	0.21	0.20	0.21	0.22
V, fps	350	383	340	320	360	308	276	320	329	P	P	P	P	P	P	---	P	P	---	319	---	324	303	319	319	276	298	308
Turns for recovery	---	---	---	---	---	---	---	---	---	i	i	i	i	i	i	---	i	i	---	---	---	---	---	---	---	---	---	---

Loading A, landing condition, slots closed																													
Ailerons	Against			Neutral			With																						
Elevators	U (k)	N (1)	D (1)	U	N (1)	D (1)	U	N	D	U	N (1)	D (1)	U	N	D	U	N	D	U	N (1)	D	U	N	D	U	N	D		
α , deg	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---		
ϕ , deg	---	N	N	N	N	N	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---		
\dot{n} , rps	---	O	O	O	O	O	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---		
V, fps	---	s	s	s	s	s	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---		
Turns for recovery	---	P	P	P	P	P	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---	---		

¹Large radius oscillatory spin, average values given.

²Oscillatory spin.

³Increasing radius - may not spin.



*Large radius oscillatory spin, average values given.

†Oscillatory spin.

*Increasing radius - may not spin.

NACA

CHART 4.- SPIN DATA OBTAINED WITH MODEL 4

[Unless otherwise indicated, the steady-spin data are for rudder-with spina of the model in the clean condition with split trailing-edge rudders installed and revised elevon deflections and recoveries were attempted by rapid full rudder reversal, right erect spina.]

	Loading A, circular-arc type rudders installed, original elevon deflections																							
Rudder	With												Neutral											
Ailerons	Against			1/2	Neutral			With			Against			Neutral			With							
	Full				U			1/2	Full															
Elevators	U	N	D	1/2 U	U (a)	N	D	1/2 U	U	1/2 U	N (b)	D	U	N	D	U	N	D	U (b)	N	D			
α , deg	N	N	N	N		N	N	37	34	33	34	N	N	N	N	S	N	N	25	N	N			
ϕ , deg	o	o	o	o		o	o	1U	2U	1U	2U	o	o	o	o	t	o	o	0	o	o			
Ω , rps	s	s	s	s		s	s					s	s	s	s	e	s	s	0.69	s	s			
V, fps	p	p	p	p		p	p			0.67		p	p	p	p	p	p	p		p	p			
	i	i	i	i		i	i					i	i	i	i	i	i	i		i	i			
	n	n	n	n	>190	n	n	196	182	194	180	n	n	n	n	s	n	n	214	n	n			
Turns for recovery	$c_{4\frac{1}{2}}$	$c_{1\frac{3}{2}}$	$cd_{4\frac{1}{2}}$	$c_{1\frac{1}{2}}$		c_7	cd_4		∞			cd_4	c_7	c_5	cd_4	p_{in}	c_5	cd_4		c_{10}	cd_8			
Loading A, circular-arc type rudders installed, original elevon deflections												Loading A, circular-arc type rudders installed, original elevon deflections, modification A												
Rudder	Against												With											
Ailerons	Against			Neutral			With			Against			Neutral			With			Neutral			With		
Elevators	U	N	D	U (a)	N	D	U (b)	N	D	U	N	D	U	N	D	U (e)	N	D	U (a)	N	D	U (e)	N	D
α , deg	N	N	N		N	N	30	N	N	N	N	N	42	45	N	51	46	N		N	33	N	N	
ϕ , deg	o	o	o		o	o	1D	o	o	o	o	o	2U	1U	o	o	o	o	o	o	1D	o	o	
Ω , rps	s	s	s		s	s	0.74	s	s	s	s	s	0.63	0.62	s	0.64	0.61	s		s	0.62	s	s	
V, fps	p	p	p		p	p	208	p	p	p	p	p	171	166	p	158	160	p		p	196	p	p	
	i	i	i		i	i		i	i	i	i	i	i	i	i	i	i	i		i	i	i	i	
	n	n	n	>249	n	n		n	n	n	n	n	n	n	n	n	n	n	231	n	n	n	n	
Turns for recovery	c_4	c_3	$cd_{3\frac{1}{2}}$		c_5	cd_5		c_{12}	$cd_{4\frac{1}{2}}$	c_{10}	c_{12}	cd_{15}	>6	$\frac{1}{2} - \frac{3}{4}$	cd_{11}	$\frac{1}{2}$	$\frac{3}{3}$	cd_{14}		c_7		c_6	cd_6	
Loading A																								
Rudder	With												Against											
Ailerons	Against			Neutral			With			Against			Neutral			With								
Elevators	U	N	D	U	N	D	U	N	D	U (b)	N	D	U (b)	N	D	U (b)	N	D						
α , deg	N	N	N	N	N	N	N	N	N	20	N	N	26	N	N	31	N	N						
ϕ , deg	o	o	o	o	o	o	o	o	o	3D	o	o	3D	o	o	2D	o	o						
Ω , rps	s	s	s	s	s	s	s	s	s	0.53	s	s	0.45	s	s	0.51	s	s						
V, fps	p	p	p	p	p	p	p	p	p	208	p	p	199	p	p	199	p	p						
	i	i	i	i	i	i	i	i	i	i	i	i	i	i	i	i	i	i						
	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n						
Turns for recovery	$c_{\frac{1}{2}}$	c_7	cd_{11}	c_8	c_{10}	cd_7	c_{18}	c_{11}	cd_6		c_8	cd_6		c_7	cd_5			c_{16}	cd_8					
Loading A, modification B																								
Rudder	With												Against											
Ailerons	Against			Neutral			With			Against			Neutral			With								
Elevators	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D						
α , deg	N	N	N	N	N	N	60	N	N	N	N	N	N	N	N	29	N	N						
ϕ , deg	o	o	o	o	o	o	1U	o	o	o	o	o	o	o	o	2D	o	o						
Ω , rps	s	s	s	s	s	s	0.56	s	s	s	s	s	s	s	s	0.52	s	s						
V, fps	p	p	p	p	p	p	163	p	p	p	p	p	p	p	p	182	p	p						
	i	i	i	i	i	i		i	i	i	i	i	i	i	i		i	i						
	n	n	n	n	n	n		n	n	n	n	n	n	n	n		n	n						
Turns for recovery	c_{11}	c_{11}	cd_8	c_{10}	$c_{7\frac{1}{2}}$	cd_7	>7	c_{13}	cd_{10}	c_9	c_5	cd_4	c_7	c_8	$cd_{4\frac{1}{2}}$			c_{10}	cd_6					

^aLarge radius spin; model may eventually recover.

^bWandering spin; slightly oscillatory in pitch.

^cNumber of turns required for model to stop spinning after being launched with initial spin rotation.

^dAfter recovery, model goes inverted.

^eOscillatory in pitch.



CHART 4.- SPIN DATA OBTAINED WITH MODEL 4-CONTINUED

Loading A, modification C

Rudder	With									Against								
Ailerons	Against			Neutral			With			Against			Neutral			With		
Elevators	U	N	D	U (r)	N	D	U (r)	N	D	U (eg)	N	D	U (eg)	N	D	U (eg)	N	D
α , deg	N	N	N	33	N	N	37	45	N	36	N	N	36	N	N	39	39	N
β , deg	o	o	o	2U	o	o	2U	2U	o	1D	o	o	3D	o	o	2D	1D	o
Ω , rps	s	s	s	0.43	s	s	0.46	0.42	s	0.62	s	s	0.50	s	s	0.52	0.65	s
V, fps	p	p	p	188	p	p	180	158	p	180	p	p	176	p	p	180	163	p
Turns for recovery	c ₉	c ₇	cd ₆	=	c ₁₂	cd ₁₂	=	=	cd ₇	=	c ₈	cd ₆	=	c ₇	cd ₆	=	=	cd ₈

Loading A, modification D

Rudder	With									Against								
Ailerons	Against			Neutral			With			Against			Neutral			With		
Elevators	U	N	D	U	N	D	U (eg)	N	D	U	N	D	U	N	D	U	N (eg)	D
α , deg	N	N	N	N	N	N	35	N	N	s	N	N	s	N	N	s	28	N
β , deg	o	o	o	o	o	o	2U	o	o	t	o	o	t	o	o	t	1D	o
Ω , rps	s	s	s	s	s	s	0.53	s	s	e	s	s	e	s	s	e	0.70	s
V, fps	p	p	p	p	p	p	176	p	p	p	p	p	p	p	p	p	260	p
Turns for recovery	c ₁₂	c ₁₈	cd ₁₈	c ₁₅	c ₇	cd ₁₅	=	c ₁₅	cd ₁₀	p	c ₇	cd ₁₀	p	c ₈	cd ₁₀	p	=	cd ₁₂

Loading B, circular-arc type rudders installed,
original elevon deflectionsLoading C, circular-arc type rudders installed,
original elevon deflections

Rudder	With									With								
Ailerons	Against			Neutral			With			Against			Neutral			With		
Elevators	U (h1)	N	D	U (i)	N	D	U (i)	N (i)	D (i)	U	N	D	U	N	D	U	N	D
α , deg	38	N	N	47	43	N	52	47	39	N	N	N	N	N	N	N	N	N
β , deg	8U	o	o	9U	o	o	3U	50	3U	o	o	o	o	o	o	o	o	o
Ω , rps	0.23	s	s	0.41	0.45	p	0.45	0.46	0.45	p	p	p	p	p	p	p	p	p
V, fps	197	n	n	185	185	n	177	174	191	n	n	n	n	n	n	n	n	n
Turns for recovery	j ₁ k ₄	j ₁ k ₄	c ₁₅	c ₁₇	1 ₁ k ₄	>6	c ₁₁	>10	>9	=	c ₄	c ₁₂	c ₅	c ₈	c ₇	cd ₄	c ₃₀	cd ₄

Loading A, modification E

Rudder	With									Against								
Ailerons	Against			Neutral			With			Against			Neutral			With		
Elevators	U	N	D	U (g)	N	D	U	N (g)	D (k)	U	N	D	U (eg)	N	D	U (e)	N (e)	D
α , deg	N	N	N	68	N	N	50	59	70	s	N	N	35	N	N	46	35	N
β , deg	o	o	o	1U	o	o	2U	1U	1U	t	o	o	3D	o	o	1U	3D	o
Ω , rps	s	s	s	0.76	s	s	0.53	0.76	0.86	e	s	s	0.67	s	s	0.63	0.69	s
V, fps	p	p	p	155	p	p	176	126	123	p	p	p	202	p	p	185	185	p
Turns for recovery	c ₂₀	c ₃₀	=	c ₂₂	c ₁₅	=	=	=	d ₇ s	p	c ₁₃	c ₁₂	=	c ₁₃	c ₁₀	=	=	cd ₁₀

c Number of turns required for model to stop spinning after being launched with initial spin rotation.

d After recovery, model goes inverted.

e Oscillatory in pitch.

f Wandering and oscillatory in pitch.

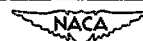
g Wandering spin.

h Large radius spin, model may eventually recover.

i Wandering spin; slightly oscillatory in pitch and roll; range of values given.

j Visual estimate.

k Oscillatory in roll.



UNCLASSIFIED

CHART 4.- SPIN DATA OBTAINED WITH MODEL 4-CONTINUED

Loading D, modification B																		
Rudder	With									Against								
Ailerons	Against			Neutral			With			Against			Neutral			With		
Elevators	U (1)	N (1m)	D (1m)	U (1)	N (1m)	D (1m)	U (1)	N (1m)	D (1m)	U	N	D	U	N	D	U (p)	N (p)	D
α , deg	73	56 25	66 90	75	69 83	58 78	58	60 76	56 81	N o	S t e e p	N o	S t e e p	S t e e p	S t e e p			S t e e p
ϕ , deg	11U	11U 11D	5U 4D	0	0	6U 6D	2U	0	7U 5D	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n			s p i n
Ω , rps	0.91	1.16	1.14	0.96	0.98	0.92	0.71	0.95	0.91							297	278	
V, fps	246	231	231	246	231	234	263	252	240									
Turns for recovery		8 > 10	8 14	>13 n o >8	>15	11	>15	>7	>6	c ₁₄	i n	c ₁₃	i n	i n	i n			c ₁₇

Loading D, modification D										Loading D, modification F									
Rudder	With									Against									
Ailerons	Against			Neutral			With			Against			Neutral			With			
Elevators	U	N	D	U	N	D	U	N	D	U	N	D	U	N	D	U (p)	N	D	U (p)
α , deg	N o	N o	N o	S t e e p	S t e e p	N o	S t e e p	S t e e p	N o	S t e e p	S t e e p	S t e e p	S t e e p	S t e e p	S t e e p			S t e e p	
ϕ , deg	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n			s p i n	
Ω , rps	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	328		p i n	272
V, fps	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n			n	341
Turns for recovery	c ₂₃	c ₂₅	c ₃₀	p i n c ₂₇	p i n c ₃₀	c ₂₀	p i n c ₂₀	p i n c ₂₀	c ₂₃	p i n c ₂₃	p i n c ₂₆	p i n c ₃₀	p i n c ₁₈	p i n c ₁₈	dk ₁₅		dk ₂₀	p i n c ₁₅	c ₁₅

Loading D, modification F										Loading D, modification G									
Rudder	Against									30° With									
Ailerons	Against			Neutral			With			Against			Neutral			With			
Elevators	U	N	D	U	N	D	U	N	D	U	N	D	U (p)	N	D	U	N	D	U (p)
α , deg	N o	N o	N o	S t e e p	S t e e p	N o	S t e e p	S t e e p	N o	N o	N o	N o	S t e e p	N o	N o	S t e e p	S t e e p	N o	S t e e p
ϕ , deg	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n
Ω , rps	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n
V, fps	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	354	309	n	341
Turns for recovery	c ₁₄	c ₁₅	dk ₁₀	p i n c ₁₃	p i n c ₁₂	cd ₁₀	p i n c ₁₅	p i n c ₁₂	c ₁₁	c ₈	cd ₁₂	cd ₁₀	cd ₁₅			c ₁₉	c ₉	c ₈	cd ₁₂

Loading D, modification H										Loading D, modification I									
Rudder	With									Against									
Ailerons	Against			Neutral			With			Against			Neutral			With			
Elevators	U	N	D	U	N	D	U (p)	N	D	U	N	D	U (p)	N	D	U	N	D	U (a)
α , deg	N o	N o	N o	S t e e p	S t e e p	N o	S t e e p	S t e e p	N o	N o	N o	N o	S t e e p	N o	N o	S t e e p	S t e e p	N o	S t e e p
ϕ , deg	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n	s p i n
Ω , rps	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n	p i n
V, fps	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n	n
Turns for recovery	c ₁₄	c ₁₂	c ₁₇	c ₁₅	c ₂₀	c ₂₀			c ₁₅	c ₁₄	c ₁₀	c ₁₀	c ₁₄	c ₈		c ₁₈	c ₂₀	c ₁₈	c ₂₅

c₁Number of turns required for model to stop spinning after being launched with initial spin rotation.d₁After recovery, model goes inverted.l₁Flat and wandering spin.m₁Oscillatory spin; range of values given.n₁Recovery attempted by elevator reversal; stick moved from full back to full left and forward.o₁Recovery attempted by simultaneous rudder and elevator reversal; stick moved from full back to full left and forward.p₁Steep, wandering spin.q₁Number of turns before model strikes safety net.r₁Recovery attempted before model reached final steep attitude.s₁Steep spin.

NACA

CHART 4.- SPIN DATA OBTAINED WITH MODEL 4-CONCLUDED

	Loading D, modification J														Loading D, modification K													
Rudder	With				Against								With				Against											
Ailerons	Neutral	With			Neutral		With			Neutral		With		Neutral			With											
Elevators	U	U	N	D	U (s)	N	U (s)	N	D	N	D	U	N	D	U (m)	N	D	U	D									
α , deg	N		N	N		N		S	N	N	N	N	N	N		N	N	S	N									
β , deg	o		o	o		o		t	o	o	o	o	o	o		o	o	e	o									
Ω , rps	s		s	s		s		e	s	s	s	s	s	s		s	s	n	s									
V, fps	i		i	i		i		p	i	i	i	i	i	i		p	i	i	i									
	n	249	n	n	315	n	315	n	n	n	n	n	n	n	297	n	n	n	n									
Turns for recovery	c ₃₀		c ₃₀	cd ₂₀		cd ₁₅			cd ₁₂	c ₁₂	cd ₁₀	c ₂₀	c ₂₀	cd ₁₀		c ₁₄	cd ₁₀		cd ₁₀									

	Loading D, wing-tip rudders neutral, modification L														Loading D, landing condition, modification B													
Rudder	30° With						30° Against						With															
Ailerons	Against		Neutral		With		Against		Neutral		With		Against		Neutral		With											
Elevators	N	D	U (t)	N	D	N (e)	D (t)	N	D	U (t)	N (t)	D	N (e)	D (t)	U	N	D	U	N	D	U (g)	N (g)	D					
α , deg	N	N	S	S	N	37.66	S	N	N	S	S	N	39	S	S	74	74	S	S	59	N	58	60					
β , deg	o	o	t	t	o	1U	t	o	o	t	t	o	1U	t	o	1U	1D	t	o	1D	o	2D	1D					
Ω , rps	s	s	e	e	s	0.61	e	s	s	e	e	s	0.65	e	s	1.08	1.05	e	s	0.74	s	0.68	0.79					
V, fps	i	i	p	p	i	282	p	i	i	p	p	i	348	p	i	234	234	p	i	240	i	263	252					
Turns for recovery	c ₁₈	c ₁₉	q ₂₁	q ₂₄	q ₂₆	q ₂₆	c ₁₃	q ₁₅	q ₁₈	q ₁₉	cd ₁₆	q ₂₀	q ₃₀	q ₄₀	q ₄₀	q ₇₀	q ₇₀	q ₇₀	q ₇₀	q ₇₀	q ₇₀	q ₇₀						

	Loading D, landing condition, modification B														Loading E, modification B													
Rudder	Against						With						Against															
Ailerons	Against		Neutral		With		Against		Neutral		With		Against		Neutral		With											
Elevators	U	N	D	U	N	D	U (g)	N (eg)	D	U	N	D	U	N	D	U (e)	N	D	U	N	D	U (ep)	N (p)	D (p)				
α , deg	N	N	N	S	S	N		S	S	N	N	N	N	N	N	62	45.75	N	N	N	N	N	22.45					
β , deg	o	o	o	t	t	o		t	t	o	o	o	o	o	o	2U	11D7U	o	o	o	o	o	2D					
Ω , rps	s	s	s	e	e	s		e	s	s	s	s	s	s	s	0.76	0.79	s	s	s	s	s	0.60					
V, fps	i	i	i	p	p	i	341	351	p	i	i	i	i	i	i	202	208	p	i	i	i	i	254	263				
Turns for recovery	c ₂₄	c ₁₄	cd ₁₂	q ₂₇	q ₂₄	q ₂₀			q ₂₁	c ₁₆	c ₃₄	cd ₂₈	c ₁₈	c ₁₄	cd ₅₃	cd _{23/4}	cd _{23/4}	c ₁₁	c ₁₀	cd ₁₂	c ₃₂	c ₁₀	cd ₁₂					

^cNumber of turns required for model to stop spinning after being launched with initial spin rotation.

^aAfter recovery, model goes inverted.

^oOscillatory in pitch.

^sWandering spin.

ⁿOscillatory spin; range of values given.

^rRecovery attempted by elevator reversal, stick moved from full back to full left and forward.

^sRecovery attempted by simultaneous rudder and elevator reversal; stick moved from full back to full left and forward.

^pSteep, wandering spin.

^qNumber of turns before model strikes safety net.

^gSteep spin.

^tAfter launching, spin progressively steepens.



CHART 5.- SPIN DATA OBTAINED WITH MODEL 5

[Unless otherwise indicated, steady-spin data are for rudder-with spins of the model in clean condition and recoveries were attempted by rapid full rudder reversal; right erect spins]

Loading A														Loading A with wing slats extended									
Ailerons	Against					Neutral				With					Against				Neutral		With		
	Full			1/3						1/3		Full			Full			1/3					
	U (a)(b)	N (c)(d)	D (e)	$\frac{2}{3}$ U (f)(g)	$\frac{1}{3}$ U (h)(i)	U (a)(b)	N (c)	D (c)(e)	D (a)(e)	$\frac{2}{3}$ U (a)(e)	U (c)(d)	N (a)	D (a)	U (e)	U (e)	N	$\frac{2}{3}$ U	U	U (c)(h)	N (a)			
α , deg	----	56 71	54 63	41 51	----	----	41 47	39 45	----	----	43 58	----	----	53 58		68 76	50 55	44 54	----	----			
ϕ , deg	----	7D 12U	5D 9U	2U 8U	----	----	1D 8U	1D 5U	----	----	16D 19U	----	----	3D 1U	No spin	4D 0	1D 7D	17D 6U	----	----			
Ω , rps	----	0.37	0.36	0.28	----	----	0.32	0.38	----	----	----	----	----	0.32		0.39	0.32	0.31	----	----			
V, fps	>290	194	191	256	>312	>294	232	230	>312	>334	250	>326	>326	209		191	214	232	----	>312			
Turns for recovery	$f \frac{1}{4}$ $f \frac{1}{2}$	"	"	$g \frac{1}{4}$ $g \frac{1}{2}$	$fg \frac{1}{4}$ $fg \frac{1}{2}$	$f \frac{1}{4}$ $f \frac{1}{2}$	$g \frac{1}{4}$ $g \frac{1}{2}$	$fg \frac{1}{4}$ $fg \frac{1}{2}$	----	$fg \frac{1}{4}$ $fg \frac{1}{2}$	1 $\frac{1}{2}$	----	----	$\frac{1}{4}$ $\frac{1}{2}$		"	$g \frac{1}{4}$ $g \frac{1}{2}$	$\frac{1}{2}$ $\frac{1}{4}$	$\frac{1}{4}$ $\frac{1}{2}$	$f \frac{1}{4}$ $f \frac{1}{2}$			
Loading B														Loading C									
Ailerons	Against				Neutral				With		Against				Neutral				With				
	Full		1/3								Full		1/3										
	U	N (c)(h)	$\frac{2}{3}$ U	U	N	D (e)	D (e)	U (c)(h)	N	U	N	$\frac{2}{3}$ U	U	N (e)	N (e)	U (c)	N						
α , deg	----	68 86	----	----	41 49	----	----	----	----	----	50 55	----	----	40 49	----	39 49	----						
ϕ , deg	----	1D 3U	----	----	2D 5U	----	----	----	----	----	0 6U	----	----	2U 10U	----	10D 10U	----						
Ω , rps	----	0.35	----	----	0.27	----	----	0.21	----	----	0.40	----	----	0.40	----	----	----						
V, fps	>312	186	>300	>300	238	274	>312	244	>362	>326	214	>300	>332	262	>332	256	>332						
Turns for recovery	$f \frac{1}{4}$ $f \frac{1}{2}$	"	$g \frac{1}{4}$ $g \frac{1}{2}$	$fg \frac{1}{4}$ $fg \frac{1}{2}$	1 $\frac{1}{2}$	2 2	----	$\frac{1}{4}$ $\frac{1}{2}$	----	$f \frac{1}{4}$ $f \frac{1}{2}$	$g \frac{1}{4}$ $g \frac{1}{2}$	$fg \frac{1}{4}$ $fg \frac{1}{2}$	$f \frac{1}{4}$ $f \frac{1}{2}$	$g \frac{1}{4}$ $g \frac{1}{2}$	$fg \frac{1}{4}$ $fg \frac{1}{2}$	$f \frac{1}{4}$ $f \frac{1}{2}$	$g \frac{1}{4}$ $g \frac{1}{2}$						

^aSteep spin.

^bLarge radius spin.

^cWandering spin.

^dModel oscillatory in roll and pitch.

^eTwo conditions possible.

^fRecovery attempted before model reached final steeper attitude.

^gRecovery attempted by reversing rudder to only 2/3 against the spin.

^hOscillatory spin.

ⁱVisual estimate.



CHART 6.- SPIN DATA OBTAINED WITH MODEL 6

[Unless otherwise indicated, steady-spin data are for rudder-with spins of the model in clean condition and recoveries were attempted by rapid full rudder reversal; right erect spins.]

[illegible]

⁵Two conditions possible.

^b Recovery attempted by neutralization of the ailerons.

^cModel recovers in an inverted dive.

^dModel oscillatory in pitch.

*Recovery attempted by neutralization of the elevators.

^fRecovery attempted by simultaneous reversal of rudder and elevators.

⁶Recovery attempted by simultaneous neutralization of the rudder and ailerons.

^hRecovery attempted by simultaneous neutralization of elevators and ailerons.

¹Recovery attempted by simultaneous reversal of the rudder and movement of ailerons full against the spin.

- Recovery attempted by reversal of the rudder from full with to 2/3 against the spin.

Upon recovery, model goes into an inverted spin.

²Upon recovery, model goes into a spin in opposite direction.

Recovery attempted by simultaneous reversal of rudder and elevators and movement of ailerons full with the spin.

"Recovery attempted by simultaneous reversal of the rudder and movement of the ailerons full with the spin.

^cRecovery attempted by simultaneous neutralization of the ailerons and reversal of the rudder.

²Wandering spin.

^cModel oscillates in roll, pitch, and yaw.

*Visual estimate.

^aRecovery attempted before model reached final steeper attitude.^tSteep spin.

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CHART 6.- SPIN DATA OBTAINED WITH MODEL 6 - Concluded

	Loading A, modification C										Loading D, modification A													
Ailerons	Against			Neutral			With				Against				Neutral			With						
							1/3	Full			Full			1/3										
Elevators	U	N	D	U	N	D	U	U	N	D	U	N	D	$\frac{2}{3}$	U	N	D	U	N	D				
α , deg	N	N	59	N	N	N	43	51	43	19,33		48	53	38		37		47						
ϕ , deg	N	N	3D, 6U	N	N	N	6D, 5U	0	3D	2D, 14D		0, 11U	2U	7U		1U		0, 11D						
Ω , rps	s	s	0.51	s	s	s	0.38	0.45	0.50	0.80		0.36	0.38	0.32		0.31		0.31						
V, fps	p	p	215	p	p	p	267	245	277	274		>350	258	227	297	>300	290	>300	246		>300			
Turns for recovery	i	i	6 1/2	i	i	i	$\frac{1}{2}$	$\frac{1}{2}$	∞	∞	1/4	∞	>6	$\frac{3}{4}$	1/4	1/2	1/4	1 1/4						
	n	n	∞	n	n	n	$\frac{1}{2}$	$\frac{1}{2}$	∞	∞	1/4	∞	>8	$\frac{3}{4}$	1/4	3/4	1/4	1 1/2		1/4				
	Loading D, modification B										Loading D, modification C													
Ailerons	Against			Neutral						With			Against			Neutral			With					
	Full			1/3												Full			1/3					
Elevators	25° U	U	N	D	$\frac{2}{3}$ U	25° U (p)	U (p)	N	N	D	D	U	N	D	U	N	D	$\frac{2}{3}$ U	U	N	D	U	N	D
α , deg	N	33	43				34	36			N	23				45	48			47				
	o	39	55				41	44			o	41				80	80							
ϕ , deg	s	40	1D				4U	1D			s	14U				15U	20U			1U				
Ω , rps	p	0.35	0.36				0.40	0.45			p	0.41				0.44	0.54			0.42				
V, fps	i	337	227	221	336	283	313	292		283	i	270	395	395	>300	212	215	>300	>300	>300	240	>300	>300	>300
Turns for recovery		r ₂	∞	∞	jr ₄	1/4	r _{1/2}	∞	rt _{1/2}	∞		su ₁	1 1/4	sc _{1/4}	1/2	∞	∞	d _{1/2}	1/2	1/2	1/4	1 1/2	3/4	1/2
		r ₂ 1/2		∞	jr ₅	3/4	r ₃	∞	rt _{1/2}	∞		su ₁	s ₁	sc _{1/2}	3/4	∞	∞	d _{1/2}	1/2	3/4	1/4	2 1/4	1	3/4

^c Model recovers in an inverted dive.

^d Recovery attempted by reversal of the rudder from full with to 2/3 against the spin.

^e Wandering spin.

^f Visual observation.

^g Recovery attempted before model reached final altitude.

^h Steep spin.

ⁱ Upon recovery model goes into a wide spiral.

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CHART 7.- SPIN DATA OBTAINED WITH MODEL 7

[Unless otherwise indicated, steady-spin data are for rudder-with spins of the model in clean condition; right erect spins]

	Loading A, single vertical tail																								
Ailerons	Against												Neutral			With									
	Full			2/3	1/2		1/3		1/4		1/3	Full													
Elevators	U	N	D	N	1/5 U	N	2/3 U	1/5 U	N	1/5 U	N	U	N	D	2/3 U	U	N	D							
α ,deg	N	O	O	N	O	N	O	O	N	O	N	O	O	N	O	N	O	N							
ϕ ,deg	S	S	S	S	S	S	S	S	S	S	S	S	S	S	S	S	S	S							
Ω ,rps	P	P	P	P	P	P	P	P	P	P	P	P	P	P	P	P	P	P							
V ,fps	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11	11							
Loading A, modification A																									
Ailerons	Against					Neutral			With			Against					Neutral			With					
	Full			1/3	1/3				Full	Full			1/3	1/3	Full										
Elevators	U	N	(a)	D (a)	2/3 U	U	N	D	2/3 U	U	N	D	(a)	U (a)	N	D	2/3 U	U	N	D	2/3 U	U	N	D	
α ,deg	N	81	70	N	77	N	O	N	O	N	O	N	81	N	O	N	O	N	O	N	O	N	O	N	O
ϕ ,deg	S	0	2D	S	1U	S	S	S	S	S	S	S	1U	S	S	S	S	S	S	S	S	S	S	S	
Ω ,rps	P	0.33	0.26	P	0.26	P	P	P	P	P	P	P	0.36	P	P	P	P	P	P	P	P	P	P	P	
V ,fps	11	186	186	11	192	11	11	11	11	11	11	11	198	11	11	11	11	11	11	11	11	11	11	11	

^aTwo types of spin.

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CHART 8.- SPIN DATA OBTAINED WITH MODEL 8

[Model launched erect with spinning rotation to right, rudder full right, indicated controls reversed]

Loading	Modifi- cation	Elevator setting prior to movement if any	Aileron setting	Description of model motion before control reversal	Flight path after full rudder reversal	Flight path after simultaneous full reversal of rudder and elevator	Flight path after full elevator reversal
A	None	Full up	Full against	Extremely oscillatory; alternate rolling and yawing motion	Made from 1/4 to 3/4 of a turn and went into stalled glide	Made from 1/4 to 1/2 of a turn and went into steep glide or dive	Made 1/4 of a turn and went into steep glide or dive
A	-do-	---do---	Neutral	Very oscillatory, inner wing dropped and model yawed into spin	Made from 1/4 to 1/2 of a turn and went into stalled glide	Made 1/4 of a turn and went into steep glide or inverted spin	Made from 1/4 to 1 turn and went into steep glide or dive
A	-do-	---do---	Full with	Extremely oscillatory; alternate rolling and yawing motion	Made 1/4 of a turn and went into a stalled glide	Made 1/4 of a turn and went into dive	Made from 1/4 to 1/2 of a turn and went into steep glide or dive
A	-do-	Neutral	Full against	Pitched and rolled onto back; went into left spin when launched with rudder against rotation	---	---	---
A	-do-	---do---	Neutral	Very oscillatory, inner wing dropped and model yawed into spin	Made 1/4 of a turn and went into stalled glide	---	---
A	-do-	---do---	Full with	---do---	Made 1/4 to 1 turn and went into stalled glide	---	---
A	-do-	Down (10°)	Full against	Pitched into dive	---	---	---
A	-do-	---do---	Neutral	Extremely oscillatory; alternate rolling and yawing motions	Would probably have gone on its back after approx. 1-1/2 turns	---	---
A	-do-	---do---	Full with	---do---	Made 1/2 of a turn and rolled on back	---	---
A	A	Full up	Full against	Stalled glide	---	---	---
A	A	---do---	Neutral	---do---	---	---	Went into steep dive
A	A	---do---	Full with	---do---	---	---	Went into erect spin or inverted dive
A	A	Neutral	Full against	---do---	---	---	---
A	A	---do---	Neutral	---do---	---	---	---
A	A	---do---	Full with	---do---	---	---	---
A	A	Down (10°)	Full against	Pitched into dive	---	---	---
A	A	---do---	Neutral	Extremely oscillatory; alternate rolling and yawing motion	Made 1/4 turn and pitched into a dive	---	---
A	A	---do---	Full with	---do---	---	---	---
A	B	Full up	Full with	Stalled spiral glide	Straight stalled glide approx. 1/4 turn after reversal	---	---
A	B	---do---	Neutral	---do---	---do---	---	---
A	B	---do---	Full against	---do---	---do---	---	---
A	B	Neutral	Full with	Wandering, wide radius spin	Stalled glide 1 1/4 turns after reversal	---	---
A	B	---do---	Neutral	---do---	Stalled glide 3/4 turn after reversal	---	---
A	B	---do---	Full against	---do---	Stalled glide 1/2 turn after reversal	---	---
A	B	Full down (20°)	Full with	Spin very oscillatory in pitch and yaw (made approx. 1 turn in flat attitude and 2 in steep attitude, then repeated)	Same as before reversal	---	---
A	B	---do---	Neutral	Steep spin	Went into inverted stalled glide approx. 1/2 turns after	---	---
A	B	---do---	Full against	Went inverted	---	---	---
B	None	Full up (30°)	Full against	Periodically pitched from a flat to a steep attitude	Steep glide, extremely oscillatory in roll and pitch	---	---
B	-do-	---do---	Neutral	Stalled glide, extremely oscillatory in roll	Same as before reversal	---	---
B	-do-	---do---	Full with	Spin very oscillatory in roll and pitch	Made 1/2 of a turn and went into stalled glide	---	---

CHART 8.- SPIN DATA OBTAINED WITH MODEL 8-CONTINUED

Loading	Modification	Elevator setting prior to movement if any	Aileron setting	Description of model motion before control reversal	Flight path after full rudder reversal	Flight path after simultaneous full reversal of rudder and elevator	Flight path after full elevator reversal
B	None	Neutral	Full against	Rolled and pitched on back	Rolled into dive	---	---
B	-do-	---do---	Neutral	Stalled glide, very oscillatory in roll	Same as before reversal	---	---
B	-do-	---do---	Full with	---do---	---do---	---	---
B	-do-	Full down (10°)	Full against	Rolled and yawed into dive or onto back	Stalled glide, extremely oscillatory in roll	---	---
B	-do-	---do---	Neutral	Stalled glide, very oscillatory in yaw and pitch	Stalled glide	---	---
B	-do-	---do---	Full with	Stalled glide	---	---	---
C	-do-	Full up	Full against	Stalled glide, extremely oscillatory in roll, pitch, and yaw	Stalled glide, very oscillatory in roll; rotation stopped in 1 turn	---	---
C	-do-	---do---	Neutral	---do---	Stalled glide, extremely oscillatory in roll; rotation stopped in 3/4 of a turn	---	---
C	-do-	---do---	Full with	Stalled glide, extremely oscillatory in roll	Same as before reversal	---	---
C	-do-	Neutral	Full against	---do---	---do---	---	---
C	-do-	---do---	Neutral	Steep dive	Stalled glide, very oscillatory in roll	---	---
C	-do-	---do---	Full with	Stalled glide	Same as before reversal	---	---
C	-do-	Full down (10°)	Full against	Model yawed and pitched into steep dive	---do---	---	---
C	-do-	---do---	Neutral	Steep glide, very oscillatory in roll	Stalled glide	---	---
C	-do-	---do---	Full with	Stalled glide, sometimes dived into inverted position	Model went into dive	---	---
D	-do-	Full up (30°)	Full against	Stalled glide, extremely oscillatory in roll, yaw, and pitch	Stalled glide, very oscillatory in roll	---	---
D	-do-	---do---	Neutral	---do---	---do---	---	---
D	-do-	---do---	Full with	---do---	---do---	---	---
D	-do-	Neutral	Full against	Model rolled and yawed into steep dive	Same as before reversal	---	---
D	-do-	---do---	Neutral	Moderately steep spin, very oscillatory in roll	Made 1 1/2 turns and went into steep stalled glide	---	---
D	-do-	---do---	Full with	Stalled glide, yawed and banked	Stalled glide	---	---
D	-do-	Full down (10°)	Full against	Rolled and yawed into steep dive	Dive	---	---
D	-do-	---do---	Neutral	Very oscillatory spin, whipping motion in roll and yaw	Made more than 1 turn and went into dive	---	---
D	-do-	---do---	Full with	---do---	---	---	---
E	-do-	Full up	Full against	Violently oscillatory in roll, yaw, and pitch	---	---	---
E	-do-	---do---	Neutral	Stalled glide, very oscillatory in roll and yaw	---	---	---
E	-do-	---do---	Full with	Stalled glide, very oscillatory in roll	---	---	---
E	-do-	Neutral	Full against	Pitched and rolled onto back	---	---	---
E	-do-	---do---	Neutral	Stalled glide, very oscillatory in roll, sometimes rolled onto back	---	---	---
E	-do-	---do---	Full with	Stalled glide, very oscillatory in roll	---	---	---
E	-do-	Full down (10°)	Full against	Rolled and pitched onto back	---	---	---
E	-do-	---do---	Neutral	Rolled and pitched into vertical or inverted position	---	---	---
E	-do-	---do---	Full with	Stalled glide, slightly oscillatory in roll	---	---	---

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CHART 8.- SPIN DATA OBTAINED WITH MODEL 8-CONTINUED

Loading	Modifi- cation	Elevator setting prior to movement if any	Aileron setting	Description of model motion before control reversal	Flight path after full rudder reversal	Flight path after simultaneous full reversal of rudder and elevator	Flight path after full elevator reversal
F	None	Full up (30°)	Full against	Stalled glide	Stalled glide, oscilla- tory in roll	---	---
F	-do-	---do---	Neutral	---do---	Same as before reversal	---	---
F	-do-	---do---	Full with	---do---	Dive or stalled glide	---	---
F	-do-	Neutral	Full against	Steep wandering and very oscillatory spin with whip	Same as before reversal	---	---
F	-do-	---do---	Neutral	---do---	Went into a steep dive in greater than $\frac{1}{2}$ turns	---	---
F	-do-	---do---	Full with	---do---	---	---	---
F	-do-	Full down (10°)	Full against	Steep spin, extremely wandering and oscillatory	Same as before reversal	---	---
F	-do-	---do---	Neutral	Steep wandering and oscil- latory spin with whip	Went into inverted dive	---	---
F	-do-	---do---	Full with	---do---	Same as before reversal	---	---
G	-do-	Full up	Full with	Stalled spiral glide	---	---	---
G	-do-	---do---	Neutral	Stalled glide	---	---	---
G	-do-	---do---	Full against	---do---	---	---	---
G	-do-	Neutral	Full with	Spiral dive	---	---	---
G	-do-	---do---	Neutral	Made 1/2 turn, dived a short distance; motion is repeated	Same as before reversal	---	---
G	-do-	---do---	Full against	Very oscillatory with wide radius; might be spin or spiral glide	Made 1/4 turn and glided (moderately steep)	---	---
G	-do-	Full down (20°)	Full with	Wandering spin with large pitching oscillations; very steep	Made 1 to $2\frac{1}{2}$ turns and went into inverted spins	---	---
G	-do-	---do---	Neutral	---do---	Same as before reversal	---	---
G	-do-	---do---	Full against	Pitched into inverted spin	---	---	---
G	A	Full up	Full with	Spiral glide	---	---	---
G	A	---do---	Neutral	---do---	---	---	---
G	A	---do---	Full against	---do---	---	---	---
G	A	Neutral	Full with	---do---	Same as before reversal	---	---
G	A	---do---	Neutral	---do---	---	---	---
G	A	---do---	Full against	Wandering spin; one yawing oscillation per turn of spin	Made 1/2 turn and went into stalled glide	---	---
G	A	Full down (20°)	Full with	Spiral dive	Made 1/4 turn and went into inverted dive	---	---
G	A	---do---	Neutral	---do---	Made 3/4 turn and went into inverted dive	---	---
G	A	---do---	Full against	Went into inverted spin	---	---	---
H	None	Full up	Full with	Stalled glide	---	---	---
H	-do-	---do---	Neutral	---do---	---	---	---
H	-do-	---do---	Full against	---do---	---	---	---
H	-do-	Neutral	Full with	Wide spiral glide oscilla- tory in pitch	Same as before reversal	---	---
H	-do-	---do---	Neutral	---do---	---	---	---
H	-do-	---do---	Full against	Wide radius spin	Made 1/2 turn and dived	---	---
H	-do-	Full down (20°)	Full with	Spin, oscillatory in roll, pitch, and yaw	Same as before reversal	---	---
H	-do-	---do---	Neutral	Spin, oscillatory in pitch and yaw	---do---	---	---
H	-do-	---do---	Full against	Spin, oscillatory in roll, pitch, and yaw	Made 3/4 turn and went into stalled glide; or made 1/4 turn and went into steep inverted dive	---	---

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CHART 8.- SPIN DATA OBTAINED WITH MODEL 8-CONCLUDED

Loading	Modifi- ca'tion	Elevator setting prior to movement if any	Aileron setting	Description of model motion before control reversal	Flight path after full rudder reversal	Flight path after simultaneous full reversal of rudder and elevator	Flight path after full elevator reversal
I	None	Full up	Full with	Went into a stalled glide	---	---	---
I	-do-	---do---	Neutral	---do---	---	---	---
I	-do-	---do---	Full against	---do---	---	---	---
I	-do-	Neutral	Full with	Steep spin	Same as before reversal	---	---
I	-do-	---do---	Neutral	---do---	---do---	---	---
I	-do-	---do---	Full against	---do---	Dived out after approx. 1 turn	---	---

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CHART 9.- SPIN DATA OBTAINED WITH MODEL 9

[Unless otherwise indicated, steady-spin data are for rudder-with spins of the model in the clean condition with the landing gear extended and stabilizer setting zero and recoveries were attempted by rapid full rudder reversal: right erect spins]


	Loading A						Loading B						Loading C											
Ailerons	Against		Neutral		With		Against		Neutral		With		Against		Neutral		With							
Elevators	U (a)	D	U (a)	N (a)	D	U (a)	D (a)	U (a)	D (c)	U (a)	N (a)	D	U (ad)	D (ad)	U (f)	N	D (f)	U (f)	N (a)	D (a)	U (f)	N	D (a)	
α , deg	-	-	-	-	No spin	-	-	-	-	-	-	No spin	-	-	-	-	-	-	-	-	-	-	-	
ϕ , deg	-	-	-	-		-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-
η , rps	-	-	-	-		-	-	-	-	-	-		-	-	-	-	-	-	-	-	-	-	-	-
V, fps	>245	-	>245	>245		>245	>245	>245	>245	>245	>245		>245	>245	>245	>245	>245	-	>245	>245	>245	>245	>245	-
Turns for recovery	-	-	-	$m \frac{2}{4}$	-	-	-	$m \frac{1}{4}$	e	-	-	-	-	-	$m \frac{2}{2}$	-	$m \frac{2}{2}$	$m \frac{2}{2}$	$m \frac{2}{4}$	$m \frac{1}{4}$	$m \frac{2}{4}$	$m \frac{2}{2}$	-	$m \frac{2}{4}$

	Loading D						Loading E						Loading F										
Ailerons	Against		Neutral		With		Against		Neutral		With		Against		Neutral		With						
Elevators	U (f)	D	U (f)	N (a)	D (a)	U (f)	D (a)	U (f)	N (ag)	D (ag)	U (f)	N (f)	D (a)	U (f)	N (f)	D	U (f)	N (f)	D (f)	U	N	D (f)	
α , deg	-	28	-	-	-	-	-	-	-	58	-	-	-	-	-	-	53	-	-	-	43	38	-
ϕ , deg	-	3U	-	-	-	-	-	-	-	1D	-	-	-	-	-	-	2D	-	-	-	5D	7D	-
η , rps	-	0.61	-	-	-	-	-	-	-	0.53	-	-	-	-	-	-	0.76	-	-	-	0.66	0.80	-
V, fps	>245	162	>245	>245	>245	>245	>245	>245	-	>245	89	>245	>245	>245	>245	>245	104	>245	>245	>245	147	169	>245
Turns for recovery	$m \frac{1}{2}$	3	$m \frac{2}{2}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{1}{2}$	-	-	$m \frac{2}{2}$	$m \frac{2}{2}$	$m \frac{2}{4}$	$m \frac{2}{4}$	-	$m \frac{2}{4}$	$m \frac{2}{2}$	$m \frac{2}{2}$	-	$m \frac{2}{2}$	$m \frac{2}{2}$	$m \frac{2}{2}$	-

	Loading G						Loading H						Loading I									
Ailerons	Against		Neutral		With		Against		Neutral		With		Against		Neutral		With					
Elevators	U (i)	D (i)	U (a)	N (a)	D (a)	U	U (f)	D	U (jk)	N (jk)	D (fj)	U (j)	D (i)	U (a)	N (i)	D	U	N	D	U	N	D (a)
α , deg	No	-	-	-	-	43	No	69	-	-	-	39	-	-	No	67	43	62	59	49	45	-
ϕ , deg	-	-	-	-	-	1D	-	4D	-	-	-	7D	-	-	-	1D	0	1D	2D	1D	0	-
η , rps	-	-	-	-	-	0.88	-	0.72	-	-	-	0.57	-	-	-	0.78	0.64	0.71	0.73	0.68	0.66	-
V, fps	>245	>245	>245	>245	>245	147	>245	116	>245	>245	>245	184	>245	>245	>245	184	122	202	155	145	158	>245
Turns for recovery	$m \frac{2}{2}$	-	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	8	$m \frac{2}{2}$	-	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	>2	-	3	-	-	8	-	-	-

	Loading A leading edge of stabilizer 30° down						Loading C leading edge of stabilizer 30° down						Loading F leading edge of stabilizer 30° down						Loading I, leading edge of stabilizer 30° down		
Ailerons	Against		Neutral		With		Against		Neutral		With		Against		Neutral		With		Against		
Elevators	U	D (c)	U	N (c)	U	D	U	D (c)	U (c)	N (c)	D (c)	U (a)	D (c)	U	N	D	U	D	U	N	D
α , deg	No	-	-	-	59	59	No	-	-	-	-	-	No	-	-	-	58	54	No	-	-
ϕ , deg	-	-	-	-	3D	2D	-	-	-	-	-	-	-	-	-	-	2D	3D	-	-	-
η , rps	-	-	-	-	0.57	0.77	-	-	-	-	-	-	-	-	-	-	0.72	0.72	-	-	-
V, fps	>245	>245	>245	>245	87	87	>245	>245	>245	>245	>245	>245	>245	>245	>245	>245	125	124	>245	>245	>245
Turns for recovery	$m \frac{2}{4}$	-	$m \frac{2}{4}$	-	-	-	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{4}$	$m \frac{2}{2}$	-	-	-	-	>6

	Loading I rudder-against spins landing gear retracted						Loading I leading edge of stabilizer 30° down landing gear retracted					
Ailerons	Against		Neutral		With		Against		Neutral		With	
Elevators	U	N	U	N	U	D (a)	U	N	U	N	U	D
α , deg	No	-	No	-	-	-	No	-	No	-	-	-
ϕ , deg	-	-	-	-	-	-	-	-	-	-	-	-
η , rps	-	-	-	-	-	-	-	-	-	-	-	-
V, fps	127	127	165	149	160	195	173	216	160	142	136	136
Turns for recovery	-	-	-	-	-	-	$m \frac{2}{4}$	$m \frac{2}{4}$	-	-	-	-



*Steep spin.

*Recovery attempted before model reached final steeper attitude

*Moderately steep spin with increasing radius.

*Model attitude did not change after rudder reversal.

*Slow recovery.

*Steep spin with increasing radius.

*Two types of spin.

When launched in a flat attitude with the rudder against the rotation, the model ceased rotating after indicated number of turns.

*Steep spin with small radius.

*Wandering spin, rate of rotation varies.

*Wide radius of spin

*Two conditions possible.

*The model recovered in less turns than indicated.



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CHART 10.- SPIN DATA OBTAINED WITH MODEL 10

[Unless otherwise indicated, steady-spin data are for rudder-with spins of the model in the clean condition and recoveries were attempted by rapid full rudder reversal, propellers off except] where indicated

Loading A, left erect spins																	
Ailerons	Against								Neutral					With			
	Full			1/2	1/3		1/4										
Elevators	U	N (a)	D (a)	D (a)	$\frac{2}{3}U$ (b)	$\frac{2}{3}U$ (a)(b)	D (b)	D (b)	U (b)	U (a)(b)	N (b)	N (a)(b)	D	U (a)	N	D	
α , deg	N o s p i n	68 82	69 77	65 76	-----	74 85	---	---	N o s p i n	64 72	-----	48 72	-----	60 76	-----	-----	
ϕ , deg		7D 3U	7D 5U	4D 4U	-----	6D 3U	---	---		2D 4U	-----	3D 2U	-----	3D 3U	-----	-----	
Ω , rps		0.71	0.59	0.60	-----	0.78	---	0.61		0.41	0.55	0.54	-----	0.56	-----	-----	
V, fps		182	194	196	>304	196	>304	199		262	199	274	>304	210	>304	>304	
Turns for recovery		c_3 c_7 1/2	"	"	d_1, e_1 d_1 1/2	e_2 e_2 1/2	d_3 d_4	"		1 1 1/2	e_2	e_2 1/2	d_1 d_2	"	d_1 d_2	d_1	
Loading A, right erect spins																	
Ailerons	Against				Neutral				With								
	Full		1/3					1/3		Full							
Elevators	U	N	D (a)(1)	$\frac{2}{3}U$	U	N (a)	D	$\frac{2}{3}U$ (b)	$\frac{2}{3}U$ (a)(b)	U	N	D					
α , deg	N o s p i n	-----	61 89	-----	-----	42 50	-----	-----	57 63	-----	-----	-----					
ϕ , deg		-----	15D 10U	-----	-----	7D 6U	-----	-----	2D 2U	-----	-----	-----					
Ω , rps		0.72	0.52	-----	-----	0.55	-----	-----	0.52	0.51	-----	-----					
V, fps		188	188	>304	>338	274	>370	>332	244	244	>304	>304					
Turns for recovery		"	"	d_1, e_1 1/2	d_1, e_1 1/2	2 7	d_2 d_3 3/4	d_1, e_1 d_1, e_1	e_2	"	d_2 d_2 1/2	d_3 3/4 d_1 1/2					
Loading A, left spins propeller pitch = 30°					Loading A, right erect spins, stability flaps deflected 25° down												
Ailerons	Against		With		Against				Neutral		With						
	1/3	1/3	Full	Full	1/3	Neutral		1/3	With								
Elevators	$\frac{2}{3}U$	$\frac{2}{3}U$ (b)	$\frac{2}{3}U$ (a)(b)	U (a)	U	N (a)(j)	D (a)(b)	D (a)(b)	$\frac{2}{3}U$	U	N (k)	$\frac{2}{3}U$ (a)	U	N (k)			
α , deg	N o s p i n	N o s p i n	40 57	40 48	N o s p i n	70 86	64 79	50 57	-----	N o s p i n	---	40 48	-----	-----			
ϕ , deg			2D 7U	0 5U		3D 4U	12D 8U	4D 3U	-----		-----	4D 4U	-----	-----			
Ω , rps			0.33	0.30		0.45	0.52	0.45	0.40		-----	0.36	0.40	0.42			
V, fps			241	244		177	199	233	227		>340	280	262	>370			
Turns for recovery			e >6	>2 3/4 >6		>5 "	"	5	e_1 1/4 e_1 1/2		e_1 1/2	e_1 1/2 e_1 1/2	>1 1/2 e_1 >3	>3 1/2 >6	>2 >3		

^aOscillatory spin; range of values or average value given.

^bTwo conditions possible.

^cRecovery attempted by simultaneous reversal of rudders to full against the spin and stick to longitudinally full back.

^dRecovery attempted before final steep attitude.

^eRecovery attempted by reversing rudders to 2/3 against the spin.

^fRecovery attempted by simultaneous reversal of rudders to full against the spin and of stick to longitudinally full back and laterally full against the spin.

^gRecovery attempted by simultaneous reversal of rudders to full against the spin and of stick longitudinally forward and laterally full with the spin.

^hVisual estimate.

ⁱWide radius spin.

^jWandering spin.

^kSteep spin.

^lModel recovers in a steep dive.

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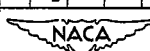
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CHART 11.- SPIN DATA OBTAINED WITH MODEL 11

[Unless otherwise indicated, steady spin data are for rudder-with spins of the model in the clean condition and recoveries were attempted by rapid full rudder reversal, elevator U, N, and D signifies stick positions of back, neutral, and forward, right erect spins]

	Loading A, rudders against the spin									Loading A									Loading A, flaps down 45°									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With			
Elevators	U (a)	N (a)	D (a)	U (b)	N (b)	D (b)	U (c)	N (c)	D (c)	U (a)	N (a)	D (a)	U (d)	N (d)	D (d)	U (b)	N (b)	D (b)	U	N	D	U (d)	U (dg)	N (d)	N (d)	U (b)	N	D (b)
α , deg	-	-	-	-	-	-	-	-	-	-	-	-	82	86	83	-	-	-	90	90	81	84	88	86	84	-	-	-
β , deg	-	-	-	-	-	-	-	-	-	-	-	-	41D 30U	39D 38U	32D 29U	-	-	-	5U	6U	36D 50U	20D 25U	3D 9U	8D 19D	19D 18U	-	-	-
Ω , rps	-	-	-	-	-	-	-	-	-	-	-	-	0.13	0.08	0.10	-	-	-	0.69	0.04	0.22	0.18	0.35	0.15	0.19	-	-	-
V , fps	-	-	-	-	-	-	-	-	-	-	-	-	121	121	118	-	-	-	107	113	123	118	118	116	118	-	-	-
Turns for recovery	-	-	-	-	-	-	-	-	-	-	-	-	e_1 2	e_1 4	e_3 4	-	-	-	-	-	-	-	-	-	-	-	-	-
	Loading B									Loading C									Loading D									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With			
Elevators	U (a)	N	D (a)	U (a)	N (a)	D (a)	U (b)	N	D (b)	U (a)	N	D (a)	U (d)	N	D (d)	U (b)	N	D (b)	U (a)	N	D (a)	U (d)	N (d)	D	U (b)	N	D (b)	
α , deg	-	-	-	-	-	-	-	-	-	-	-	-	82	-	80	-	-	-	-	-	-	80	83	-	-	-	-	
β , deg	-	-	-	-	-	-	-	-	-	-	-	-	33D 20U	-	30D 26U	-	-	-	-	-	-	19D 24U	42D 39U	-	-	-	-	
Ω , rps	-	-	-	-	-	-	-	-	-	-	-	-	0.10	-	0.12	-	-	-	-	-	-	0.08	0.06	-	-	-	-	
V , fps	-	-	-	-	-	-	-	-	-	-	-	-	118	-	118	-	-	-	-	-	-	121	121	-	-	-	-	
Turns for recovery	-	-	-	-	-	-	-	-	-	-	-	-	e_3 4	-	e_1 2	-	-	-	-	-	-	e_3 4	e_3 4	-	-	-	-	
	Loading E									Loading F									Loading G									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With			
Elevators	U (a)	N	D (a)	U (a)	N	D (a)	U (b)	N	D (b)	U (a)	N	D (a)	U (d)	N	D (d)	U (b)	N	D (b)	U (a)	N	D (a)	U	N	D (g)	D (g)	U (h)	N (h)	D (i)
α , deg	-	-	-	-	-	-	-	-	-	-	-	-	76	---	72	-	-	-	-	-	-	56	57	42	61	-	-	-
β , deg	-	-	-	-	-	-	-	-	-	-	-	-	22D 32U	---	17D 12U	-	-	-	-	-	-	3D	2D	6U	1D	-	-	-
Ω , rps	-	-	-	-	-	-	-	-	-	-	-	-	0.08	---	---	-	-	-	-	-	-	0.15	0.15	0.20	---	-	-	-
V , fps	-	-	-	-	-	-	-	-	-	-	-	-	123	123	121	-	-	-	-	-	-	125	129	138	135	-	-	-
Turns for recovery	-	-	-	-	-	-	-	-	-	-	-	-	e_1 4	e_1 2	e_1 4	-	-	-	-	-	-	f_1 2	f_3 4	f_3 4	f_3 4	-	-	-
	Loading H																											
Ailerons	Against			Neutral			With																					
Elevators	U	N	D	U	N	D	U	N	D																			
α , deg	----	58	46	58	52	41	32	33	35																			
β , deg	----	8U	14U	5U	6U	12U	4U	6U	9U																			
Ω , rps	0.39	0.38	0.40	0.41	0.39	0.42	0.43	0.42	0.46																			
V , fps	123	129	135	118	123	141	160	157	160																			
Turns for recovery	-	>5	-	-	-	-	> $\frac{1}{2}$	> $\frac{1}{2}$	-																			



*Oscillated violently in pitch and roll. Rate of rotation decreased as the violence of the oscillations increased.

^bInitial rotation stopped. Fuselage remained approximately horizontal.

^cInitial rotation stopped. Model then began to rotate in opposite direction and oscillated violently in pitch and roll. Rate of rotation decreased as violence of the oscillations increased.

^dOscillated in roll.

^eFuselage remained approximately horizontal after rotation stopped in number of turns indicated.

^fModel nosed over into steep dive after rotation stopped in number of turns indicated.

^gTwo types of spin.

^hSlid around with large radius. Nose approximately 40° below horizontal.

ⁱSlid around with large radius. Nose approximately 40° below horizontal. After a few turns nosed over and went into inverted dive.

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CHART 11.- SPIN DATA OBTAINED WITH MODEL 11 (CONCLUDED)

	Loading A, landing condition									Loading A			Loading A, flaps down 45°			Loading A			Loading A, flaps down 45°			Loading A, freely rotating propeller installed														
Ailerons	Against			Neutral			With			Modification A			Modification A			Modification B			Modification B			Against			Neutral			With								
Elevators	U (d)	N (d)	D (d)	U (d)	N (d)	D (d)	U (b)	N (b)	D (b)	U (b)	N (b)	D (j)	U (d)	N (d)	D (j)	U (j)	N (j)	D (k)	U (d)	N (d)	D (k)	U (a)	N (a)	D (a)	U (d)	N (d)	D (c)	U (c)	N (c)	D (b)						
α , deg	83	80	68	82	89	78	-	-	-	-	-	-	75	79	-	-	-	-	79	83	-	-	-	-	65	80	-	-	-							
ϕ , deg	39D 51U	42D 48U	41D 44U	21D 25U	16D 23U	20D 18U	-	-	-	-	-	-	16D 12U	21D 17U	-	-	-	-	41D 26U	5U	-	-	-	-	36D 31U	28D 25U	-	-	-							
n, rps	0.15	0.14	0.17	0.17	0.13	0.14	-	-	-	-	-	-	0.11	0.11	-	-	-	-	0.31	0.27	-	-	-	-	0.07	0.10	-	-	-							
V, fps	123	121	121	121	118	121	-	-	-	-	-	-	116	116	-	-	-	-	107	107	-	-	-	-	121	121	118	-	-	-						
Turns for recovery	$>\frac{3}{2}$	$e\frac{1}{2}$	>5	e_1	e_1	$e\frac{3}{4}$	-	-	-	-	-	-	$e\frac{1}{4}$	$e\frac{1}{2}$	-	-	-	-	$\frac{1}{2}$ $2\frac{3}{4}$	$\frac{1}{2}$	-	-	-	$e\frac{1}{2}$	$e\frac{1}{2}$	$e\frac{1}{2}$	-	-	-							
Loading A, modification C									Loading A, modification D									Loading A, modification E									Loading A, modification F.									
Ailerons	Against			Neutral			With			Against			Neutral			With			Against			Neutral			With			Against			Neutral			With		
Elevators	U	N	D (a)	U	N	D (j)	U	N	D (j)	U	N	D (a)	U	N	D (a)	U	N	D (b)	U	N	D (b)	U	N	D (a)	U	N	D (a)	U	N	D (b)						
α , deg	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	76	80	-	-	-	-	-	-	-	-	-	-	-						
ϕ , deg	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	34D 19U	34D 46U	-	-	-	-	-	-	-	-	-	-	-						
n, rps	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	0.08	0.14	-	-	-	-	-	-	-	-	-	-	-						
V, fps	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	127	129	-	-	-	-	-	-	-	-	-	-	-						
Turns for recovery	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	$e\frac{3}{4}$	$e\frac{1}{2}$	-	-	-	-	-	-	-	-	-	-	-						
Loading A, modification G									Loading A, modification H																											
Ailerons	Against			Neutral			With			Against			Neutral			With																				
Elevators	U	N	D (a)	U	N	D (d)	U	N	D (b)	U	N	D (a)	U	N	D (d)	U	N	D (b)																		
α , deg	-	-	-	-	-	78	-	-	-	-	-	-	-	-	84	-	-	-																		
ϕ , deg	-	-	-	-	-	12D 9U	-	-	-	-	-	-	-	-	20D 30U	-	-	-																		
n, rps	-	-	-	-	-	---	-	-	-	-	-	-	-	-	---	-	-	-																		
V, fps	-	-	-	-	-	121	-	-	-	-	-	-	-	-	121	-	-	-																		
Turns for recovery	-	-	-	-	-	$e\frac{3}{4}$	-	-	-	-	-	-	-	-	$e\frac{3}{4}$	-	-	-																		





^aOscillated violently in pitch and roll. Rate of rotation decreased as the violence of the oscillations increased.

^bInitial rotation stopped. Fuselage remained approximately horizontal.

^cInitial rotation stopped. Model then began to rotate in opposite direction and oscillated violently in pitch and roll. Rate of rotation decreased as violence of the oscillations increased.

^dOscillated in roll.

^eFuselage remained approximately horizontal.

^fInitial rotation stopped. Glided forward rapidly with nose approximately 15° below horizontal.

^gInitial rotation stopped. Model nosed over into steep dive.

^hGlided forward rapidly with nose approximately 15° below horizontal.

ⁱInitial rotation stopped. Glided forward for a few feet 35° below horizontal and then nosed over into a steep dive.

^jInitial rotation stopped. Glided with slight rotation to right. Fuselage approximately horizontal. Oscillation in roll of approximately 125°.

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CHART 12.- SPIN DATA OBTAINED WITH MODEL 12

[Unless otherwise indicated, steady-spin data are for rudder-with spins of the model in the clean condition and recoveries were attempted by rapid full rudder reversal; elevator U, N, and D signifies stick positions of back, neutral, and forward, right erect spins]

	Loading A , right spins															Loading A , left spins																								
Ailerons	Against					Neutral					With					Against					Neutral					With														
Elevators	U (a)	N (ab)	N (bc)	D (c)	Free (e)	U (d)	N (d)	D (d)	Free (e)	U (d)	N (d)	D (d)	Free (d)	U (a)	N (a)	D (c)	Free (e)	U (d)	N (d)	D (c)	Free (e)	U (d)	N (d)	D (bd)	D (bi)	Free (bd)	Free (b)													
α , deg	90 74	95 59				74	91 71	76 58	73 62	88 62	---	97 66	83 57	82 54	94 55			66 54	86 69			73 62	97 64	74 61	---	79 52														
β , deg	6U 8D	9U 17D	N o	N o	N o	12U 18D	22U 5D	19U 12D	18U 7D	18U 19D	---	6U 18D	10U 15D	10U 6D	2U	N o	N o	9U 12D	13U 15D	N o	N o	12U 12D	19U 24D	10U 7D	---	11U 21D	N o													
Ω , rps	0.19	0.15	s p i n	s p i n	s p i n	0.19	0.21	0.26	0.20	0.20	0.13	0.21	0.21	---	0.11	s p i n	s p i n	0.13	0.11	s p i n	s p i n	0.15	0.09	0.16	---	0.16	s p i n													
V, fps	182	182				182	171	174	171	171	171	171	166	179	171			171	171			171	161	171	---	185														
Turns for recovery	$e\frac{1}{4}$	$f\frac{1}{2}$				$e\frac{1}{4}$	$e\frac{1}{4}$	$g\frac{1}{4}$	$g\frac{1}{2}$	$e\frac{1}{2}$	$f\frac{1}{2}$	$g\frac{1}{2}$	$h\frac{1}{2}$	$f\frac{1}{2}$	$e\frac{1}{2}$			$e\frac{1}{4}$	$f\frac{1}{4}$			$e\frac{1}{4}$	$e\frac{1}{4}$	$h\frac{1}{2}$	---	$f\frac{3}{4}$														
Loading A, wing-tip trimmers used in conjunction with the ailerons, 1 to 1 deflection ratio between ailerons and the trimmers						Loading A, wing-tip trimmers used in conjunction with the rudders, 1 to 1 deflection ratio between the rudders and the trimmers. Trimmer moves up as adjacent rudder moves outboard.										Loading A, wing-tip trimmer used in conjunction with the elevator. 2 to 1 deflection ratio between the elevator and the trimmers. Trailing edge of trimmer moves up as trailing edge of elevator moves down.																								
Ailerons	Against					With					Against					Neutral					With					Against					Neutral					With				
Elevators	U (a)	D (c)	Free (e)	U (a)	D (ab)	D (bi)	Free (a)	U (j)	D (j)	Free (j)	U (j)	N (dk)	D (j)	Free (j)	U (d)	N (d)	D (j)	Free (ab)	Free (bj)	U (c)	D (c)	U (c)	D (c)	U (c)	D (d)	U (d)	D (d)													
α , deg	N o	N o	N o		94 63	78 59	----	71 56	N o	N o	N o		81 71	N o	N o	65 60			74 41	N o	N o	N o	N o	N o	60 87	92 54	92 53													
β , deg	s p i n	s p i n	s p i n		29U 31D	11U 24D	----	2U 16D	s p i n	s p i n	s p i n		1U 43D	s p i n	s p i n	12U 11D	38U 13D		2U 14D	s p i n	s p i n	s p i n	s p i n	3U 31U	44U 47D	23U 22D														
Ω , rps					0.17	0.18	----	0.17					0.08			0.12	0.12		0.16					0.18	0.21	0.18														
V, fps					171	174	----	174					171			182	189		198					174	189	171														
Turns for recovery					$e\frac{1}{2}$	$e\frac{1}{2}$	----	$e\frac{1}{2}$					$e\frac{1}{4}$			$e\frac{3}{4}$	$e\frac{1}{2}$		----					$h\frac{1}{4}$	$e\frac{1}{4}$	$f\frac{3}{4}$														
Loading B															Loading C																									
Ailerons	Against					Neutral					With					Against					Neutral					With														
Elevators	U (c)	D (b)	D (bd)	Free (m)	U (j)	N (a)	D (m)	Free (bd)	Free (b)	U (d)	D (bd)	D (bd)	Free (dk)	U (a)	D	Free (c)	U (d)	N (a)	D (d)	Free (d)	U (d)	D (d)	U (d)	D (d)	Free (p)															
α , deg			74 41			92 72		68 52		71 58	70	75 47	78 58	89 55			87 30	96 60	77 56	72 57	73 60	77 60	----																	
β , deg	N o	N o	10U 11D	N o	N o	58U 75D	N o	16U 9D	N o	2D 33D	28U 25D	10U 17D	17U 25D	50U 25D			38U 38D	56U 67D	22U 31D	13U 7D	20D 41D	32U 20D	----																	
Ω , rps	s p i n	s p i n	0.11	s p i n	s p i n	0.09	s p i n	0.18	s p i n	0.17	0.16	0.15	0.18	0.23			0.20	0.17	0.23	0.24	0.19	0.25	----																	
V, fps			182			182		182		190	182	177	185	190			179	183	177	179	174	174	----																	
Turns for recovery			----			$e\frac{1}{2}$		$h\frac{1}{4}$		$e\frac{1}{2}$	$f\frac{3}{4}$	$f\frac{1}{2}$	$n\frac{2}{2}$	$e\frac{3}{4}$			$e\frac{1}{2}$	$f\frac{1}{2}$	$h\frac{1}{4}$	$h\frac{1}{2}$	$e\frac{1}{2}$	$h\frac{1}{4}$	----																	

*Model oscillatory in roll and pitch; range of values or average value given.

^bTwo conditions possible.

^cModel recovered by pitching and/or rolling out of the spin. Motion during recovery was extremely violent.

^dOscillatory spin; range of values or average value given.

^eAfter recovery, model glided forward at a flat attitude for an appreciable distance before striking safety net.

^fAfter recovery, model glided forward at a flat attitude for a short distance before striking safety net.

^gAfter recovery, model glided forward at a flat attitude for a short distance and then nosed down into a steep dive.

^hAfter recovery model nosed down into a steep dive.

ⁱModel too oscillatory in pitch and roll to test completely.

^jModel yawed in a circle of extremely large radius at a high angle of attack. Rotational velocity was low.

^kWandering spin.

^lModel oscillates in pitch and wanders; appears to gallop.

^mModel recovered of its own accord in a wide spiral glide.

ⁿModel recovered in a wide spiral glide.

^oModel went into an inverted spin after a short vertical dive.

^pHigh rate of descent. Model executed one violent oscillation in pitch per turn of spin.



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CHART 12.- SPIN DATA OBTAINED WITH MODEL 12 (CONCLUDED)

	Loading D																Loading E																														
Ailerons	Against					Neutral					With						Against					Neutral					With																				
Elevators	U (c)	N (c)	D (c)	Free (bd)	Free (b)	U (d)	N (d)	D (d)	Free (bd)	Free (b)	U (d)	N (d)	D (d)	Free (bd)	Free (b)	U (a)	N (a)	D (a)	Free (c)	U (d)	N (d)	D (d)	Free (bd)	Free (b)	U (d)	N (d)	D (d)	Free (bd)	Free (b)	U (d)	N (d)	D (d)	Free (bd)	Free (b)													
α , deg				57 41		73 21	85 48	49 39	73 50	52 37	75 63	84 55	---	76 43	44 44	95 47	81 65				98 68				93 64	---		90 65	98 79	102 61																	
β , deg	No spin	No spin	No spin	22U 0	No spin	21U 18D	50U 42D	8U 5D	11U 7D	1U 15D	30U 12D	19U 14D	---	0 14D	13U 6D	61U 48D	35U 64D	No spin	No spin	No spin	33D 48D	No spin	No spin	No spin	42U 47D	---	No spin	24U 44D	---	39U 44D	No spin	No spin	No spin	No spin													
Ω , rps				0.18		0.13 0.20	0.20 0.19	0.19 0.22	0.22 0.21	0.20 0.22	0.22 ---	0.20 ---	0.17 ---	0.16 ---	0.17 ---	0.16 ---	0.17 ---				0.18				0.22	---		0.16 0.13	0.16 0.16																		
V, fps				204		174 171	203 177	177 206	177 206	177 177	---	182 208	193 185								182				185	---		179 182	171 171																		
Turns for recovery				----		e ₁ 4	e ₁ 2	h ₁ 2	h ₁ 1	h ₁ 1	e ₂ 4	h ₁ 2	---	h ₁ 4	----	e ₁ 2	e ₁ 1				e ₁ 1				e ₂ 4	---		f ₂ 4	e ₁ 1	e ₁ 2																	
Loading A, flaps down 15°																Loading A, landing gear extended																Loading A, landing condition															
Ailerons	Neutral					With					Neutral						With						Against					Neutral					With														
Elevators	D (d)	Free (bd)	Free (bs)	U (a)	D (a)	Free (dt)	D (dt)	D (dt)	Free (dt)	Free (dt)	Free (st)	D (d)	Free (d)	D (i)	Free (d)	U (bs)	U (bd)	N (d)	Free (d)	U (d)	D (d)	Free (d)	U (d)	D (d)	Free (d)	U (d)	D (d)	Free (d)	U (d)	D (d)	Free (d)	U (d)	D (d)														
α , deg	79 62	82 63	----	----	87 49	87 57	72 41	----	60 41	50 37	----	61 46	65 52			66 22	----	65 54	91 69	62 47	65 58	78 58	64 29																								
β , deg	10U 27D	25U 18D	----	----	9U 9D	3D 10D	11U 8D	----	1D 3U	3U ----	----	8D 3D	3D ----			16U 2U	----	12U 14D	27U 40D	9U 3D	20U 15U	15U 25D	13U 15D																								
Ω , rps	0.21	0.19	----	----	0.17	0.19	0.20	0.19	----	0.19	0.23	----	0.16	0.16			0.15	----	0.14	0.09	0.16	0.16	0.16	0.14																							
V, fcs	179	179	----	----	179	179	185	198	----	182	201	----	195	193			198	----	176	171	188	179	176	183																							
Turns for recovery	h ₁ 4	h ₂ 4	----	----	h ₃ 4	h ₂ 4	h ₃ 4	h ₁ 2	----	h ₃ 4	----	----	h ₂ 4	h ₁ 1			h ₁ 2	----	e ₁ 2	e ₁ 4	h ₁ 2	f ₁ 4	h ₁ 2	h ₁ 4																							

- ^aModel oscillatory in roll and pitch, range of values or average value given.
- ^bTwo conditions possible.
- ^cModel recovered by pitching and for rolling out of the spin. Motion during recovery was extremely violent.
- ^dOscillatory spin, range of values or average value given.
- ^eAfter recovery, model glided forward at a flat attitude for an appreciable distance before striking safety net.
- ^fAfter recovery, model glided forward at a flat attitude for a short distance before striking safety net.
- ^gAfter recovery, model glided forward at a flat attitude for a short distance, and then nosed down into a steep dive.
- ^hAfter recovery model nosed down into a steep dive.
- ⁱModel too oscillatory in pitch and roll to test completely.
- ^jModel yawed in a circle of extremely large radius at a high angle of attack. Rotational velocity was low.

- ^kWandering spin.
- ^lModel oscillates in pitch and wanders; appears to gallop.
- ^mModel oscillatory in pitch and roll, too wandering to test.
- ⁿModel oscillatory in pitch and appears to gallop; range of values or average value given.
- ^oModel spins steeply and smoothly with radius of spin too large to test.
- ^pThree conditions possible.
- ^qModel pitched into an inverted flat attitude after short vertical dive.

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CHART 14.- RESULTS OF SPIN-RECOVERY PARACHUTE TESTS FOR MODELS

[Model in clean condition except where otherwise indicated; all results are for spin rotation to pilot's right, dimensions given are full-scale]

Model	Attitude	Parachute location	Parachute diameter (ft)	Towline length (ft)	Drag coefficient	Loading	Turns for recovery								Remarks
							Elevator								
							U		2/3U		N		D		
							Ailerons								
Against	Neutral	With	1/3 against	1/3 with	Neutral	With	Against	Neutral							
2	Erect	Outboard wing	5.0	2.5	0.70	A	---	=	---	---	---	---	---	---	Towline attached between pitch flap and elevator
	-do-	-do-	-do-	15.0	-do-	-do-	---	1, $\frac{1}{2}$	=	---	---	---	---	---	Do.
	-do-	-do-	-do-	30.0	-do-	-do-	---	1, $\frac{1}{2}$	=	---	---	> 3	=	---	Do.
	-do-	-do-	7.0	2.5	-do-	-do-	---	$\frac{3}{4}$, =	=	---	$\frac{3}{4}$, $\frac{1}{4}$	=	---	---	Do.
	-do-	-do-	-do-	15	-do-	-do-	---	$\frac{3}{4}$, $\frac{1}{2}$	=	---	$\frac{1}{4}$, 2	=	---	---	Do.
	-do-	-do-	-do-	30	-do-	-do-	---	$\frac{1}{2}$, $\frac{3}{4}$	$\frac{1}{2}$, 2	---	$\frac{1}{2}$, $\frac{1}{2}$	=	---	---	Do.
	-do-	-do-	8.8	2.5	-do-	-do-	---	$\frac{1}{2}$, =	= 3, 3	---	$\frac{1}{2}$, $\frac{1}{2}$	=	---	---	Do.
	-do-	-do-	-do-	15	-do-	-do-	---	$\frac{1}{2}$, $\frac{3}{4}$	$\frac{1}{2}$, $\frac{1}{2}$	---	$\frac{1}{4}$, 1	$\frac{1}{2}$, 4	---	---	Do.
	-do-	-do-	-do-	30	-do-	-do-	---	$\frac{1}{2}$, $\frac{1}{2}$	$\frac{1}{2}$, 2	---	$\frac{1}{2}$, $\frac{1}{4}$	$\frac{1}{2}$, 2	---	---	Do.
	-do-	Outboard wing tip	7.0	10	-do-	-do-	---	$\frac{1}{2}$, $\frac{3}{4}$	$\frac{1}{2}$	---	1	1, $\frac{1}{2}$	---	---	---
	-do-	-do-	-do-	30	-do-	-do-	---	$\frac{1}{2}$, $\frac{1}{2}$	$\frac{1}{2}$, $\frac{1}{2}$	---	$\frac{1}{2}$, 1	1, $\frac{1}{4}$	---	---	---
	-do-	-do-	5.0	10	-do-	-do-	---	$\frac{3}{4}$, 1	$\frac{2}{4}$, $\frac{3}{2}$	---	$\frac{1}{2}$, > 3	=	---	---	---
	-do-	-do-	-do-	15	-do-	-do-	---	$\frac{3}{4}$, $\frac{1}{4}$	=	---	> $\frac{3}{2}$	=	---	---	---
	-do-	-do-	-do-	30	-do-	-do-	---	$\frac{1}{2}$, $\frac{1}{4}$	2, > 3	---	1, > 2	=	---	---	---
4	-do-	Outboard wing tip	4.0	19.50	-do-	E	---	---	3, $\frac{3}{2}$	---	---	---	---	---	25-percent semispan slats extended
	-do-	-do-	-do-	9.75	-do-	-do-	---	---	$\frac{3}{2}$, 4	---	---	---	---	---	Do.
	-do-	-do-	5.33	19.50	-do-	-do-	---	---	$\frac{2}{4}$, $\frac{3}{2}$	---	---	---	---	---	Do.
	-do-	-do-	-do-	9.75	-do-	-do-	---	---	$\frac{2}{4}$, $\frac{3}{2}$	---	---	---	---	---	Do.
	-do-	-do-	6.67	19.50	-do-	-do-	---	---	$\frac{1}{4}$, 4	---	---	---	---	---	Do.
	-do-	-do-	-do-	9.75	-do-	-do-	---	---	$\frac{3}{4}$, $\frac{1}{4}$	---	---	---	---	---	Do.
	-do-	-do-	8.0	-do-	-do-	-do-	---	---	$\frac{1}{4}$	---	---	---	---	---	Do.
	Inverted	-do-	6.67	19.50	-do-	-do-	---	$\frac{1}{4}$, $\frac{1}{4}$	---	---	---	---	---	---	Do.
	-do-	-do-	8.0	19.50	-do-	-do-	---	---	1, $\frac{1}{2}$	---	---	---	---	---	Do.
	Erect	-do-	5.60	-do-	-do-	D	---	---	4, > $\frac{1}{2}$	---	---	---	---	---	Do.
	-do-	-do-	6.67	-do-	-do-	-do-	---	$\frac{1}{2}$, $\frac{2}{4}$	$\frac{1}{2}$, $\frac{2}{4}$	---	---	---	---	---	Do.
	Inverted	-do-	-do-	-do-	-do-	-do-	---	---	3	---	---	---	---	---	Do.
	-do-	-do-	8.0	-do-	-do-	-do-	---	---	$\frac{2}{4}$, $\frac{2}{4}$	---	$\frac{1}{4}$	---	---	---	Do.
	5	Erect	-do-	4.24	25	0.83	A	---	$\frac{1}{2}$	---	1	---	---	---	---
-do-		Parachutes at both wing tips	4.39	-do-	-do-	-do-	---	---	---	1, 2	---	---	---	---	Two parachutes opened simultaneously
-do-		-do-	7.31	-do-	0.70	-do-	---	---	$\frac{1}{2}$, > $\frac{2}{4}$	---	---	---	---	---	---
-do-		-do-	8.77	-do-	-do-	-do-	---	$\frac{1}{4}$, $\frac{1}{2}$	---	$\frac{1}{4}$, $\frac{3}{4}$	---	---	---	---	---
6	Erect	Tail cone	8	13.4	0.7	A	---	---	$\frac{2}{4}$, $\frac{2}{4}$	---	---	---	---	---	---
	-do-	-do-	10	-do-	-do-	-do-	---	---	1, $\frac{1}{2}$	---	---	---	---	---	---
	-do-	-do-	11.7	-do-	-do-	-do-	---	---	$\frac{1}{4}$, 1	---	---	---	---	---	---
	-do-	Outboard wing tip	3.3	7.9	-do-	-do-	---	---	> 8, > 9	---	---	---	---	---	---
	-do-	-do-	5.0	-do-	-do-	-do-	---	---	$\frac{2}{4}$, $\frac{2}{4}$	---	---	---	---	---	---
	-do-	-do-	6.2	-do-	-do-	-do-	---	---	$\frac{1}{4}$, $\frac{1}{4}$	---	---	---	---	---	---

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CHART 14.- RESULTS OF SPIN-RECOVERY PARACHUTE TESTS FOR MODELS - Concluded

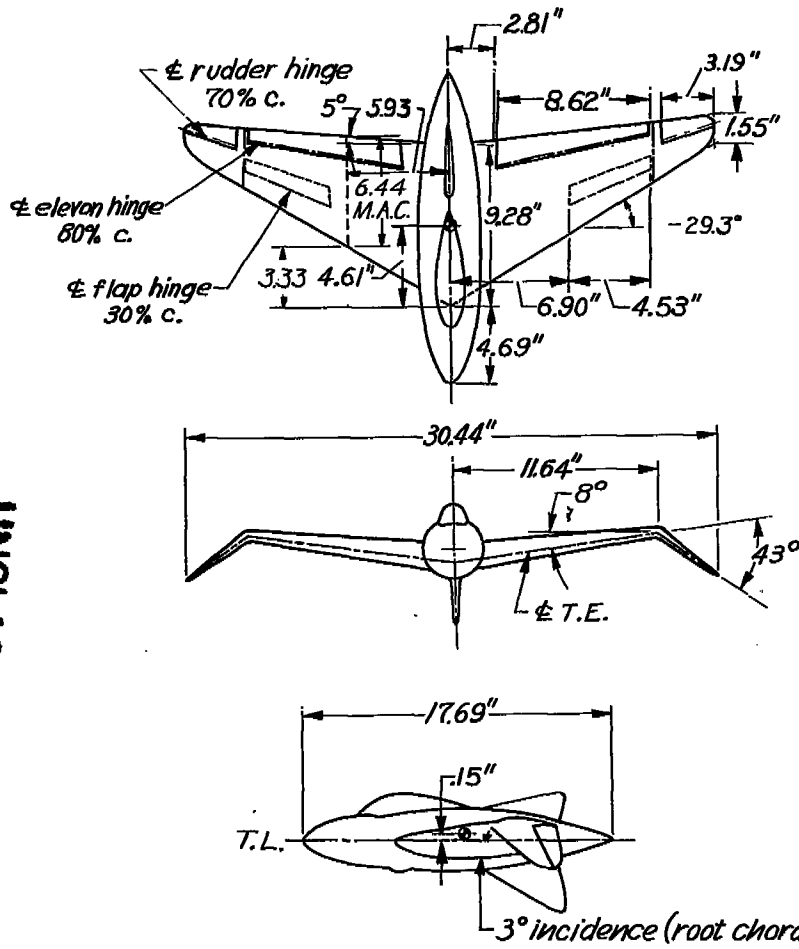
Model	Attitude	Parachute location	Parachute diameter (ft)	Bowline length (ft)	Drag coefficient	Loading	Turns for recovery										Remarks
							Elevator										
							U		2/3U		N		D				
							Ailerons										
							Age- inst	Neu- tral	With	1/3 age- inst	1/3 with	Neu- tral	With	Age- inst	Neu- tral		
8	Erect	Tail cone	3.6	27	0.70	A	----	$\frac{1}{2}$	----	----	----	----	----	----	----	$2\frac{1}{2}, 2\frac{3}{4}$	x/E = 0.14
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	$\frac{3}{4}$	1	----	----	----	----	----	----	$2\frac{1}{2}, 2\frac{3}{4}$	Do.
	-do-	-----do-----	4.5	-do-	-do-	-do-	----	$\frac{3}{4}$	1	----	----	----	----	----	----	$1\frac{1}{4}, 1\frac{1}{2}$	Do.
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	----	----	----	----	----	----	----	----	$1\frac{1}{4}, 1\frac{1}{2}$	Do.
	-do-	-----do-----	5.5	-do-	-do-	G	----	1, 2	----	----	----	----	----	----	----	----	Do.
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	----	----	----	----	----	----	----	----	1, $2\frac{3}{4}$	Do.
	-do-	-----do-----	7.1	-do-	-do-	-do-	----	$\frac{1}{4}$	$\frac{3}{4}$	----	----	----	----	----	----	----	Do.
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	----	----	----	----	----	----	----	----	$1\frac{1}{4}, 2$	Do.
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	$\frac{1}{2}$	----	----	----	----	----	----	----	----	x/E = 0.19
	-do-	-----do-----	-do-	13.5	-do-	-do-	----	$\frac{1}{4}$	----	----	----	----	----	----	----	----	x/E = 0.14
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	----	----	----	----	----	----	----	----	1, $1\frac{3}{4}$	Do.
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	----	----	----	----	----	----	----	----	----	x/E = 0.19
	-do-	-----do-----	-do-	-do-	-do-	-do-	----	----	----	----	----	----	----	----	----	$\frac{1}{4}, \frac{3}{4}$	Do.
	-do-	Arresting gear mast (aft)	13.3	30	0.70	A	----	----	----	2	$2\frac{1}{2}, 3\frac{1}{4}$	----	=	----	----	>3	-----
10	-do-	-----do-----	16.0	30	-do-	-do-	>7	----	----	$1\frac{3}{4}, 2, 2\frac{3}{4}$	$2\frac{1}{2}, 3\frac{1}{4}$	----	2, =	----	----	-----	
	-do-	-----do-----	-do-	23	-do-	-do-	----	----	----	$1\frac{3}{4}, 2, 2\frac{3}{4}$	$2\frac{1}{2}, 3\frac{1}{4}$	----	=	----	----	-----	
	-do-	-----do-----	-do-	15	-do-	-do-	>8	----	----	----	----	----	=	----	----	-----	
	-do-	-----do-----	20	30	-do-	-do-	----	----	----	----	----	----	4, =	----	----	-----	
	-do-	-----do-----	20	15	-do-	-do-	----	----	----	----	----	----	3, 4	----	----	-----	
	-do-	Arresting gear mast and outboard end of wing	b6.9 c13.3	30 Q	-do-	-do-	----	----	----	----	$2\frac{3}{4}, 3\frac{1}{4}$	----	----	----	----	Two parachutes - wing tip parachute attached at c/4	
	-do-	-----do-----	b11.7 c6.9	-do-	-do-	-do-	----	----	----	----	3, $3\frac{3}{4}$	----	----	----	----	Do.	
	-do-	-----do-----	b-do c8.0	-do-	-do-	-do-	----	----	----	----	$2\frac{1}{2}, 3\frac{1}{4}$	----	----	----	----	Do.	
	-do-	-----do-----	b-do c10.6	-do-	-do-	-do-	----	----	----	----	> $2\frac{1}{2}$	----	----	----	----	Do.	
	-do-	-----do-----	b13.3 c6.9	-do-	-do-	-do-	----	----	----	----	$1\frac{3}{4}, 2\frac{3}{4}$	----	----	----	----	Do.	
	-do-	-----do-----	b-do c-do-	-do-	-do-	-do-	----	----	----	----	$1\frac{1}{2}, 1\frac{3}{4}$	----	----	----	----	Do.	
	-do-	-----do-----	b-do c8.0	-do-	-do-	-do-	----	----	----	----	1, $1\frac{1}{4}$	----	----	----	----	Do.	
	-do-	-----do-----	b-do c-do-	-do-	-do-	-do-	----	----	----	1, $1\frac{3}{4}$	$1\frac{1}{4}, 1\frac{1}{2}$	----	$1\frac{1}{2}, 8$	----	----	Do.	
	-do-	-----do-----	b-do c11.2	-do-	-do-	-do-	----	----	----	----	1, 2	----	----	----	----	Do.	

^a Visual estimate.^b Attached to arresting gear mast.^c Attached to outboard wing tip at the c/4 line.~~CONFIDENTIAL~~

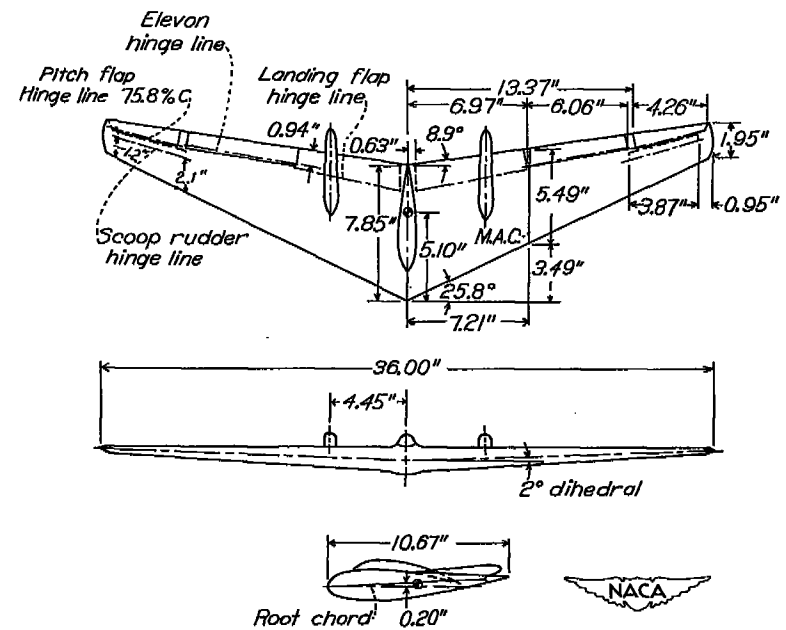
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(a) Model 1.

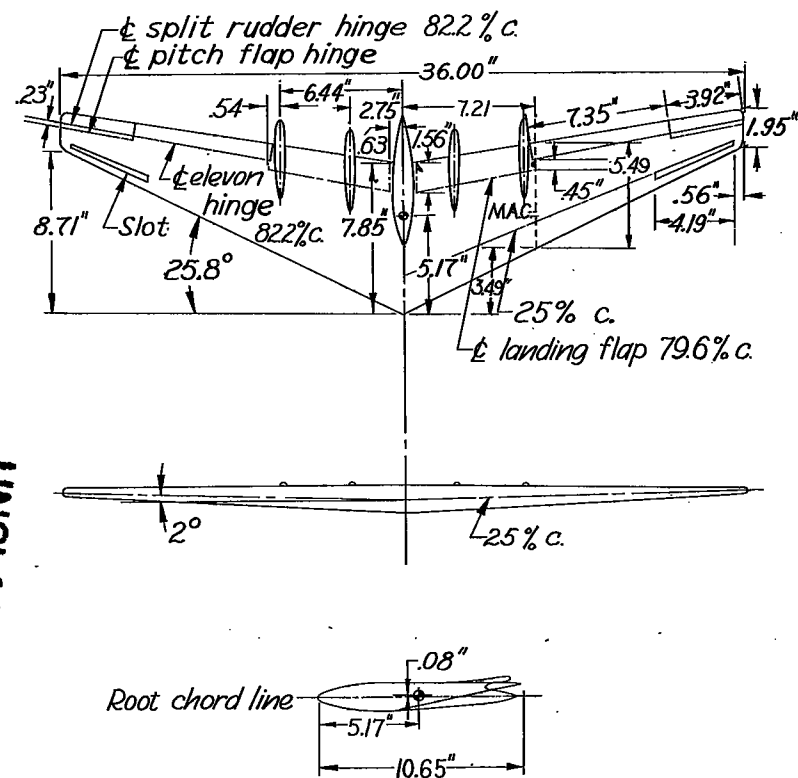


(b) Model 2.

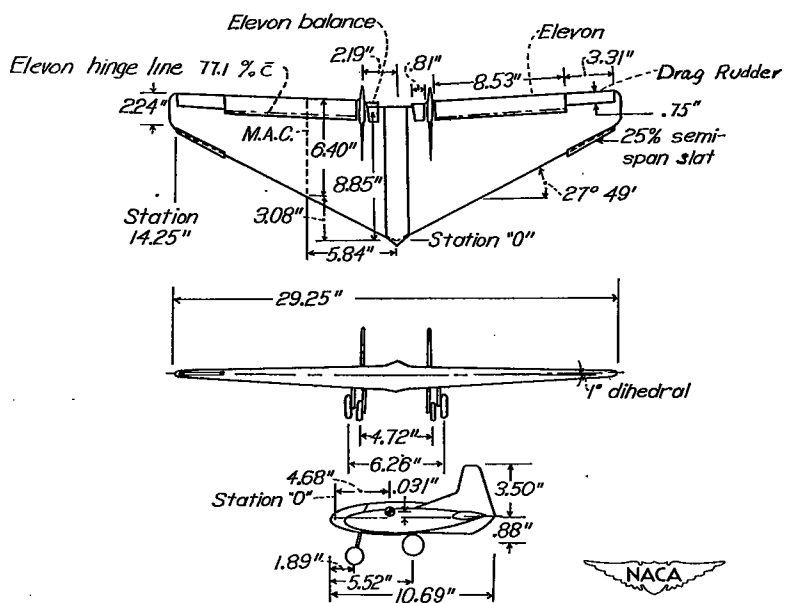
Figure 1.- Three-view drawings of models as tested.

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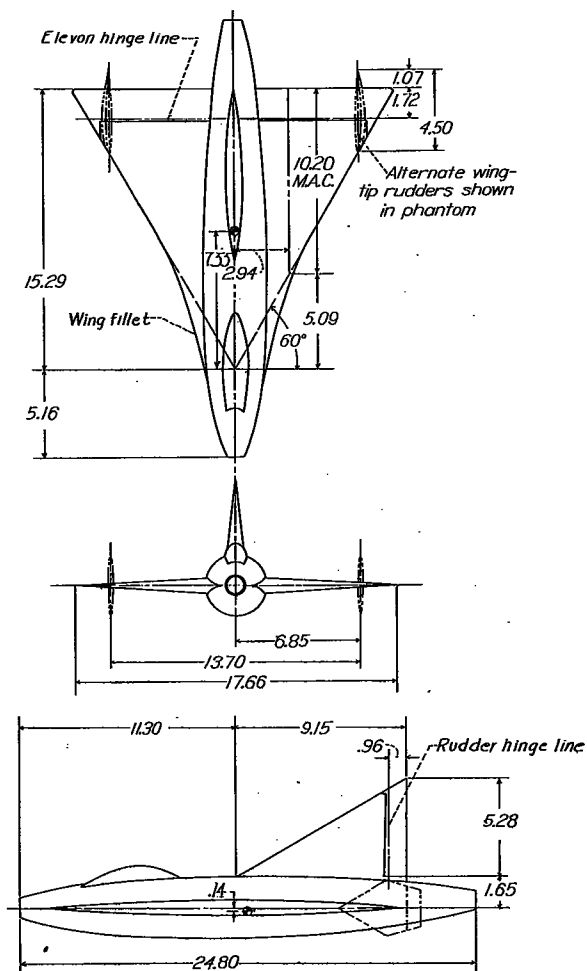
(c) Model 3.



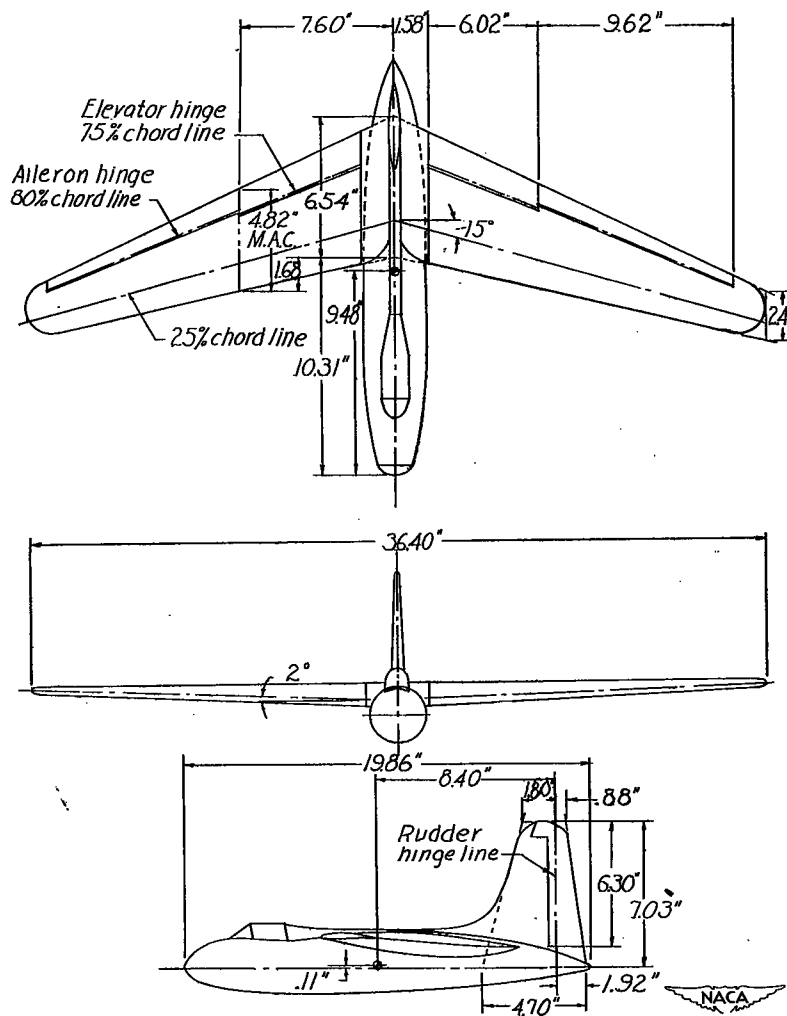
(d) Model 4.

Figure 1.- Continued.

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(g) Model 7.

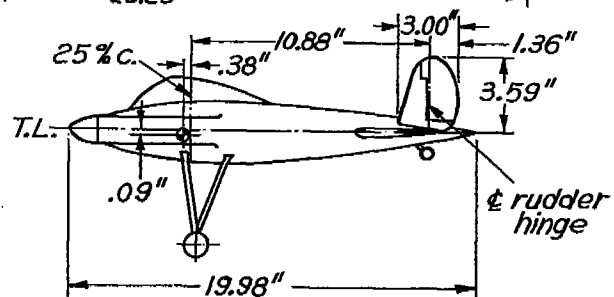
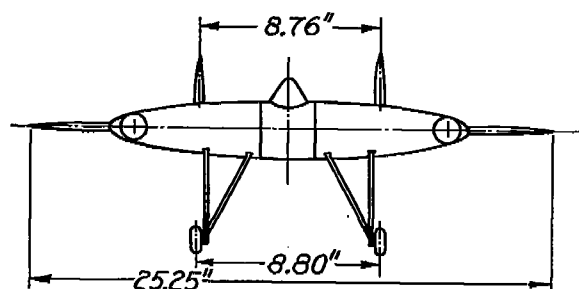
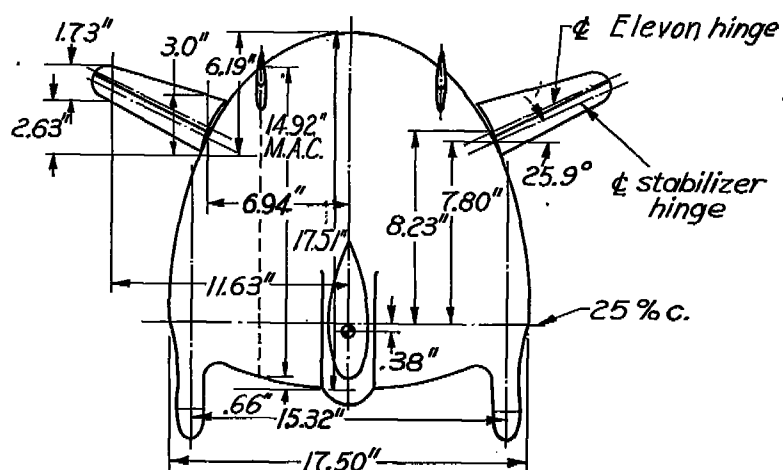


(h) Model 8.

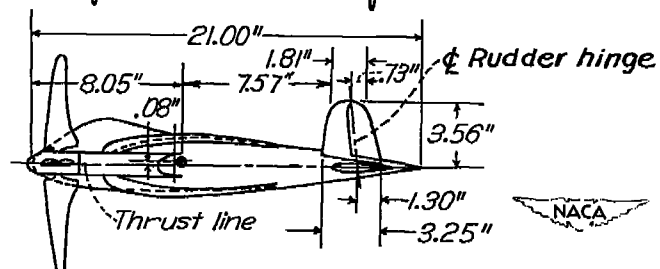
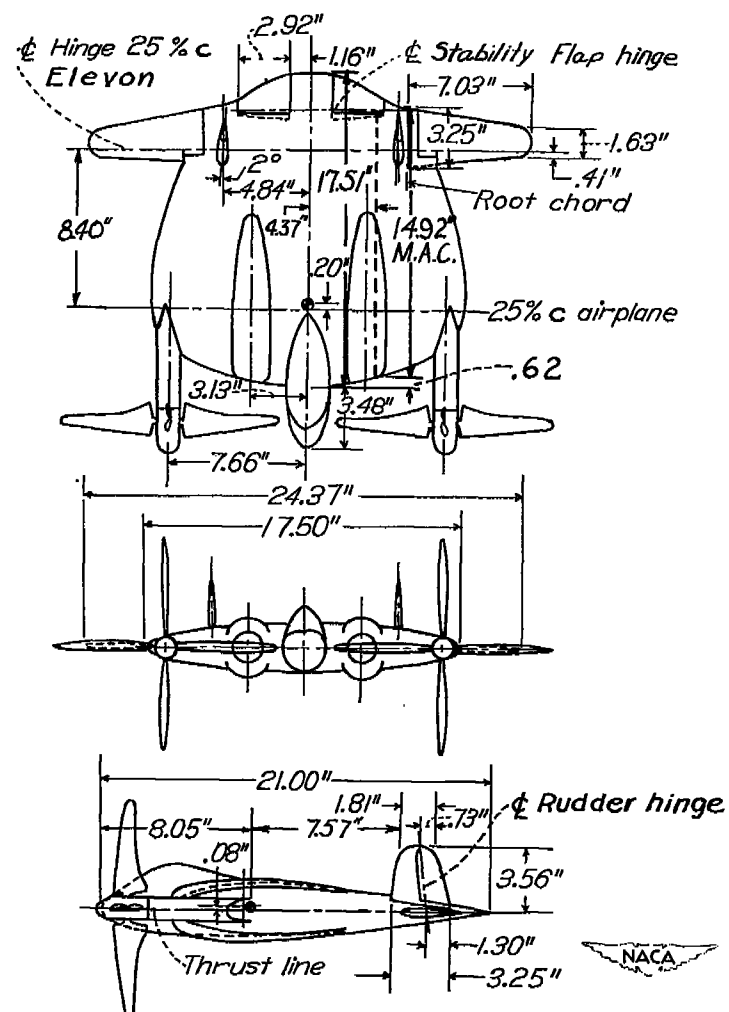
Figure 1.- Continued.

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(i) Model 9.

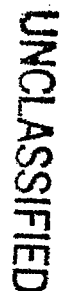


(j) Model 10.

Figure 1.- Continued.

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(k) Model 11.

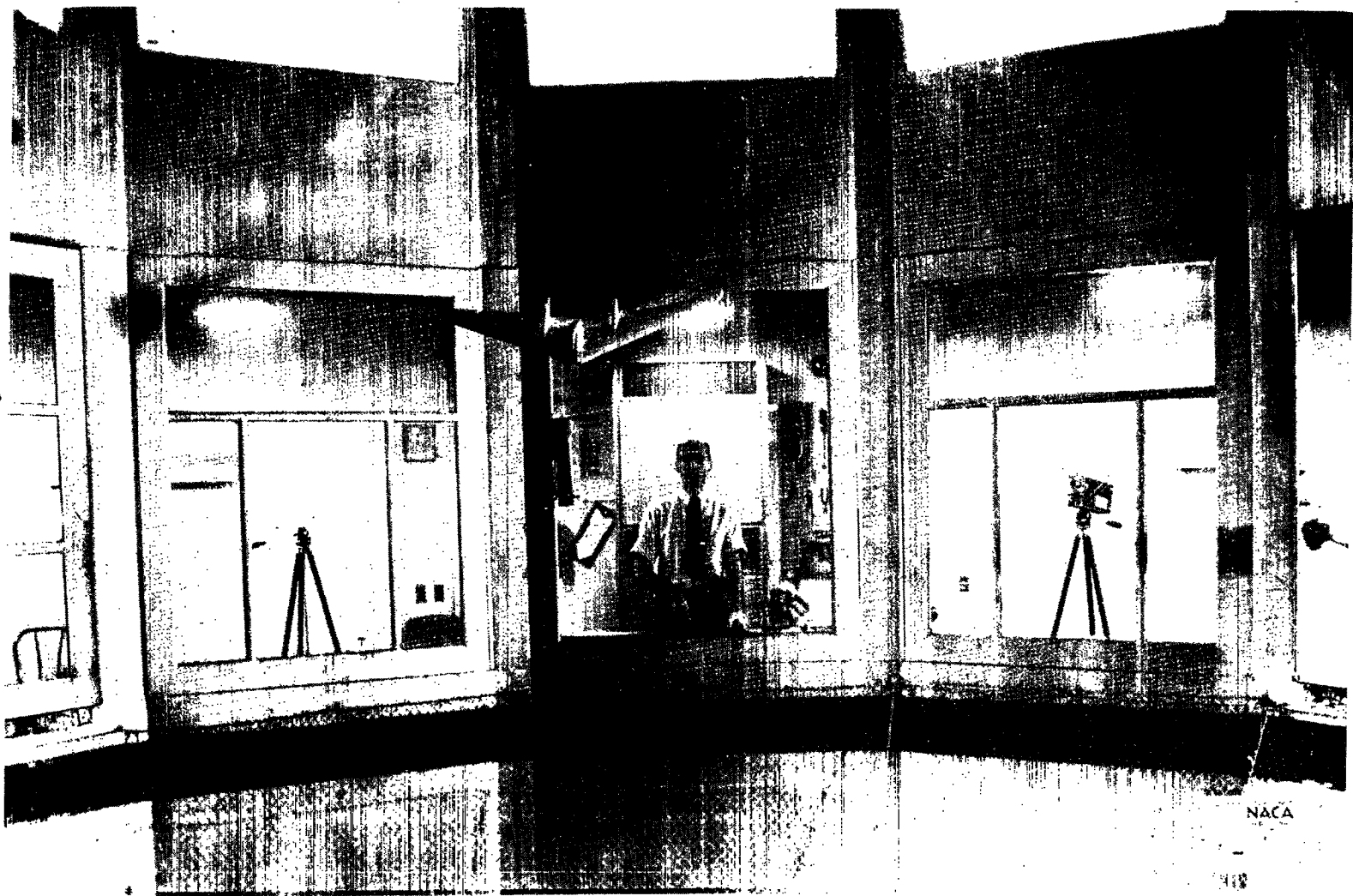


(2) Model 12.

Figure 1.- Concluded.

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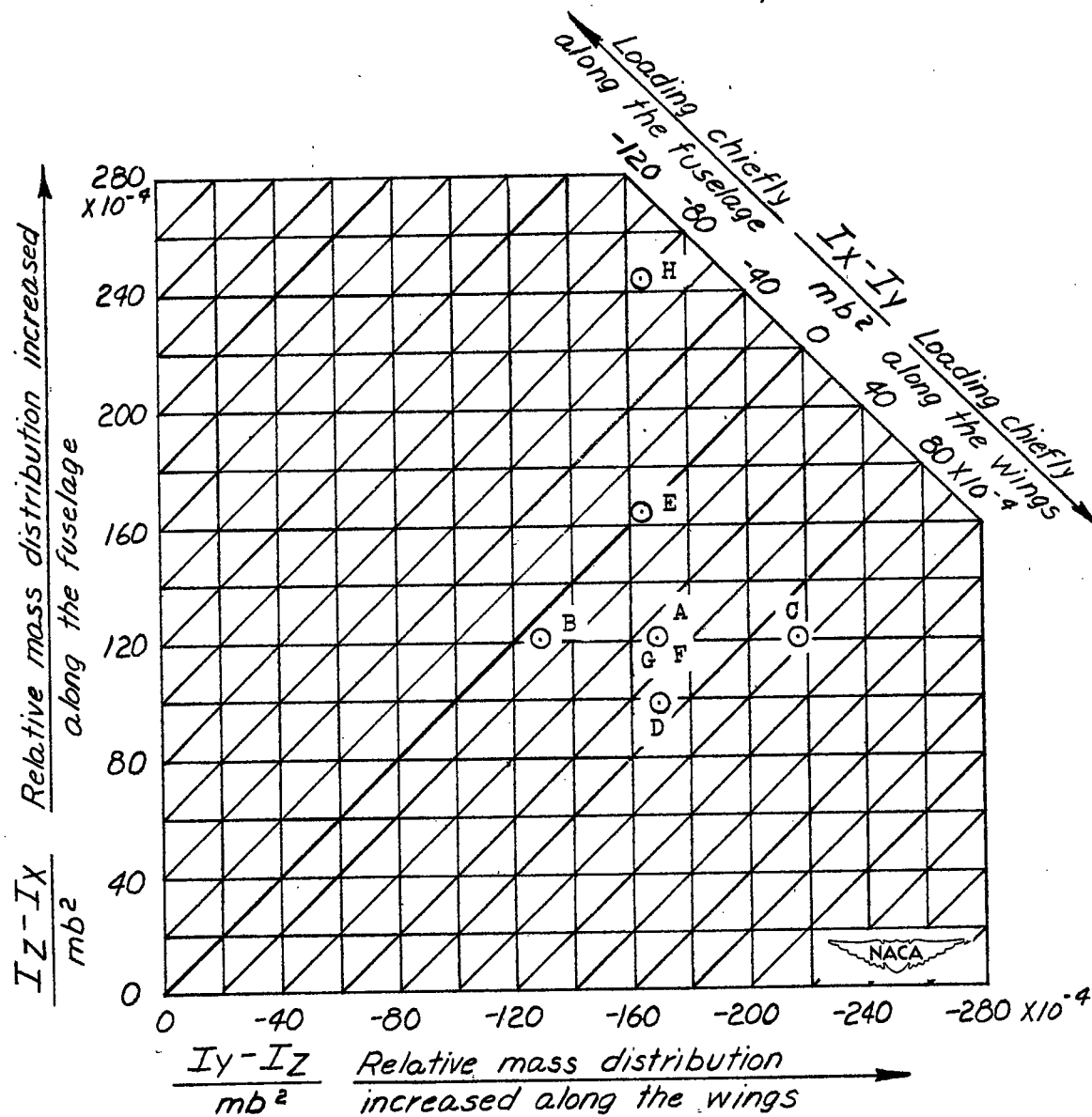


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Figure 2.- Photograph of model 2 spinning in the Langley 20-foot free-spinning tunnel.

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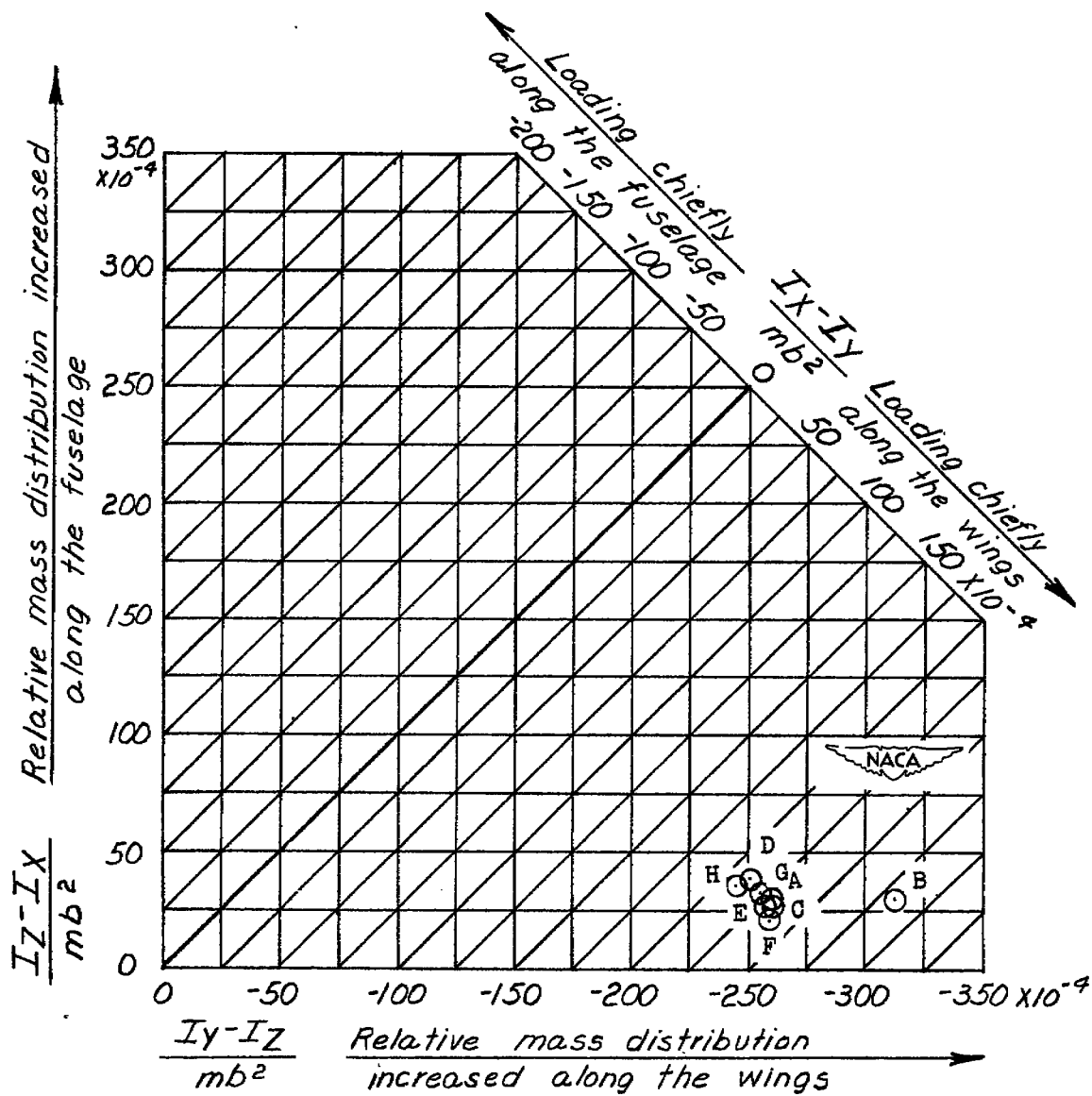
(a) Model 1.

Figure 3.- Mass parameters for loadings tested on models. (Loadings found in table II.)

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(b) Model 2.

Figure 3.- Continued.

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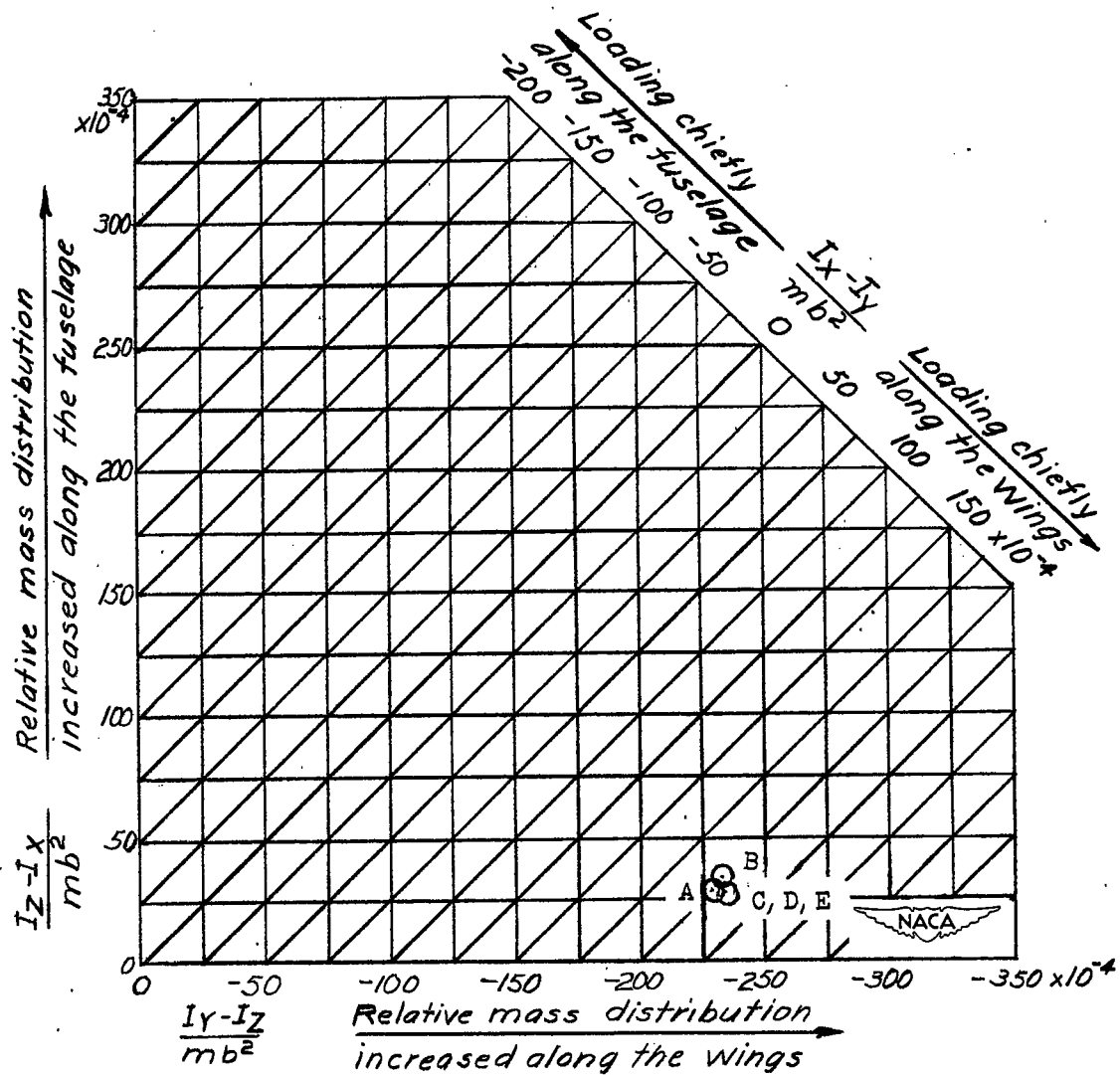
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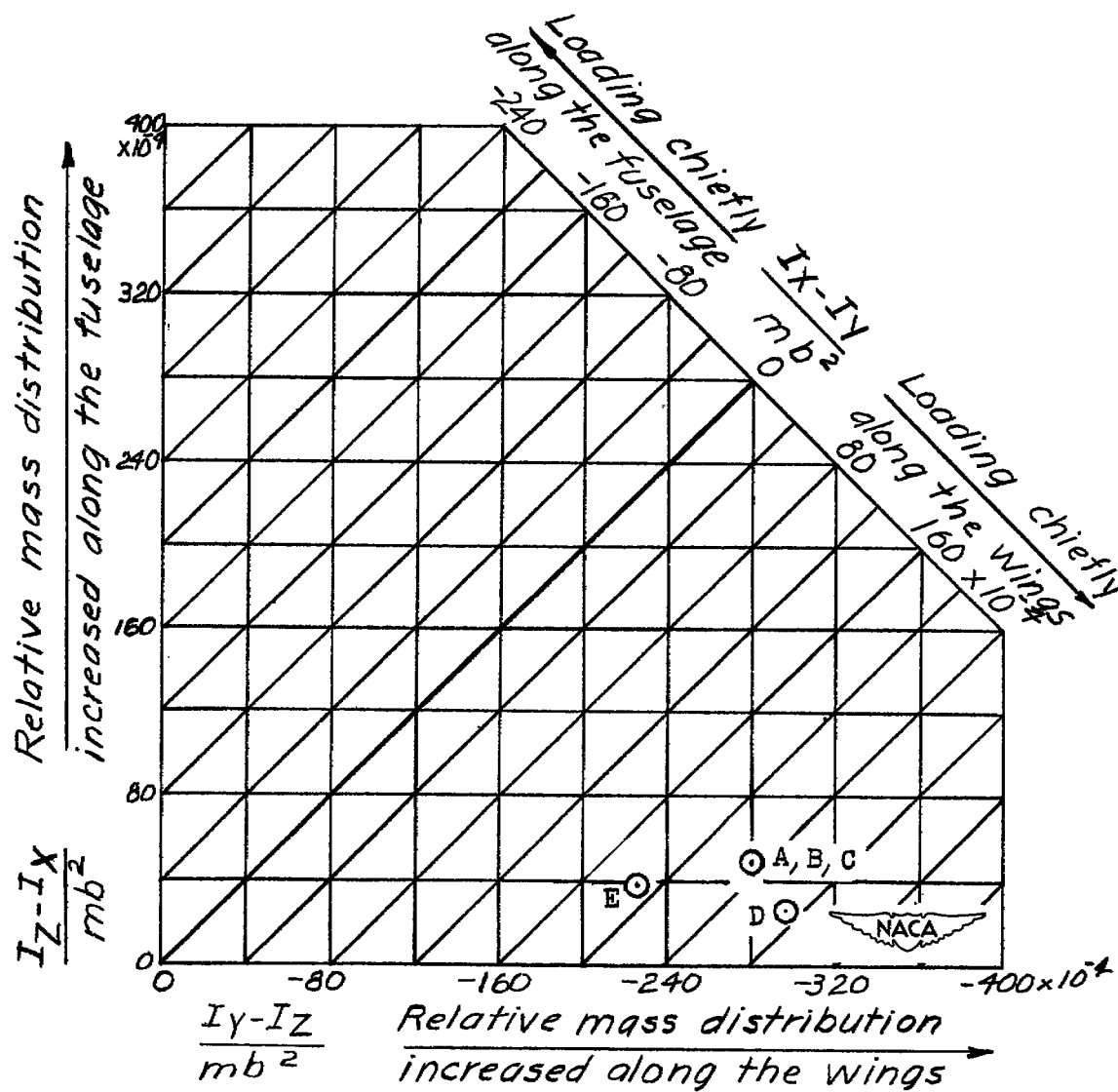


(c) Model 3.

Figure 3.- Continued.

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(d) Model 4.

Figure 3.- Continued.

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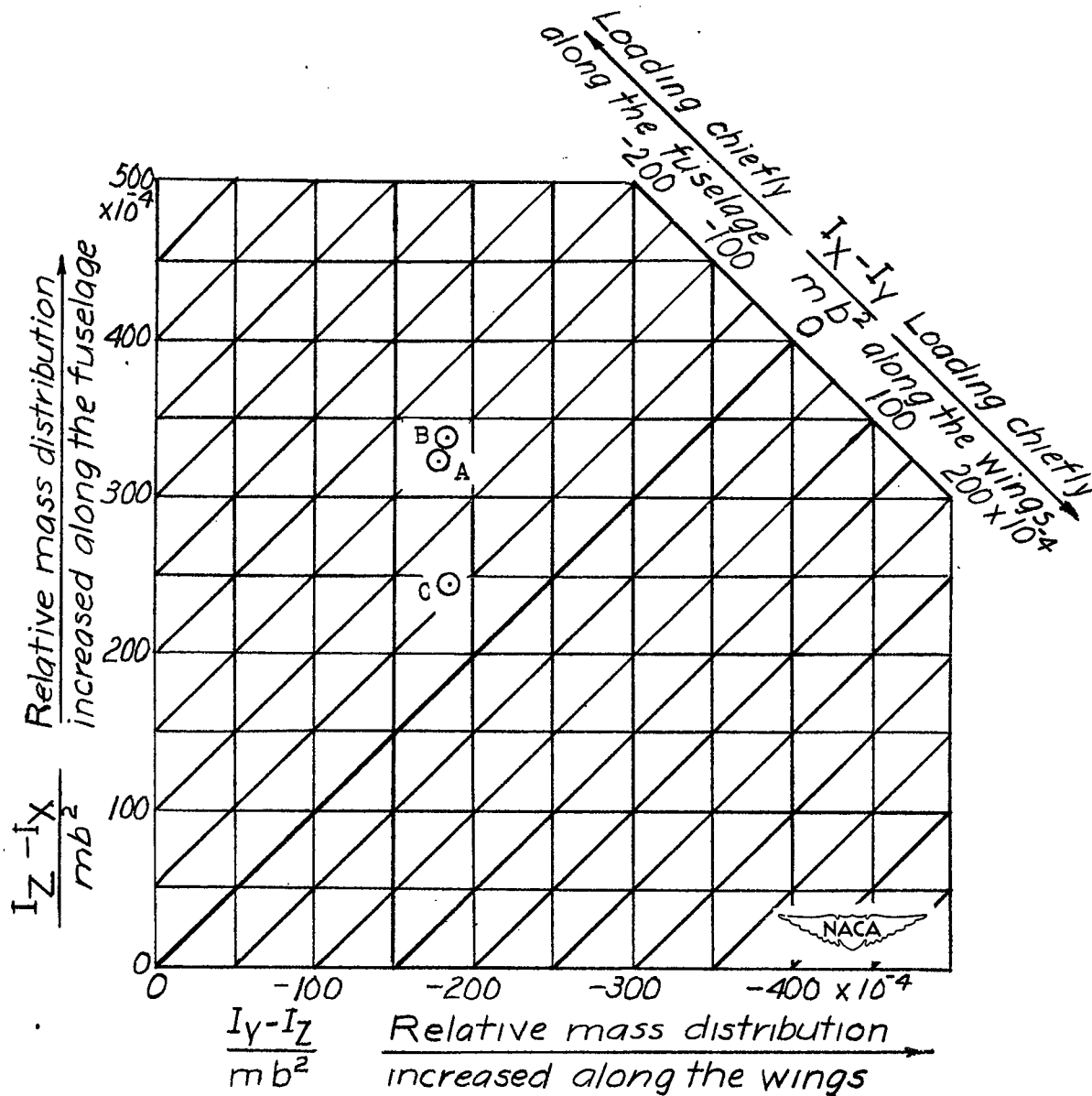
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(e) Model 5.

Figure 3.- Continued.

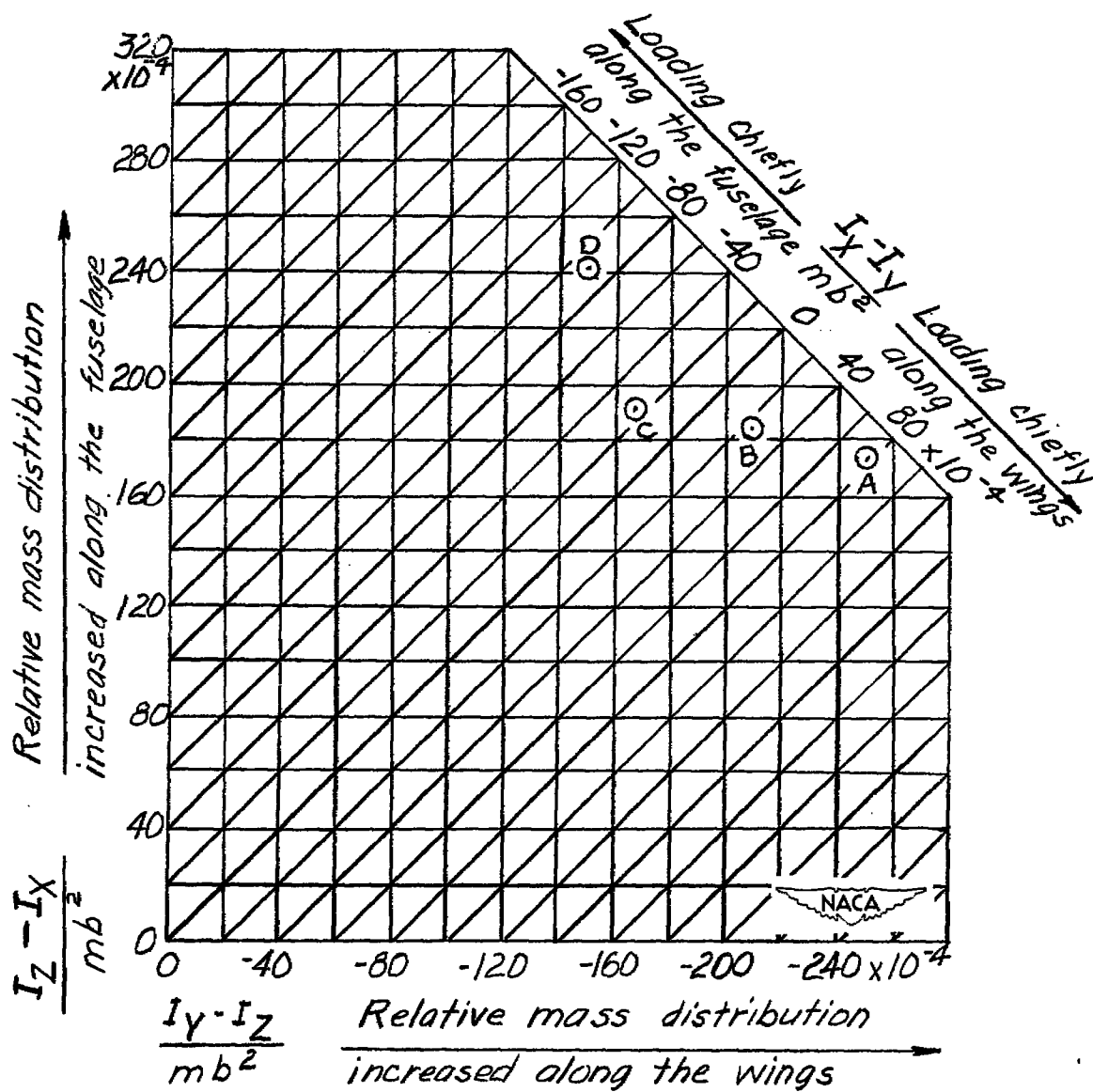
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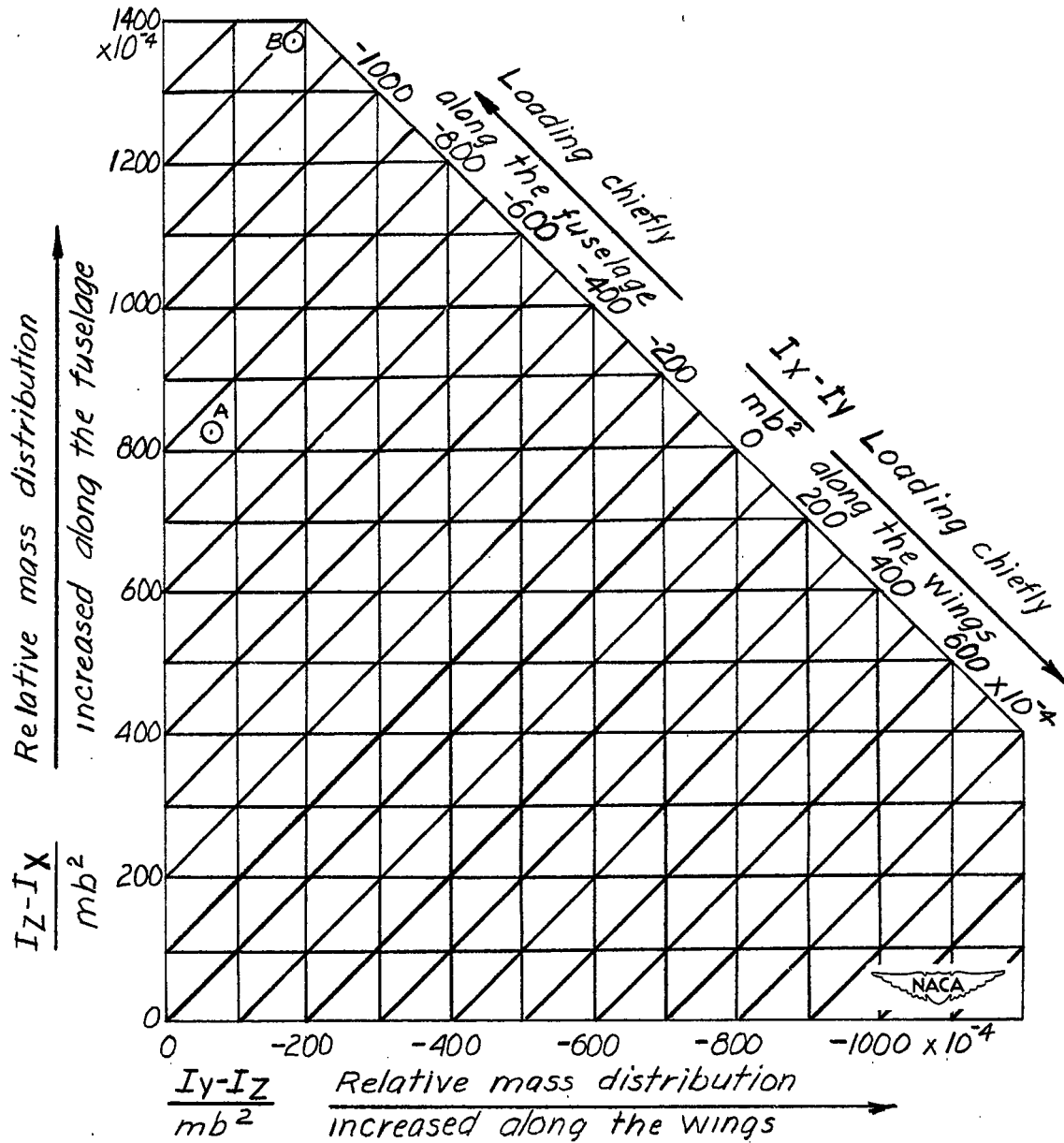


(f) Model 6.

Figure 3.- Continued.

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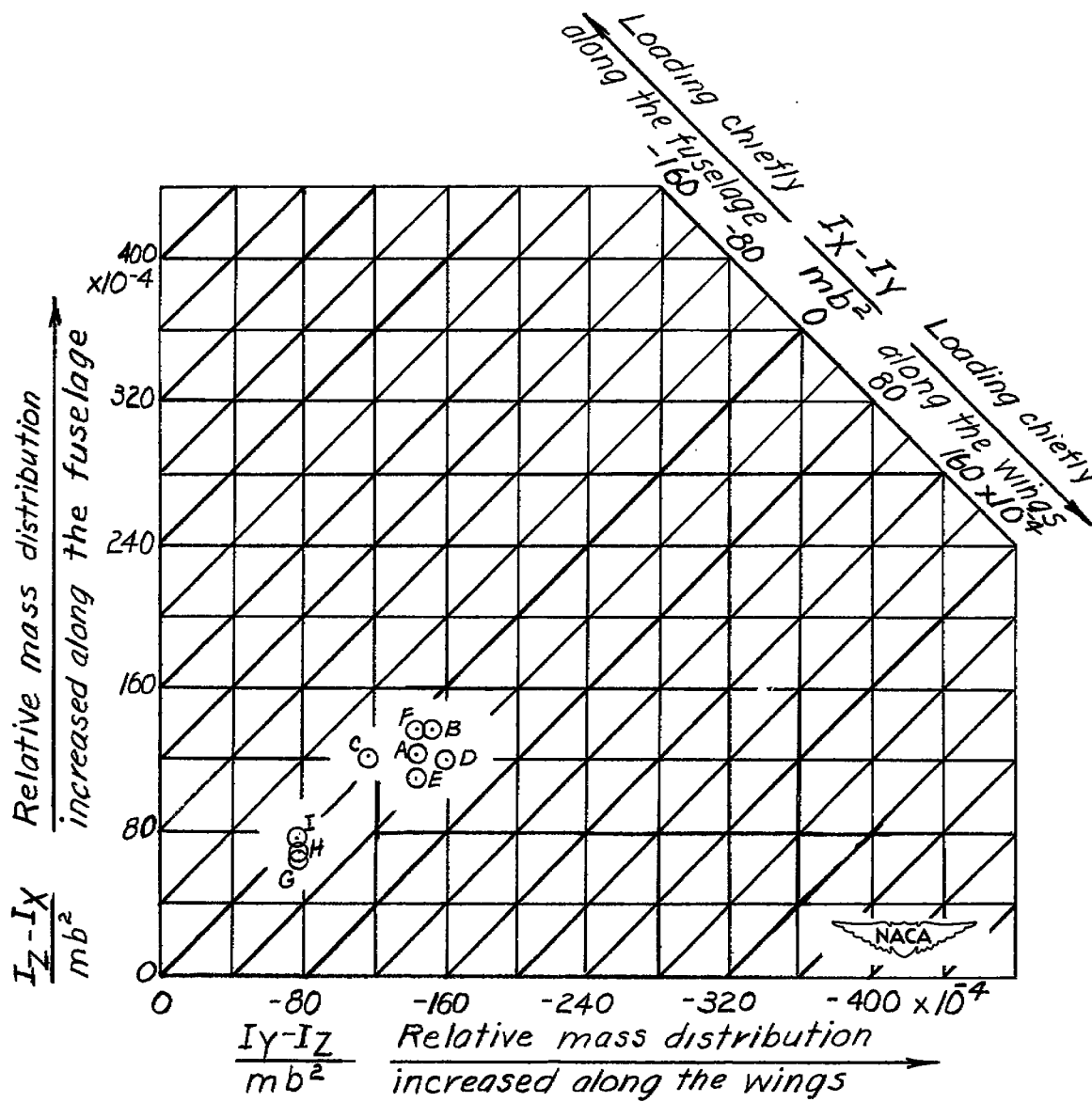
(g) Model 7.

Figure 3.- Continued.

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(h) Model 8.

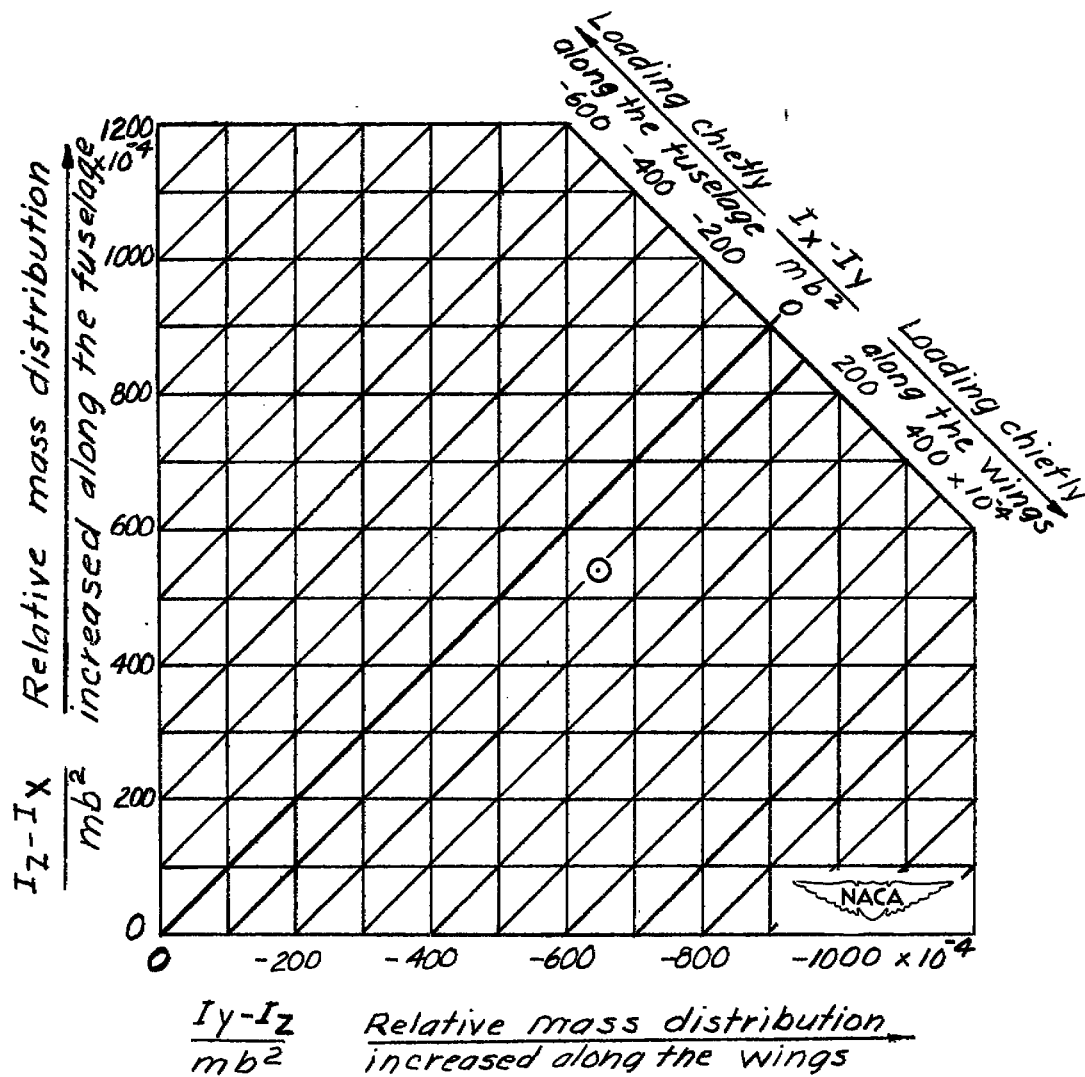
Figure 3.- Continued.

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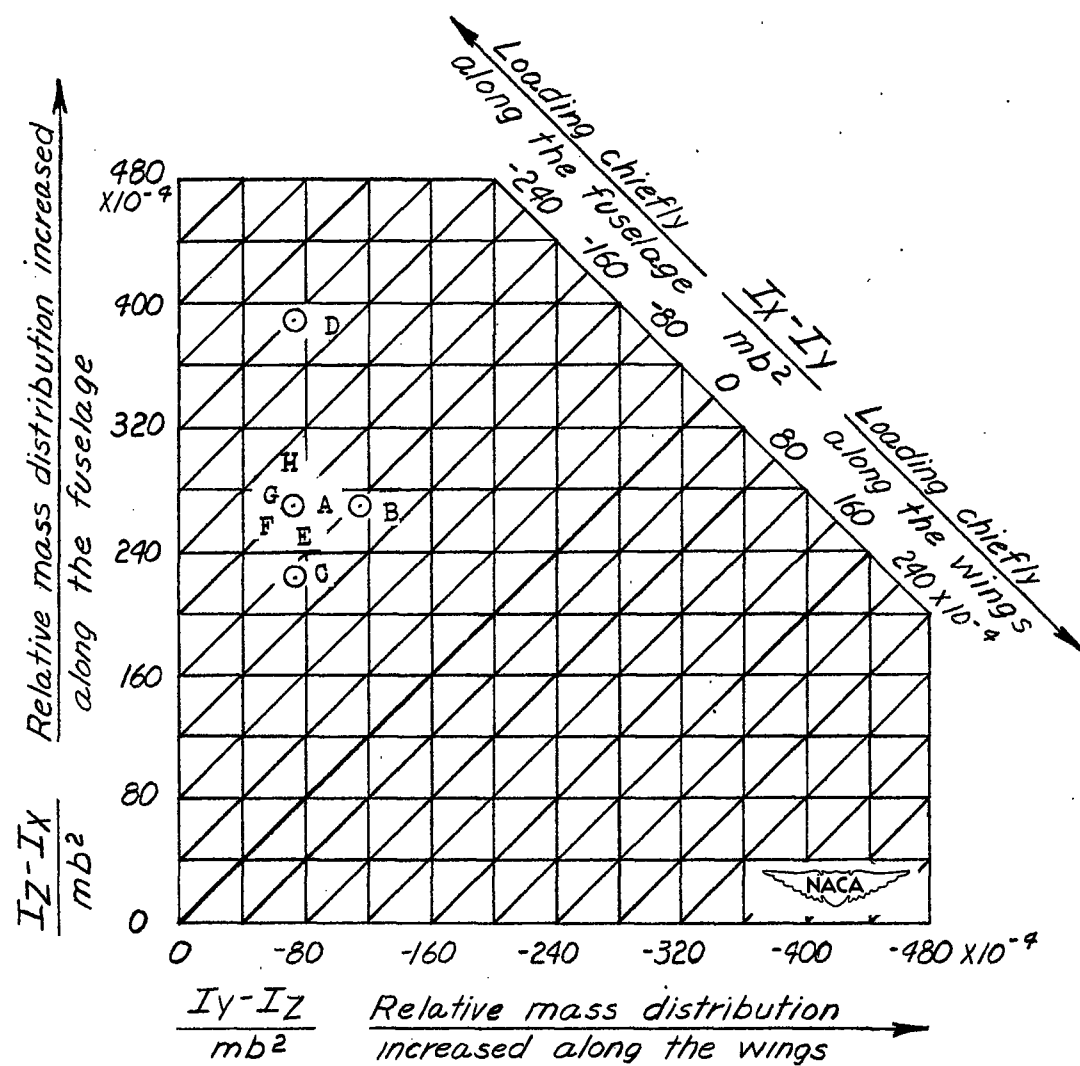


(j) Model 10.

Figure 3.- Continued.

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(k) Model 11.

Figure 3.- Continued.

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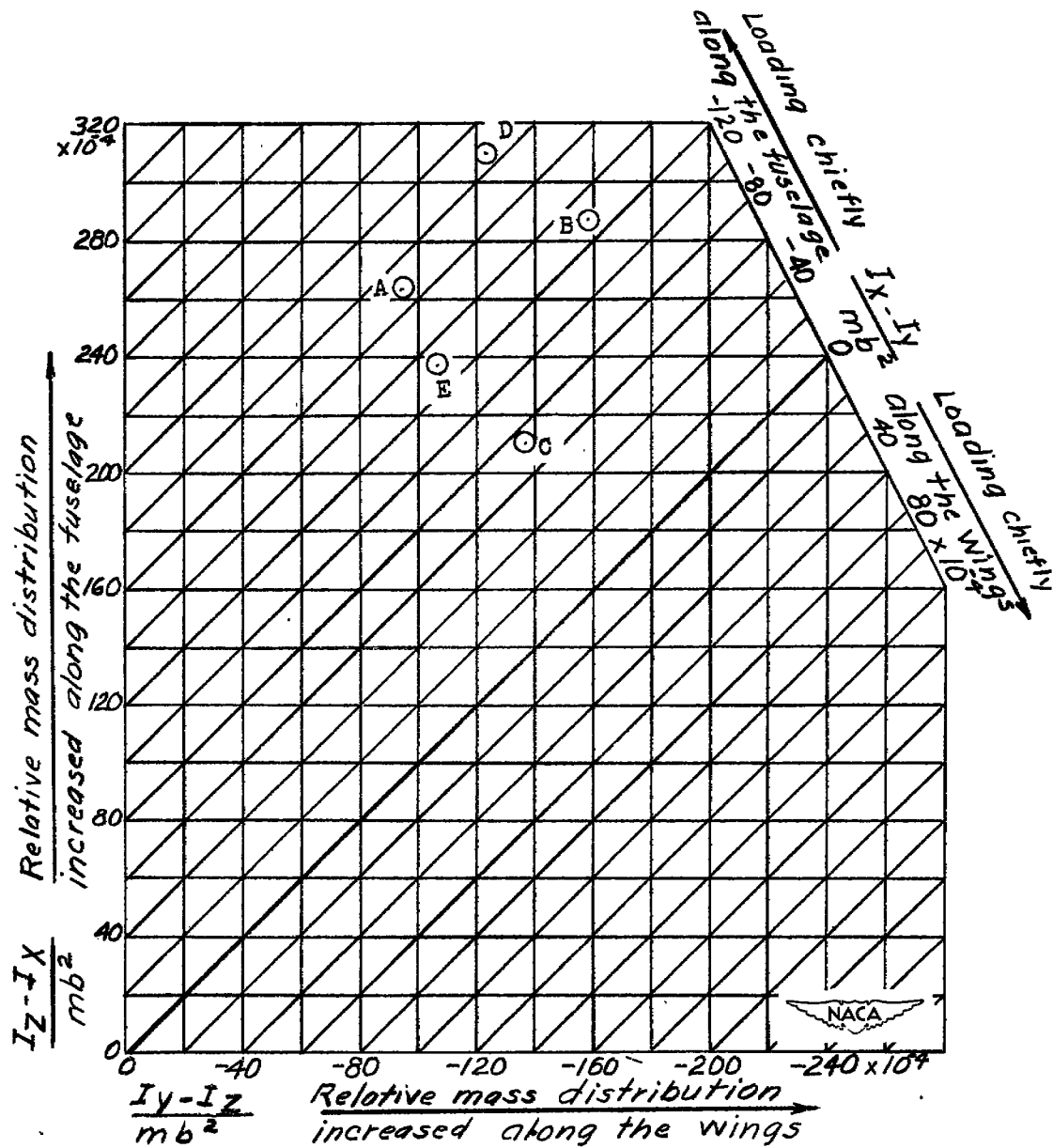
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(2) Model 12.

Figure 3.- Concluded.

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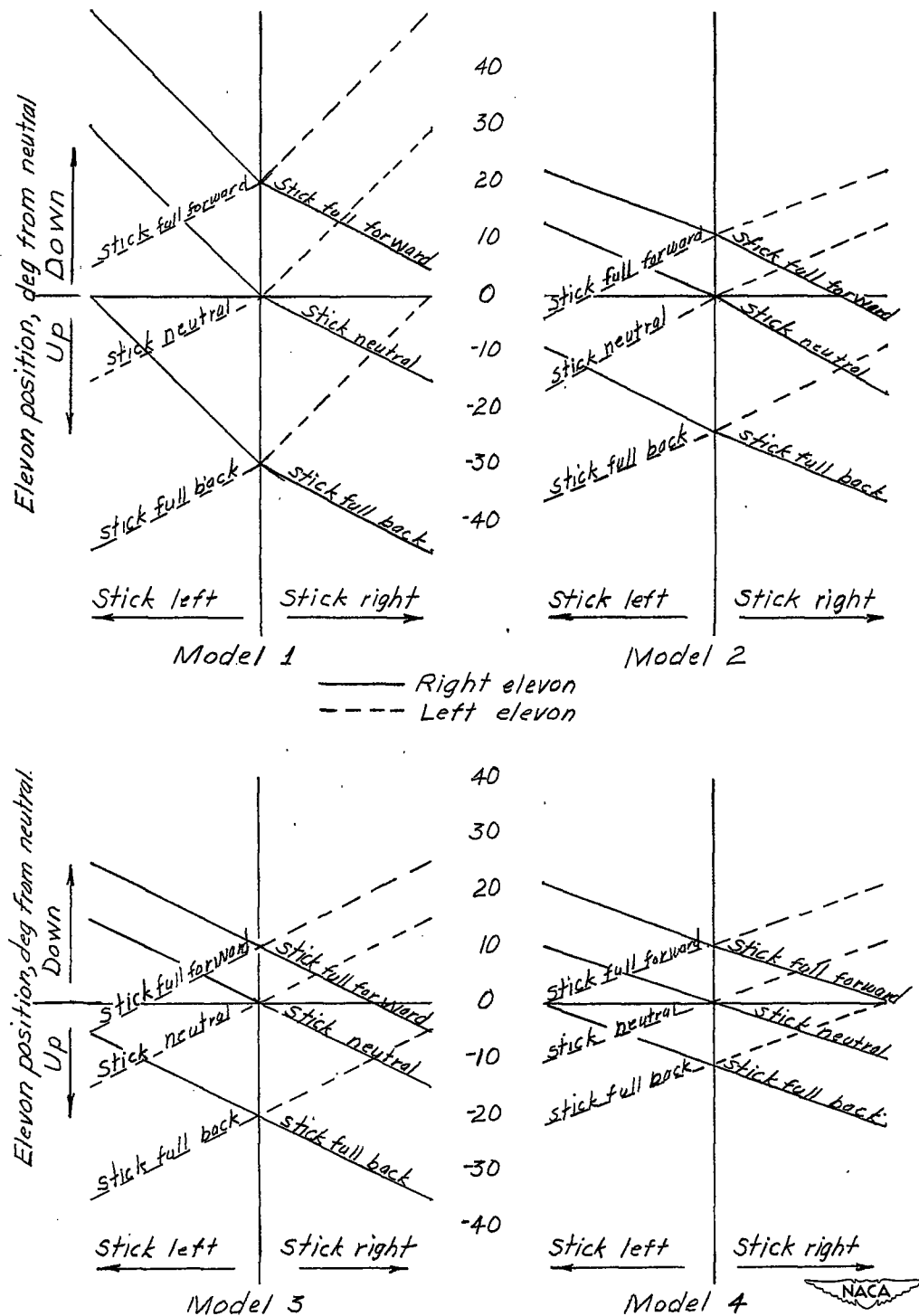


Figure 4.- Combination elevator-aileron (elevon) deflections for the models tested.

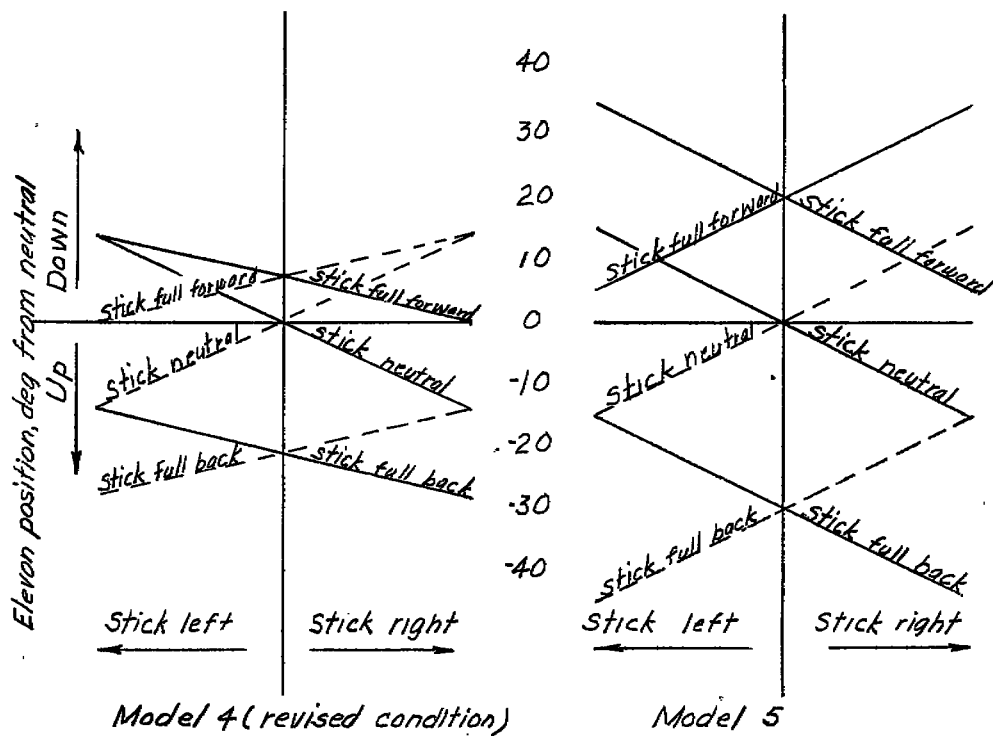
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———— Right elevon
 - - - - Left elevon

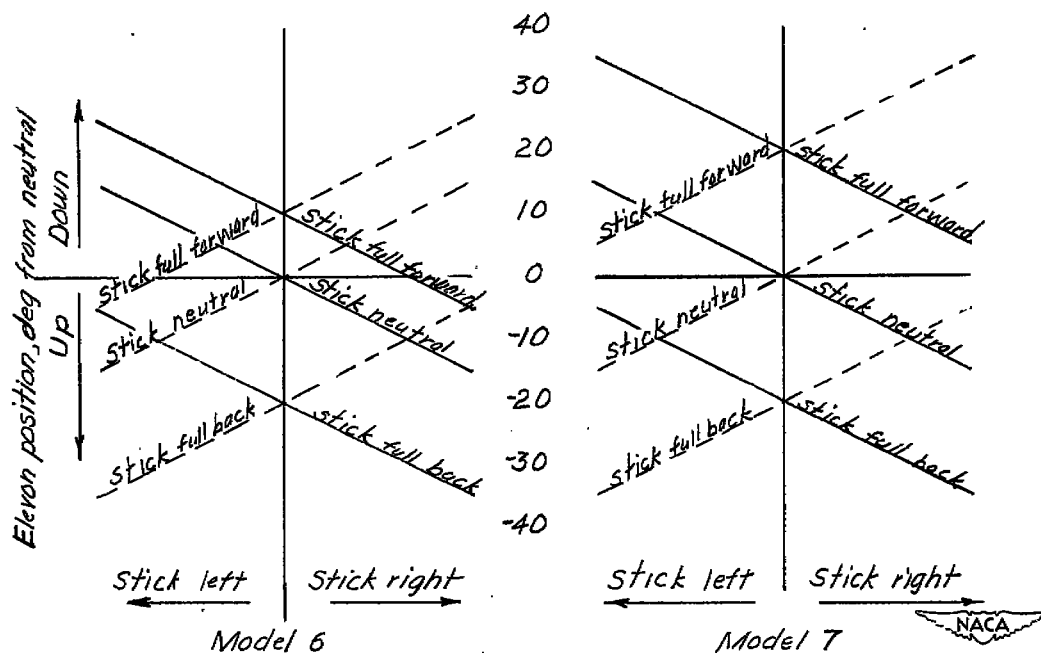


Figure 4.- Continued.

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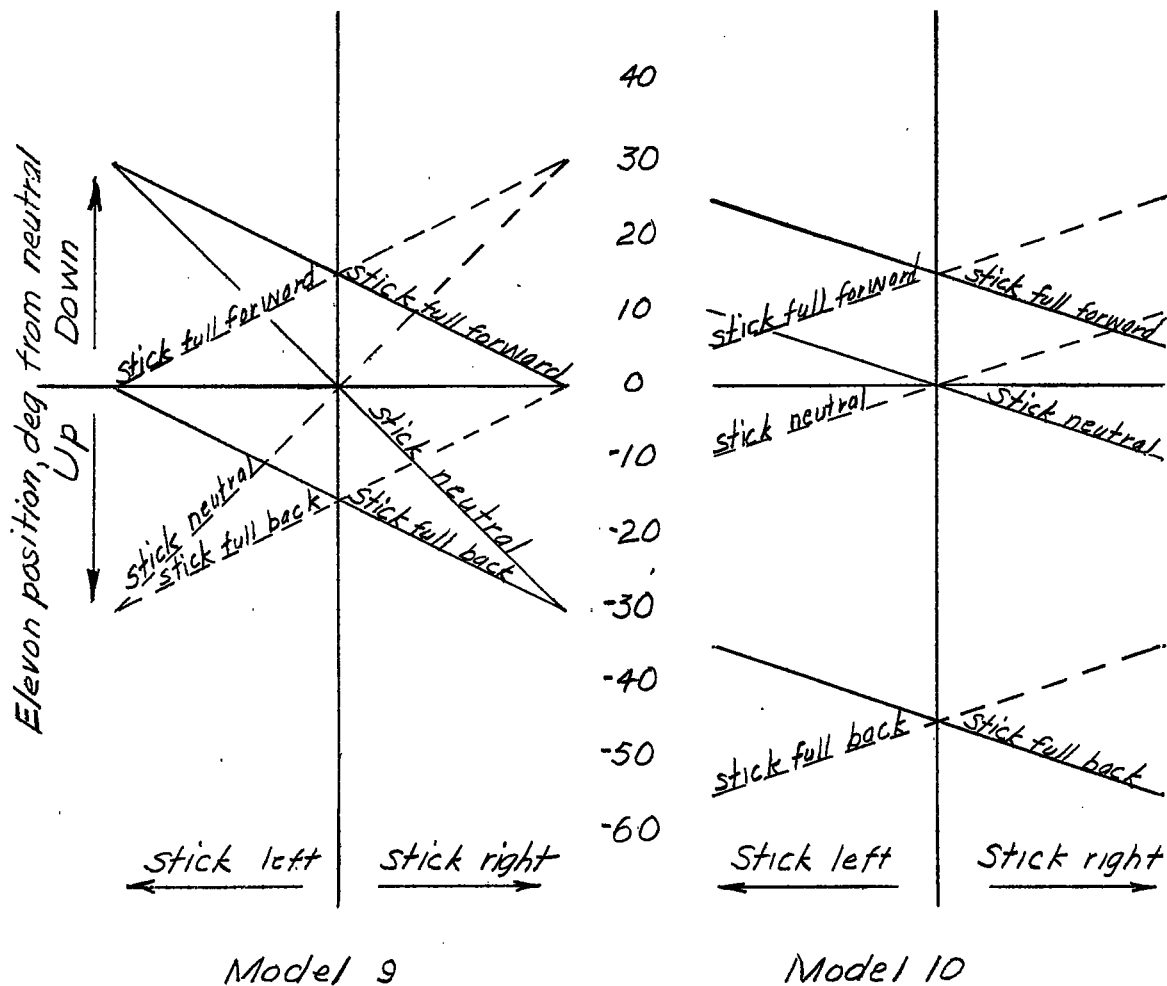
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—— Right elevon
 ---- Left elevon



Figure 4.- Concluded.

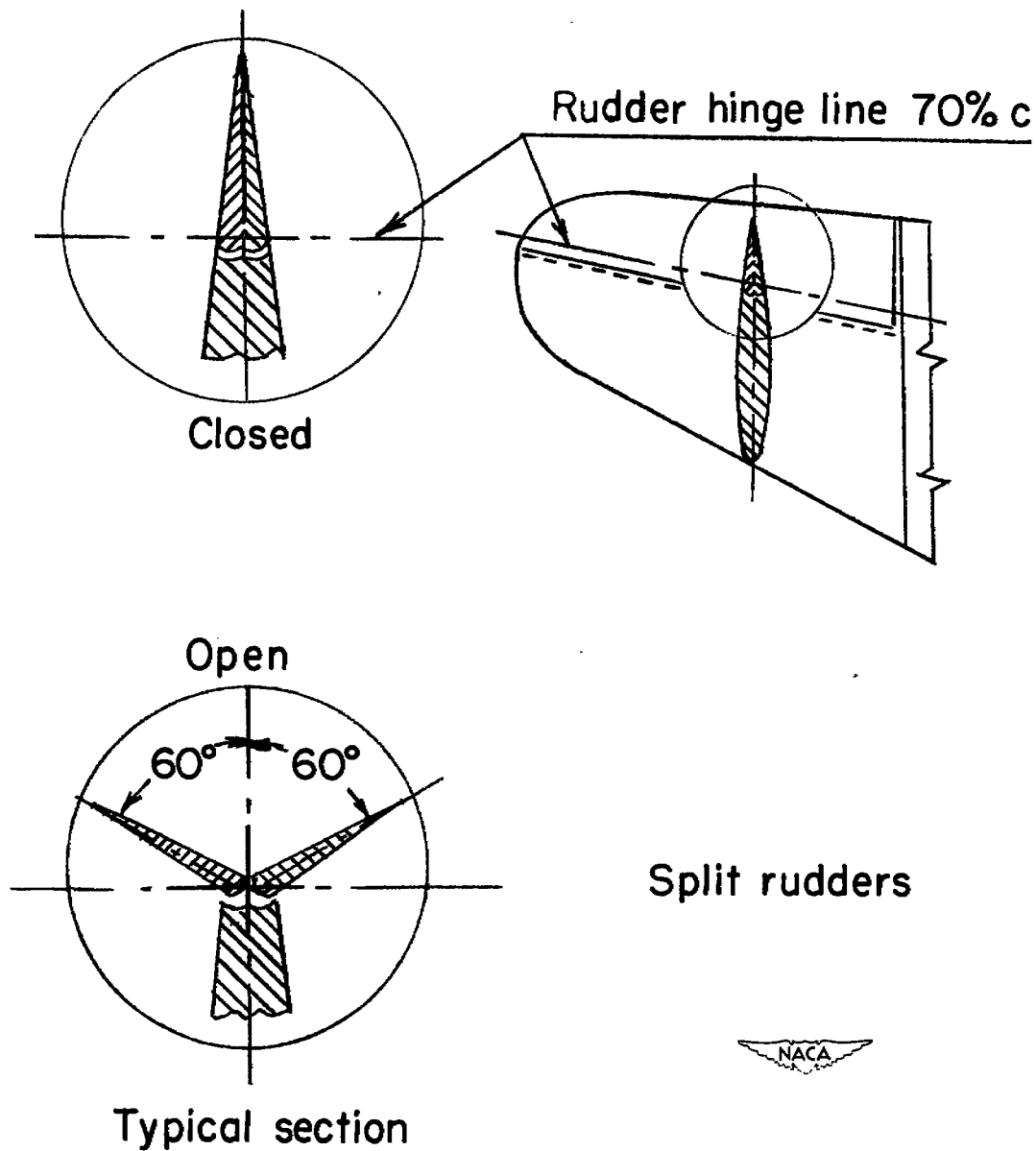
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(a) Model 1.

Figure 5.- Modifications tested on models.

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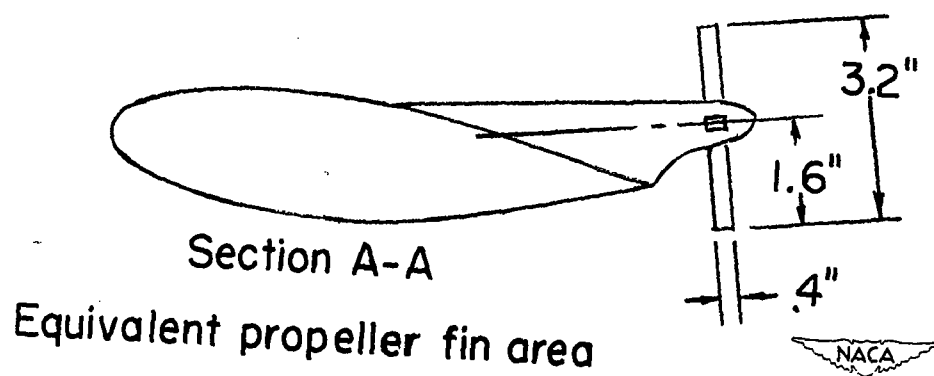
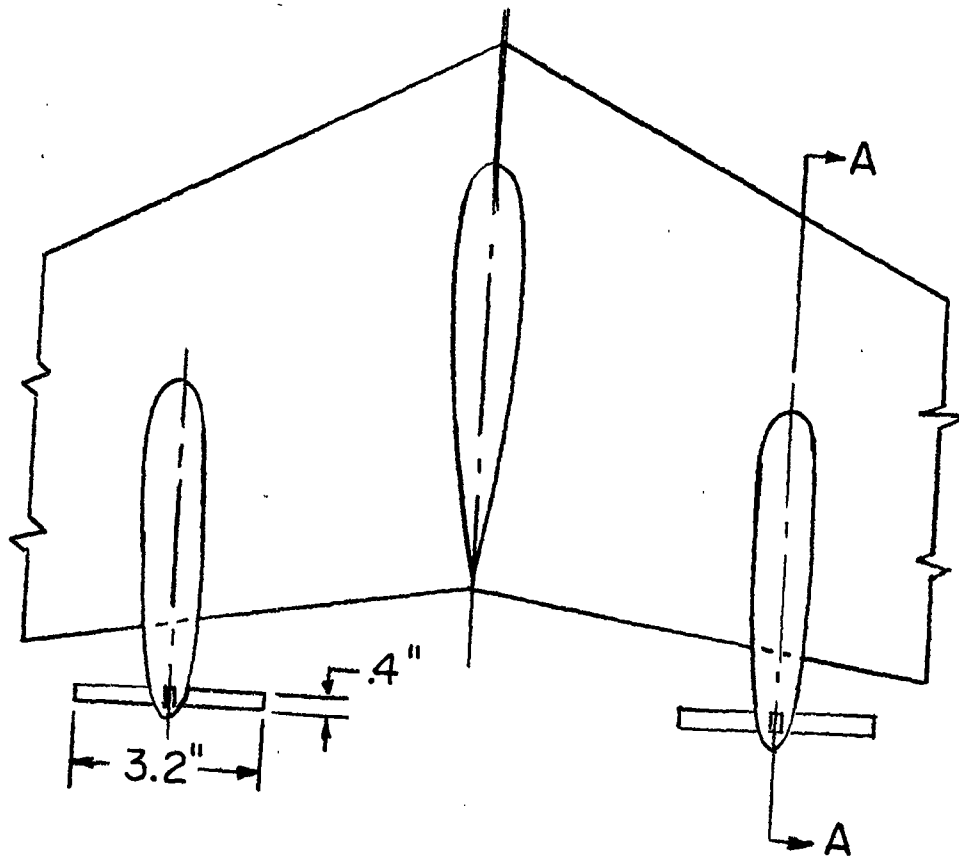
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(b) Model 2.

Figure 5.- Continued.

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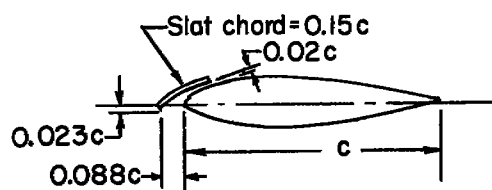
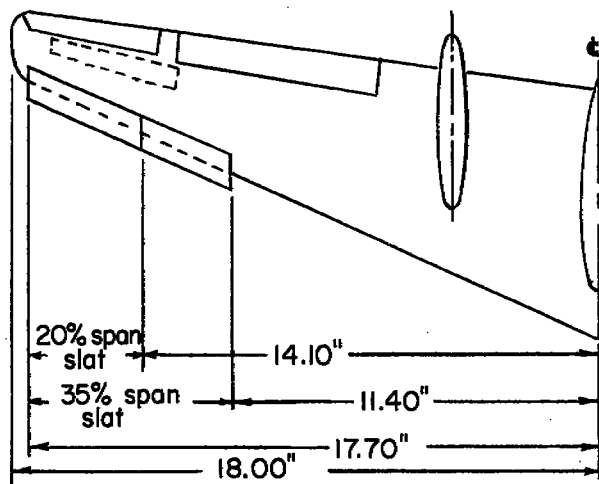
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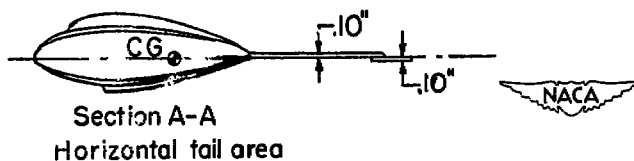
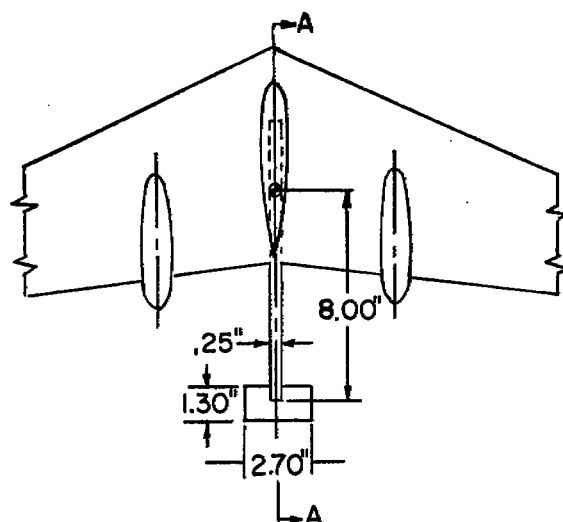
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20% and 35% semispan slats

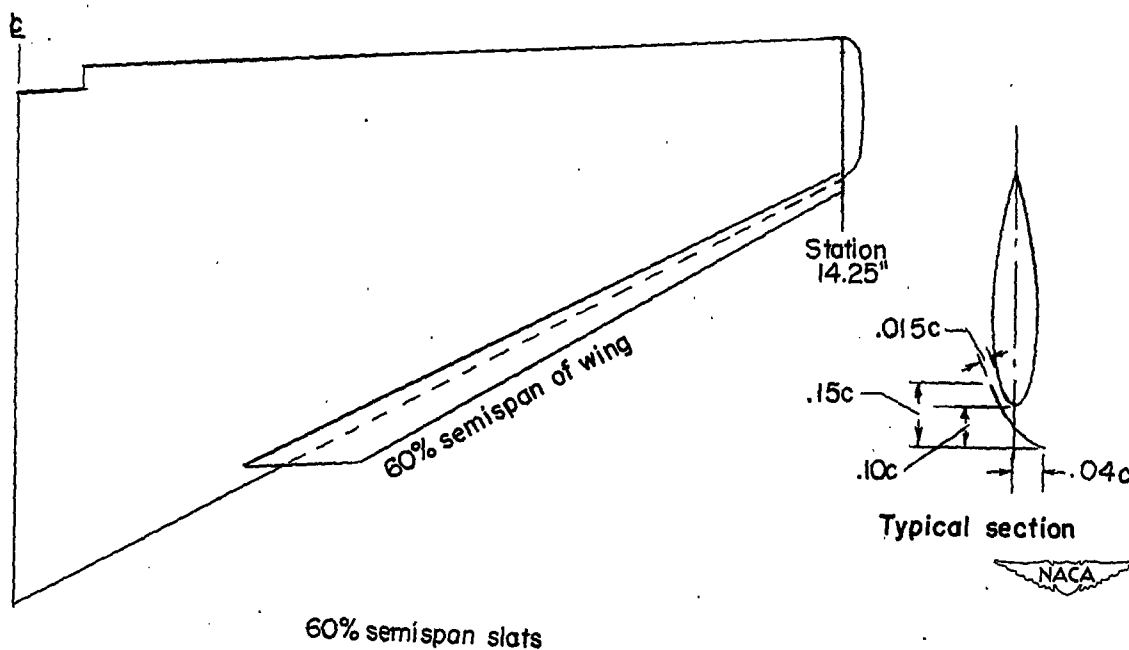
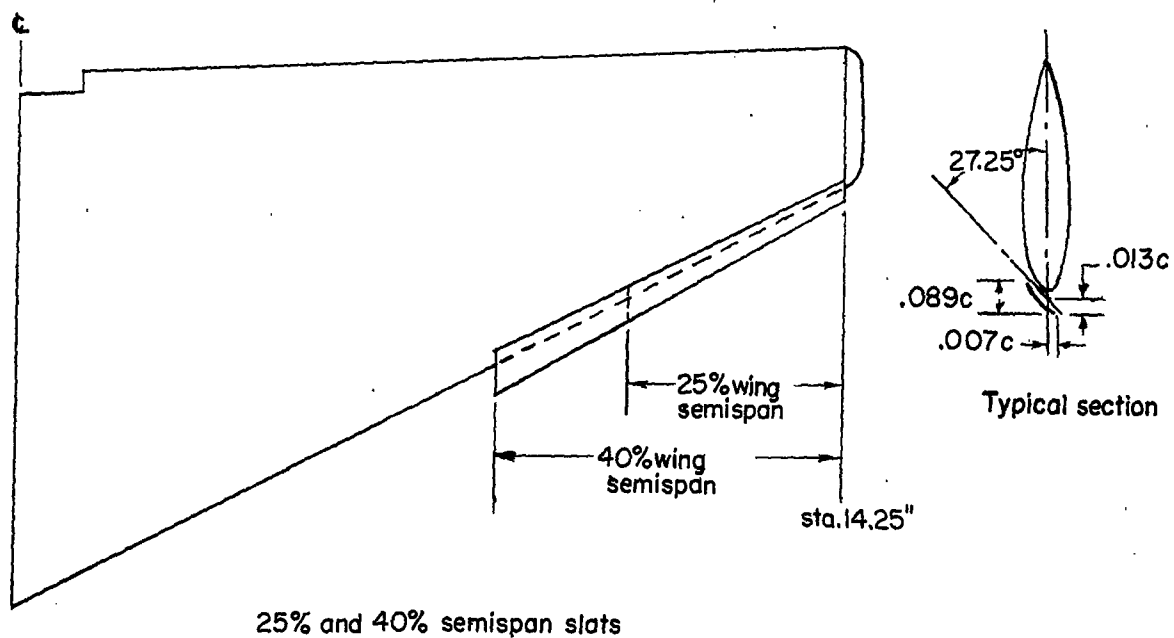


(b) Concluded.

Figure 5.- Continued.

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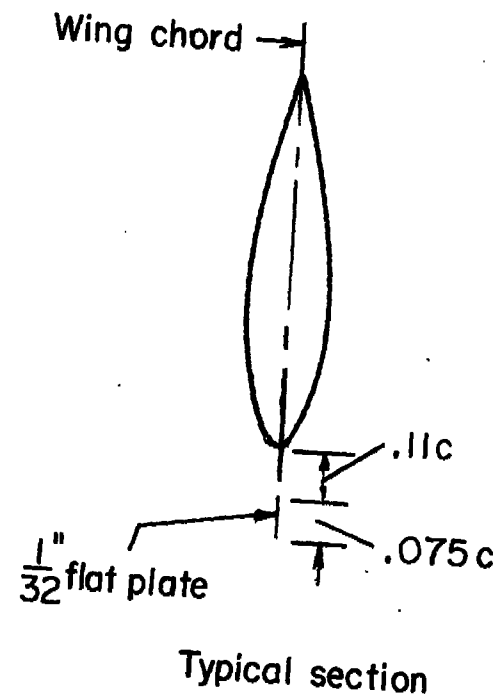
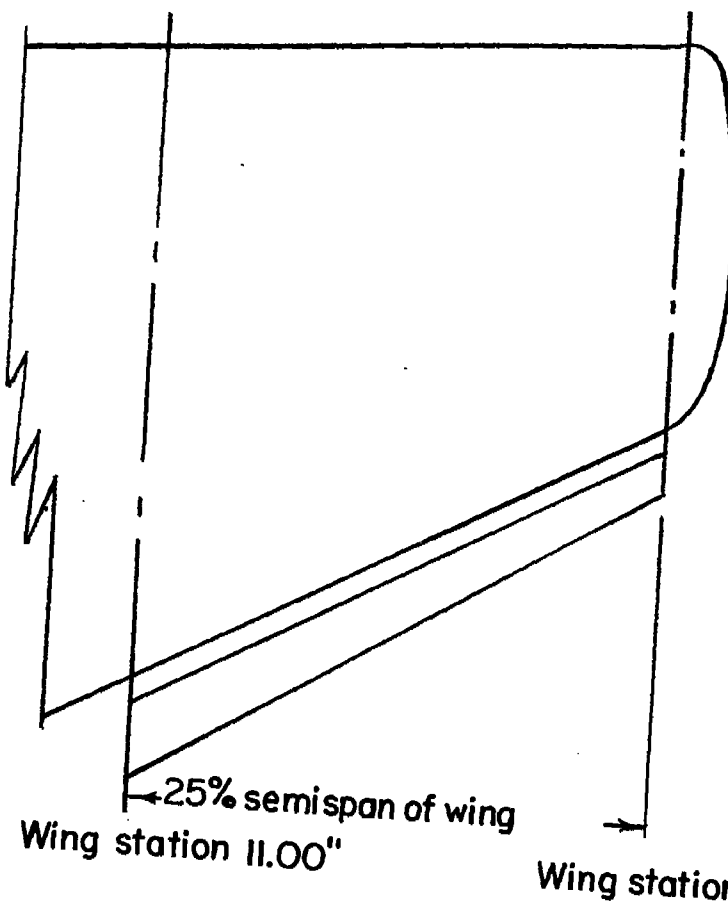
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(c) Model 4.

Figure 5.- Continued.

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25% semispan auxiliary airfoil slat

(c) Continued.

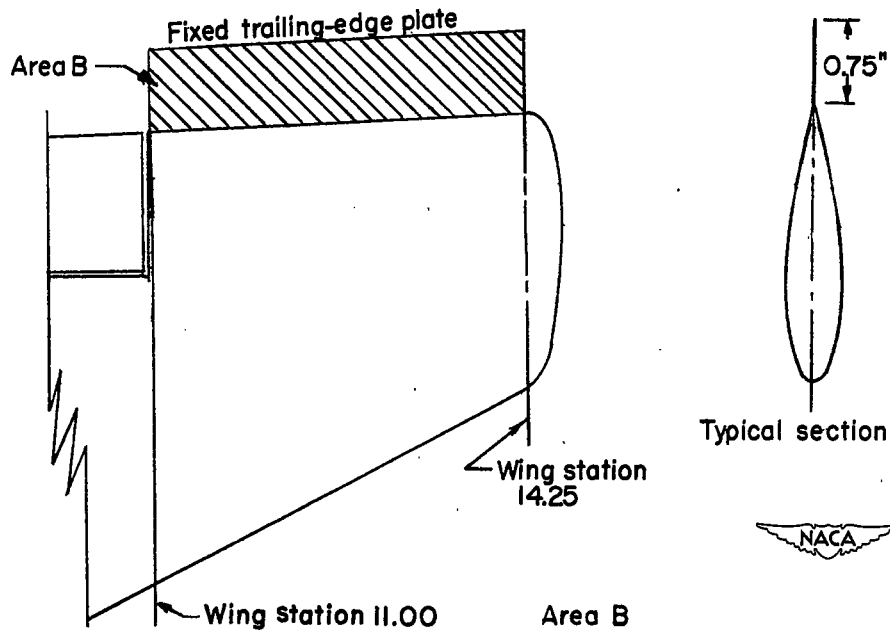
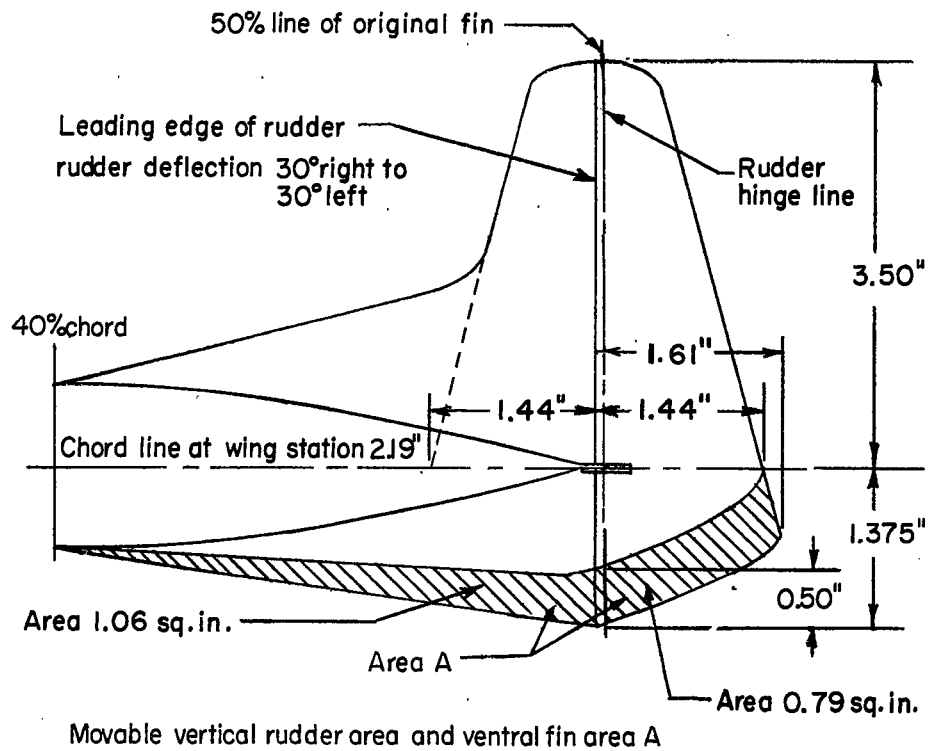
Figure 5.- Continued.

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(c) Continued.

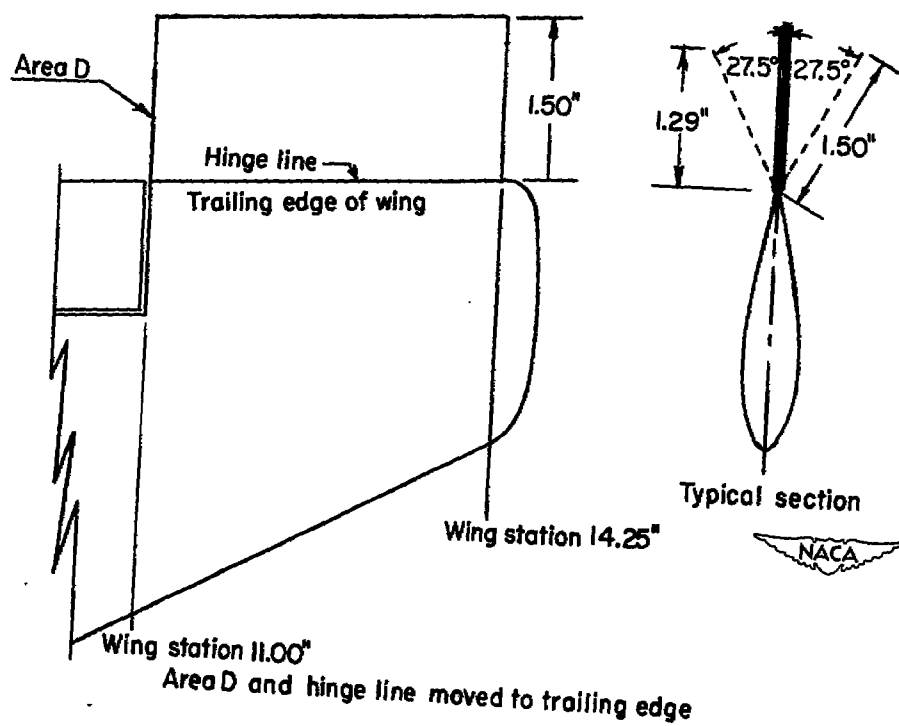
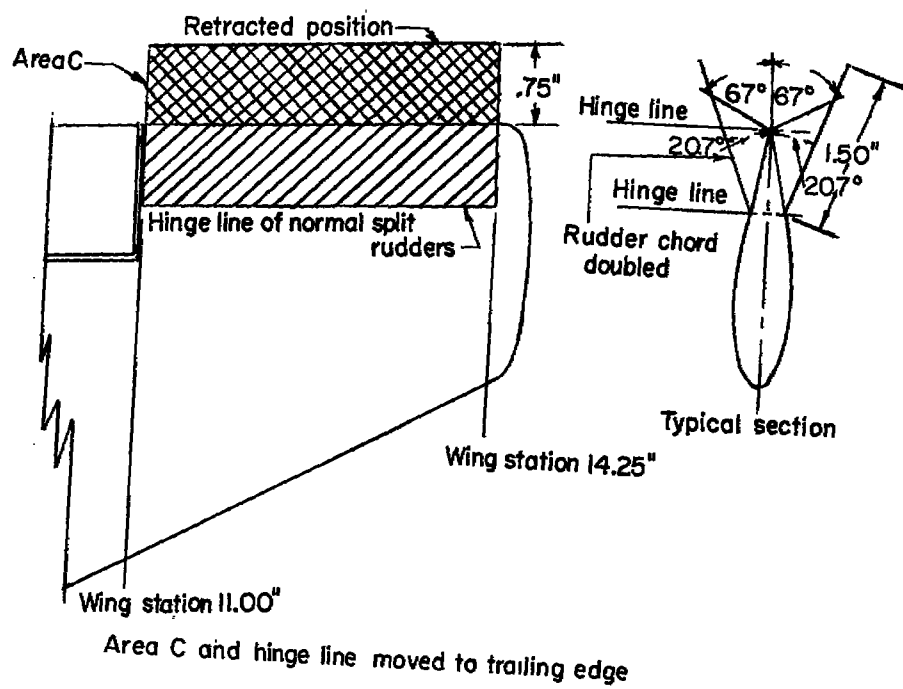
Figure 5.- Continued.

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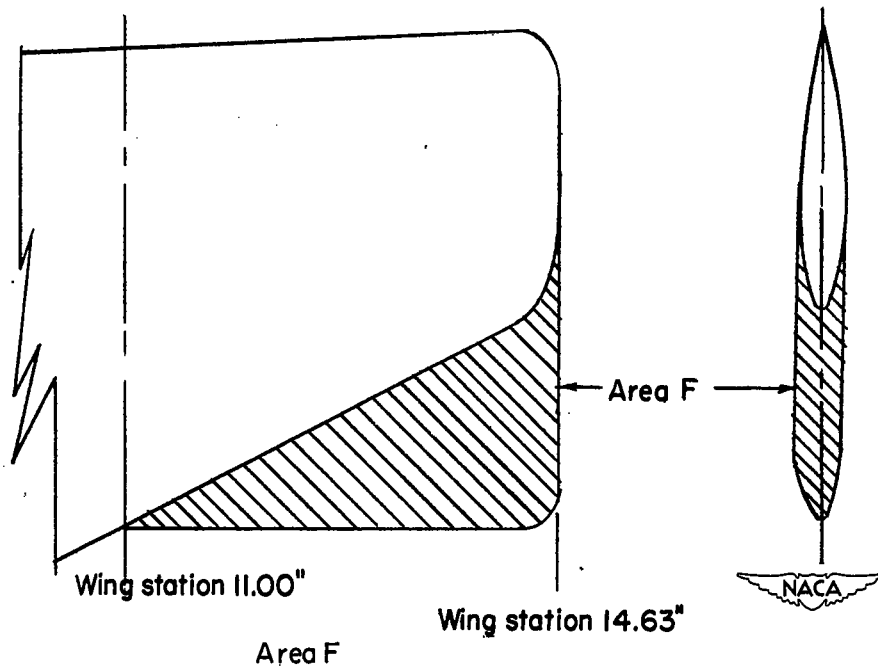
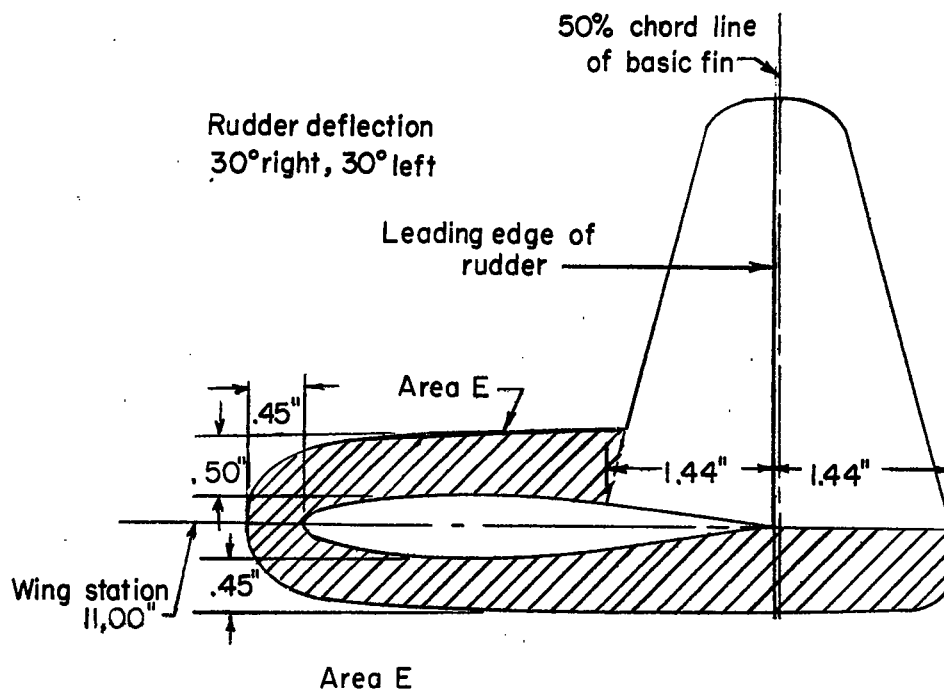


(c) Continued.

Figure 5.- Continued.

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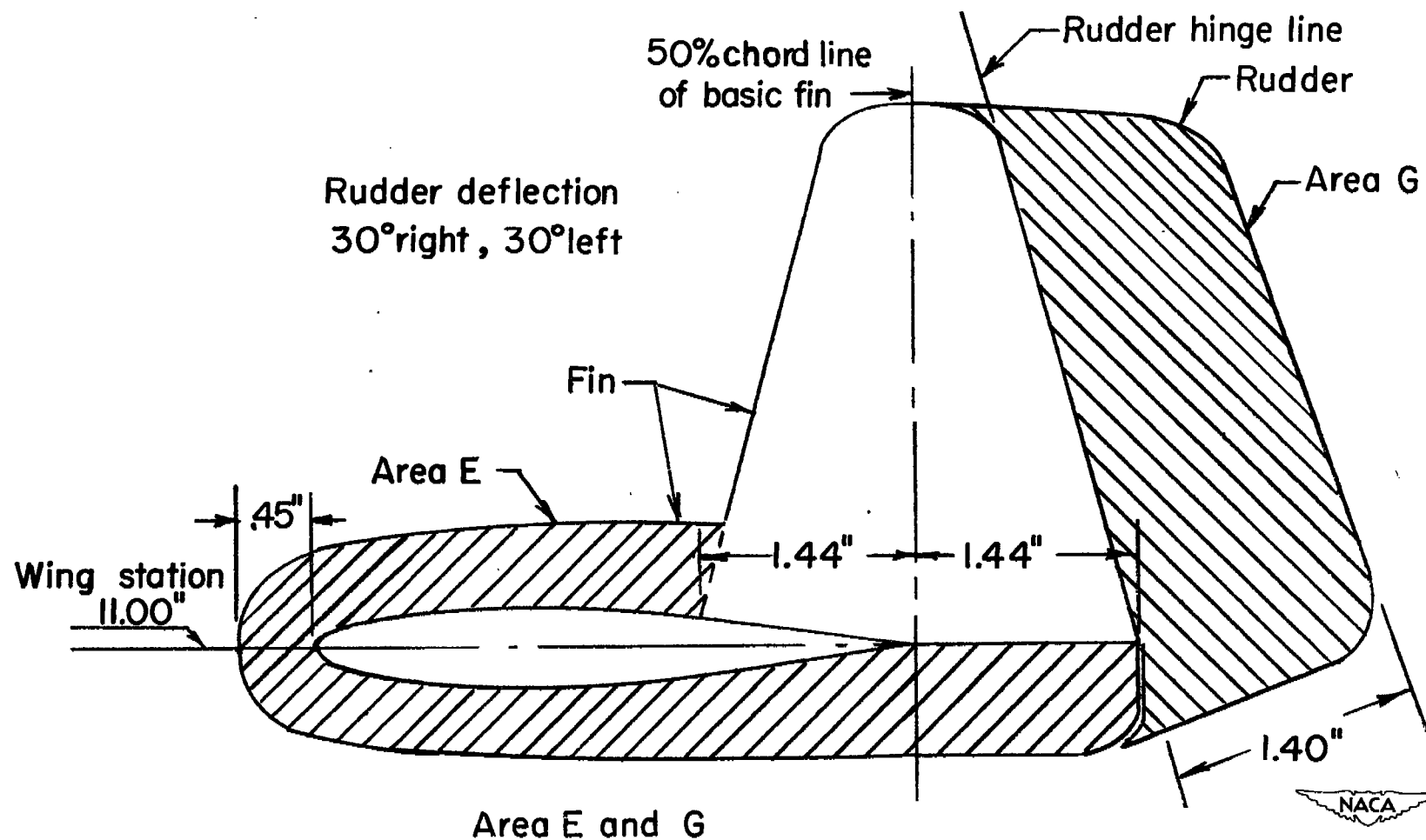
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(c) Continued.

Figure 5.- Continued.

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(c) Concluded.

Figure 5.- Continued.

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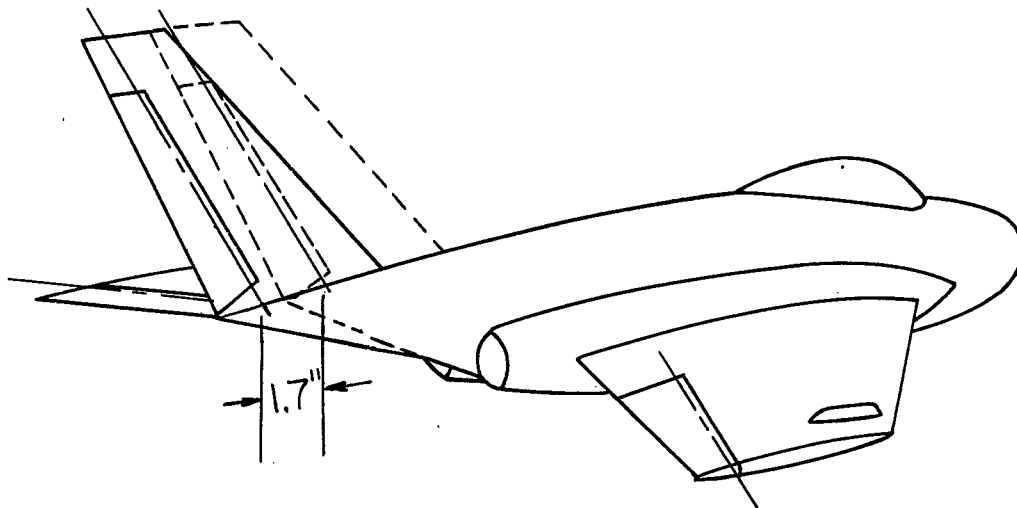
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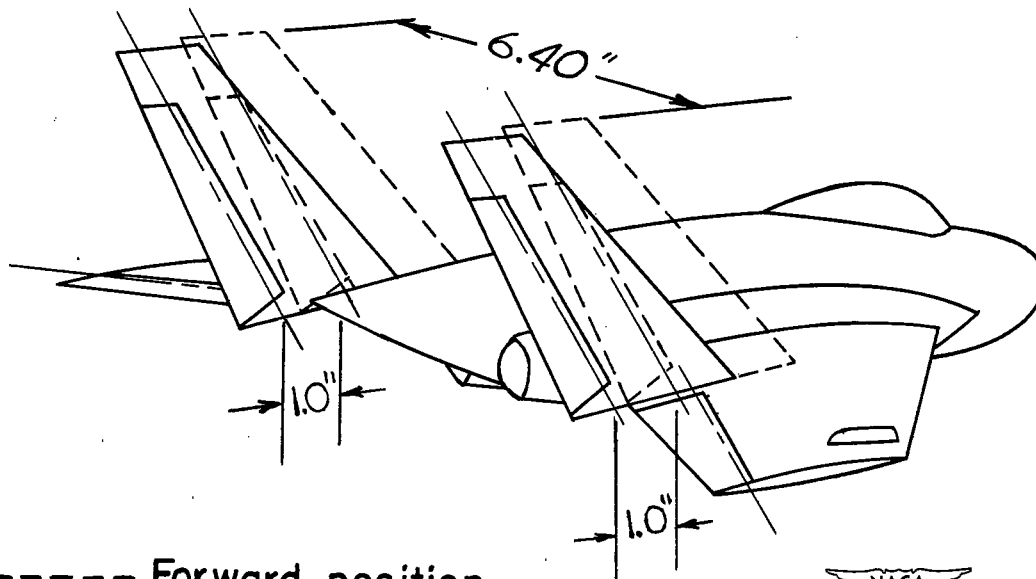
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----- Original position
——— Rearward position

Single vertical tail moved rearward



----- Forward position
——— Rearward position



Dual vertical tails in forward and rearward positions

(d) Model 6.

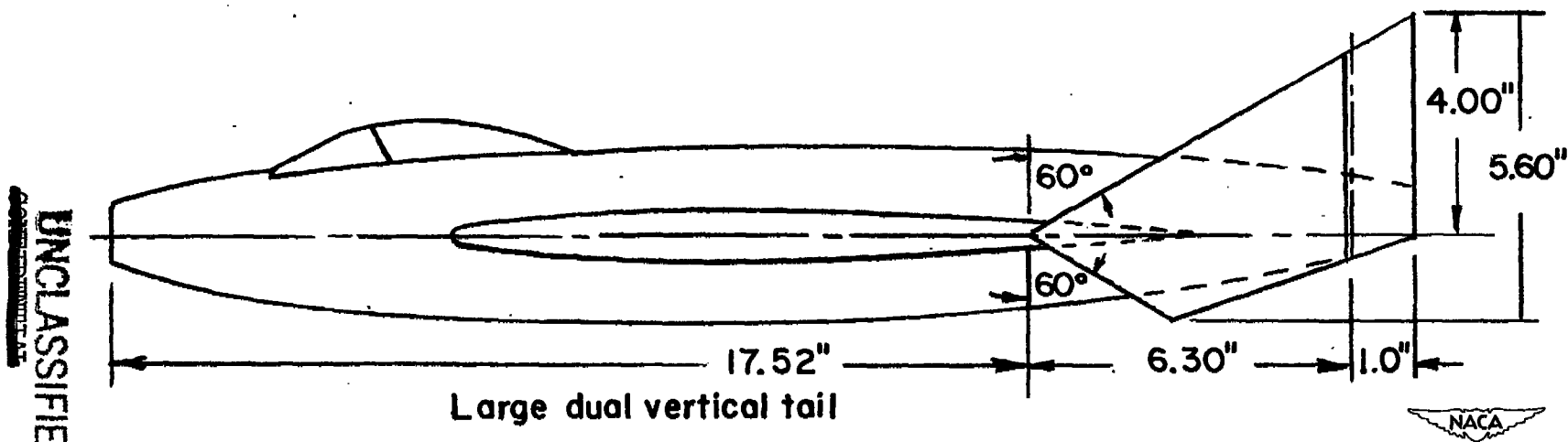
Figure 5.- Continued.

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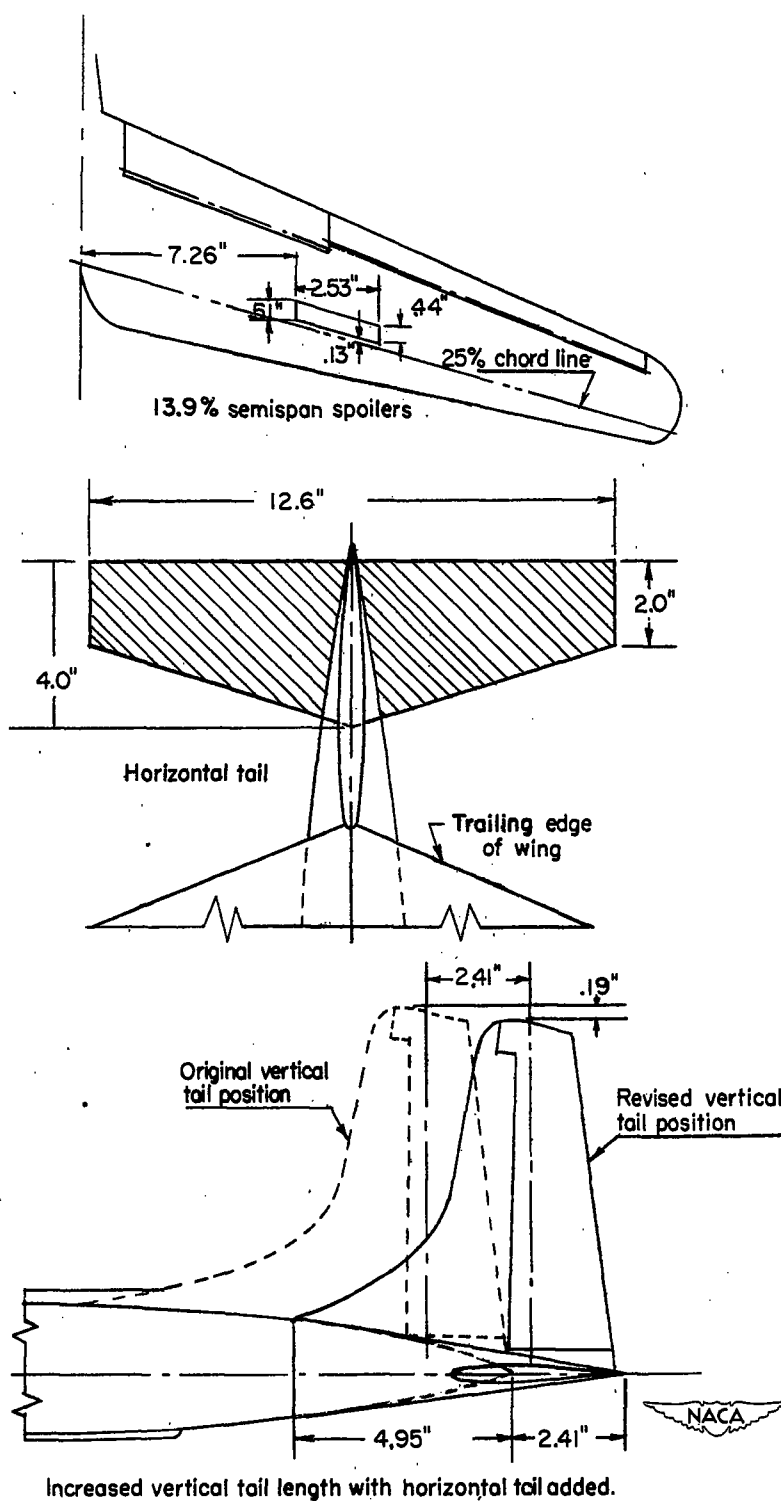
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(e) Model 7.

Figure 5.- Continued.

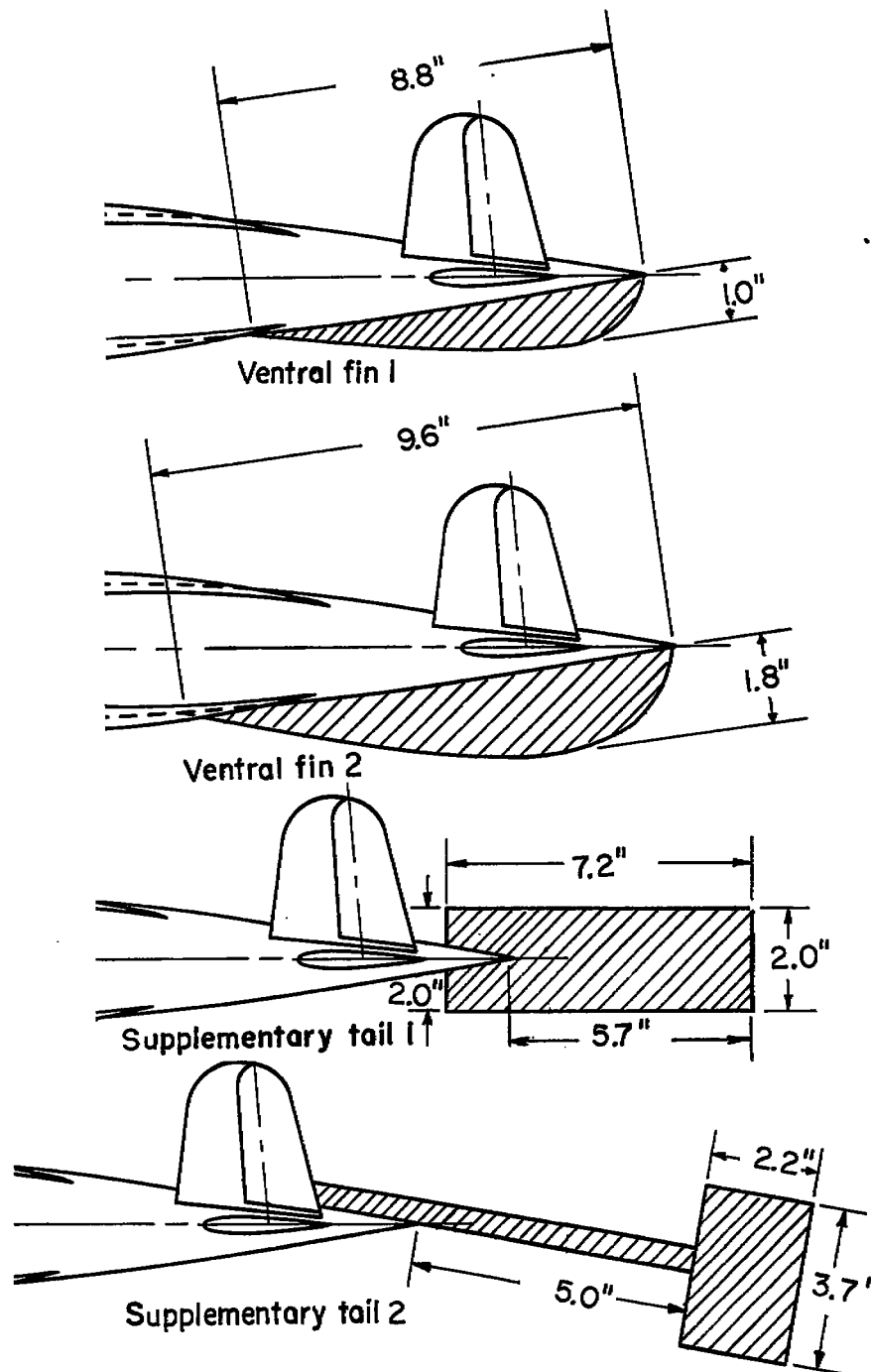
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(f) Model 8.

Figure 5.- Continued.

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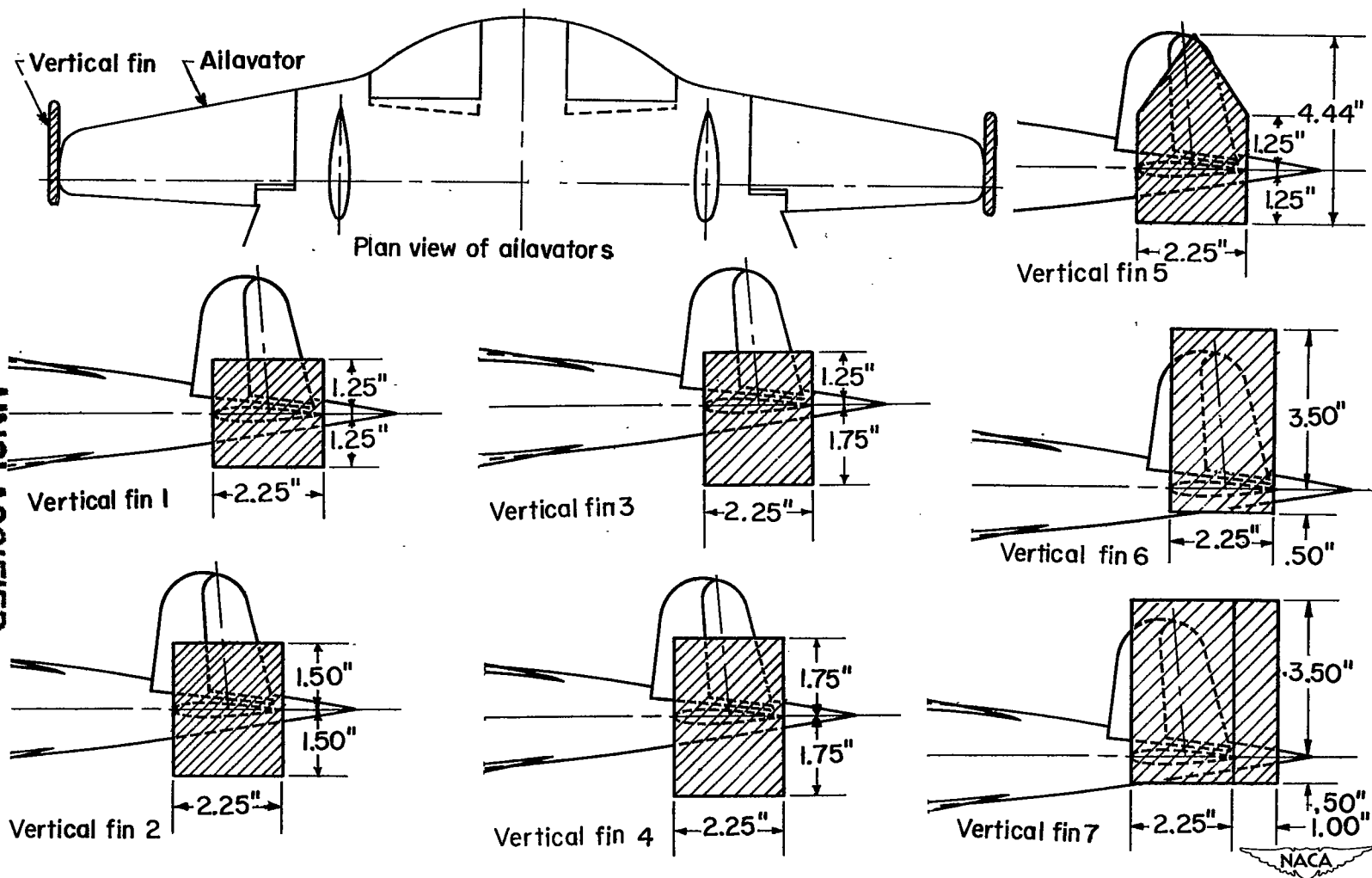
Ventral fins and supplementary tails added in plane of symmetry



(g) Model 10.

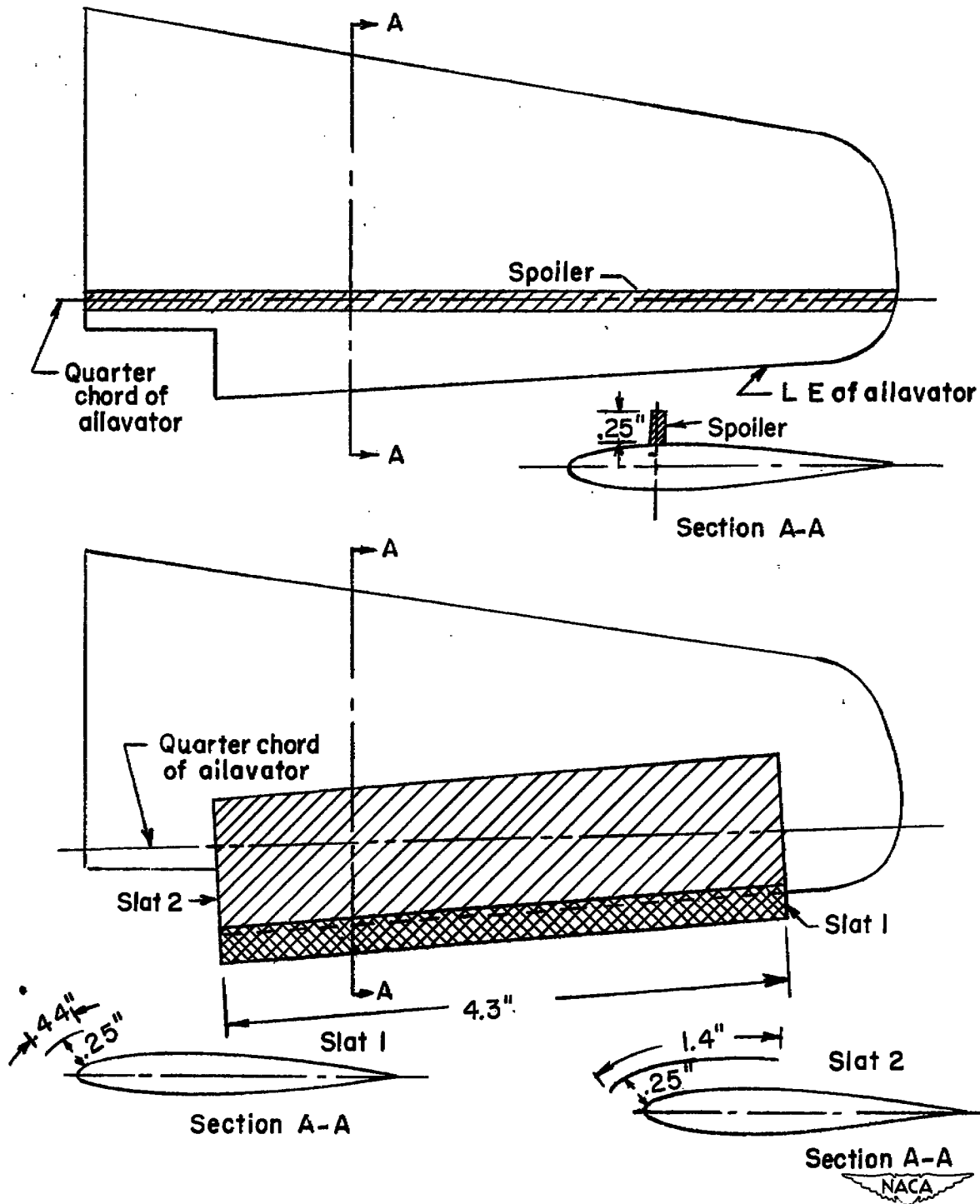
Figure 5.- Continued.

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(g) Continued.

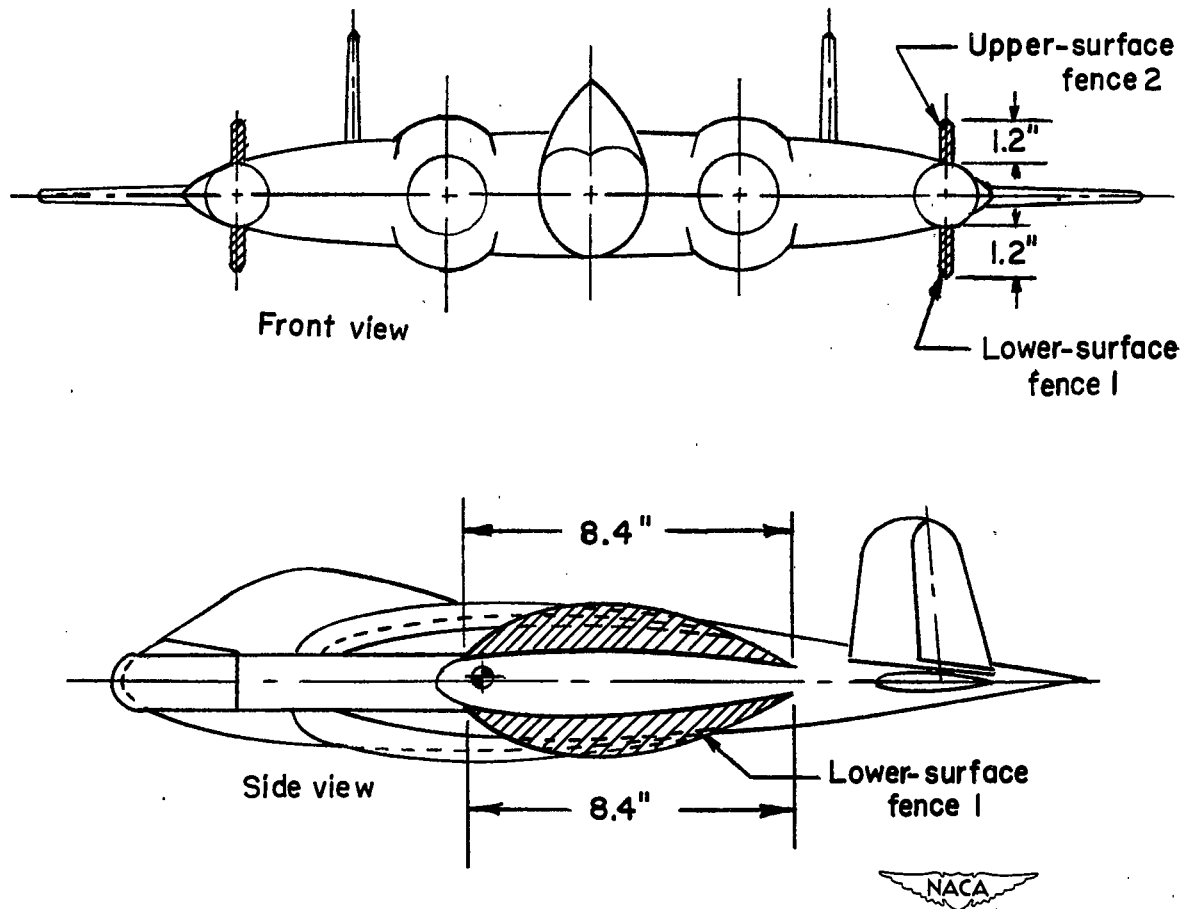
Figure 5.- Continued.



(g) Continued.

Figure 5.- Continued.

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(g) Continued.

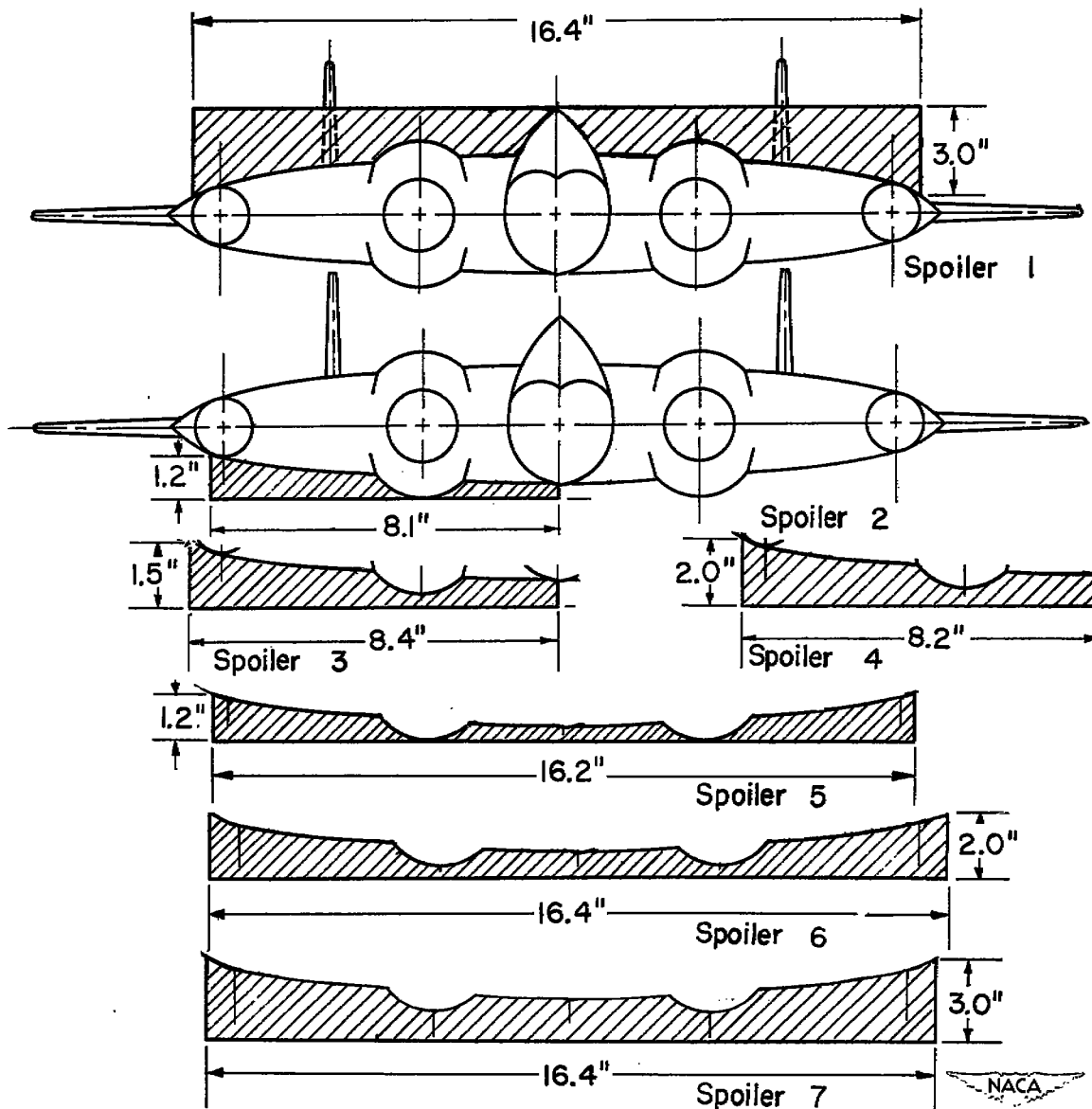
Figure 5.- Continued.

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Spoilers added at c/4 line

(g) Continued.

Figure 5.- Continued.

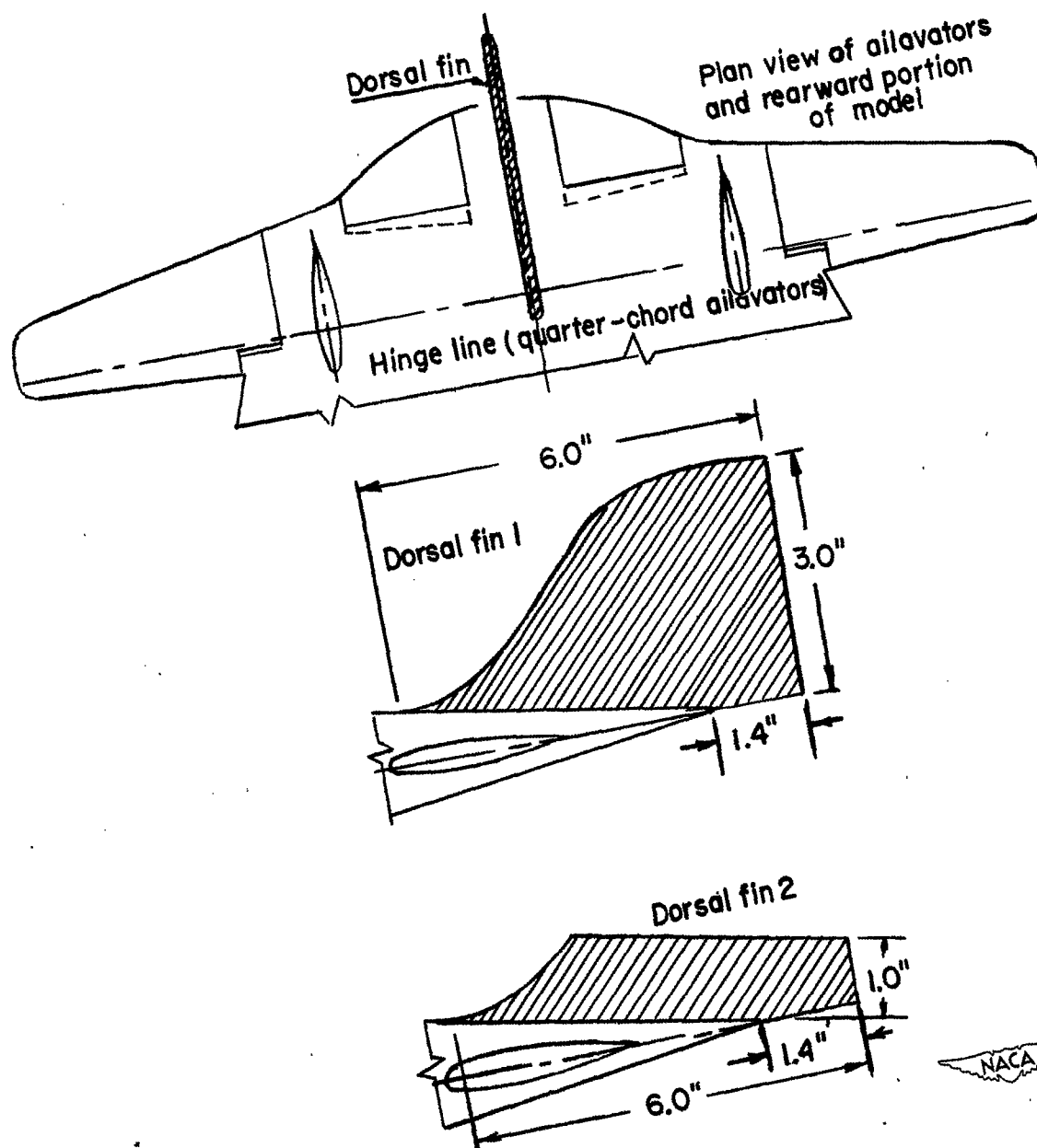
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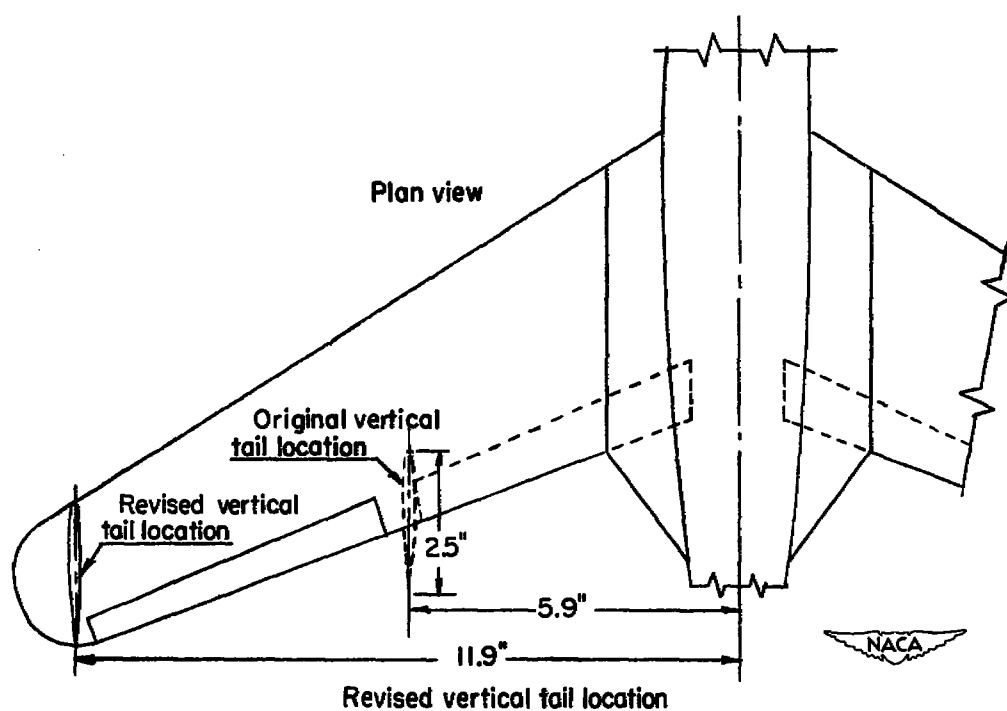
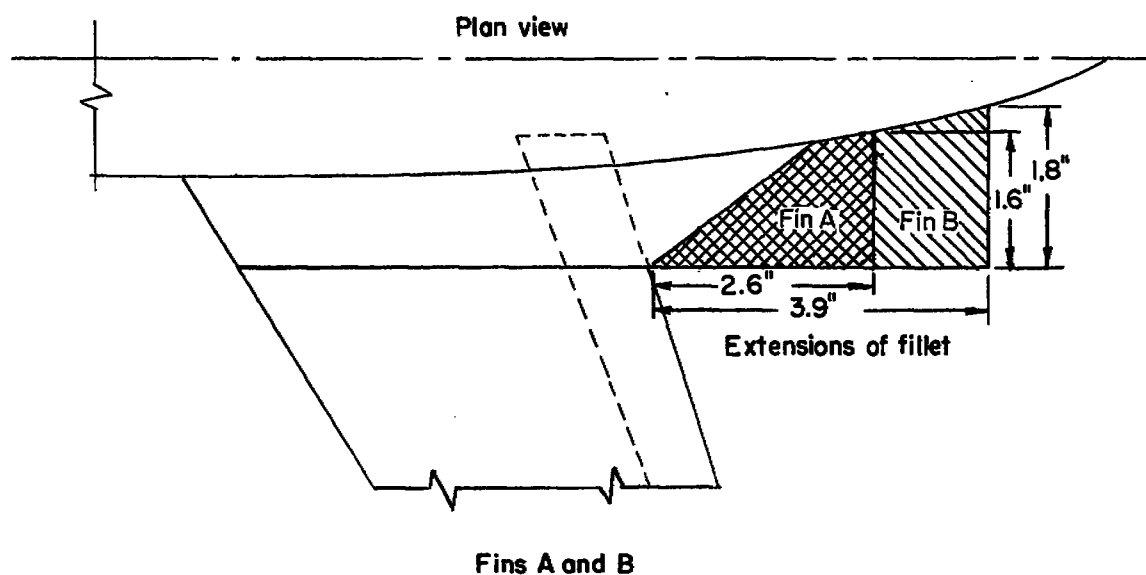


(g) Concluded.
Figure 5.- Continued.

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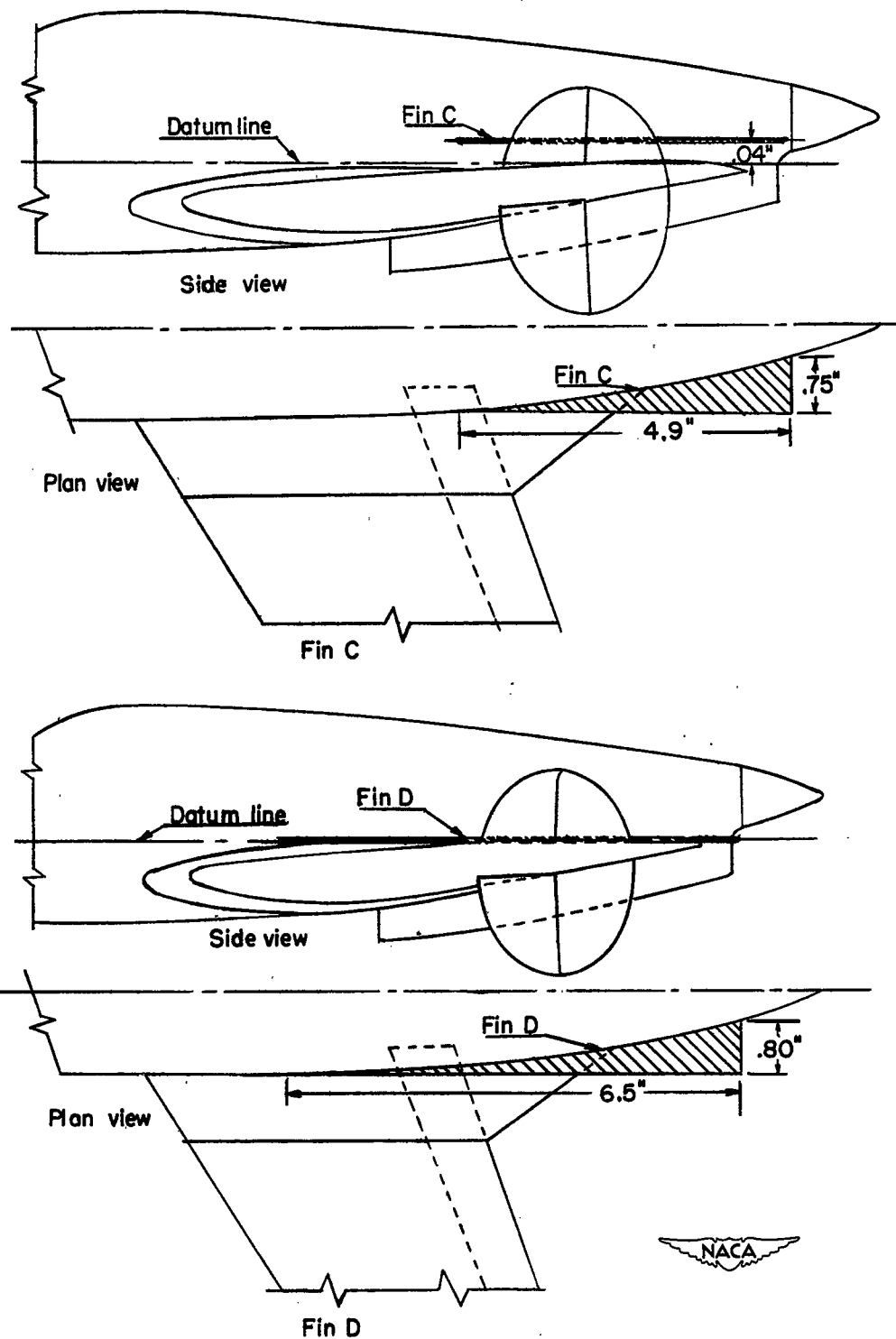


(h) Model 11.

Figure 5.- Continued.

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(h) Continued.

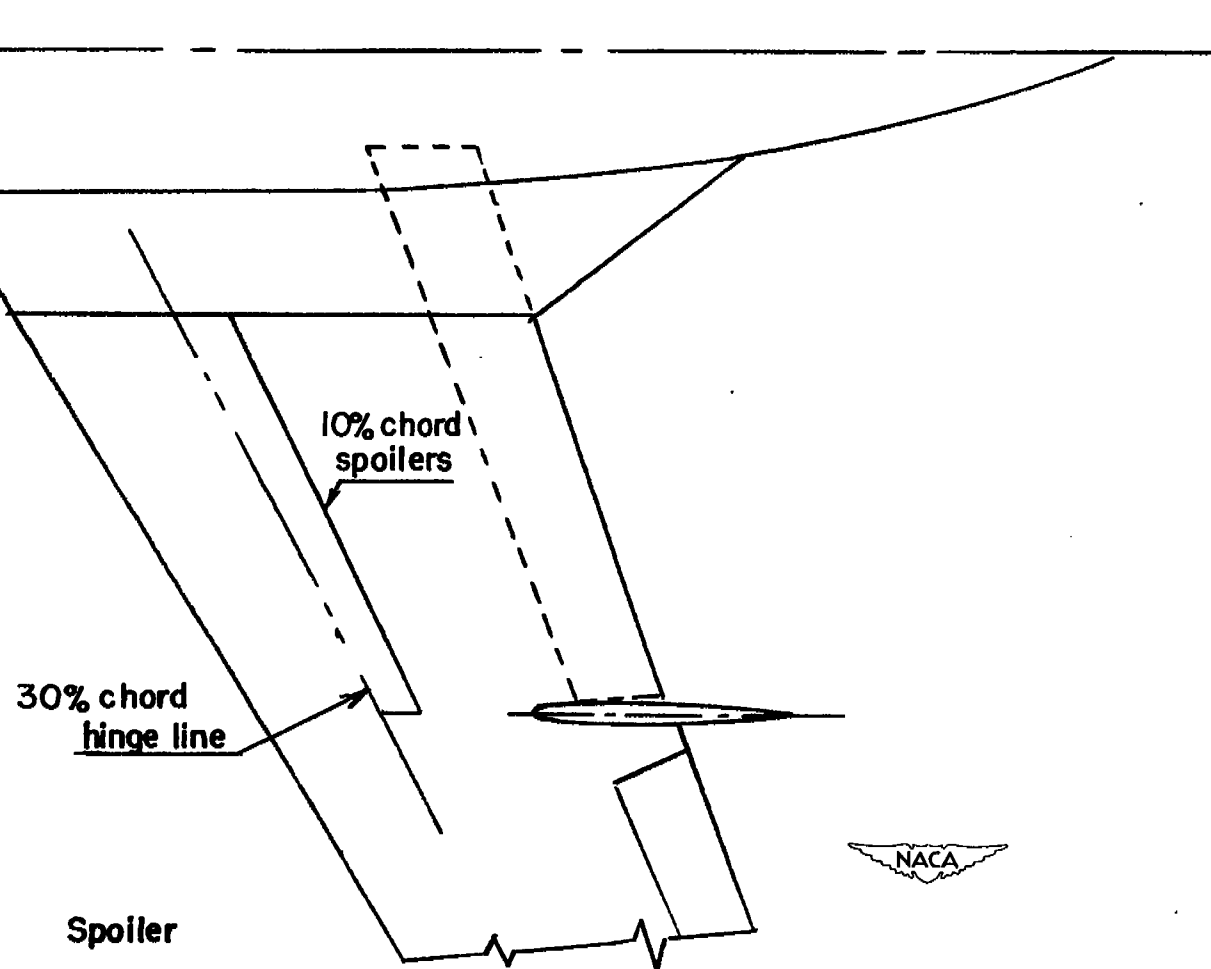
Figure 5.- Continued.

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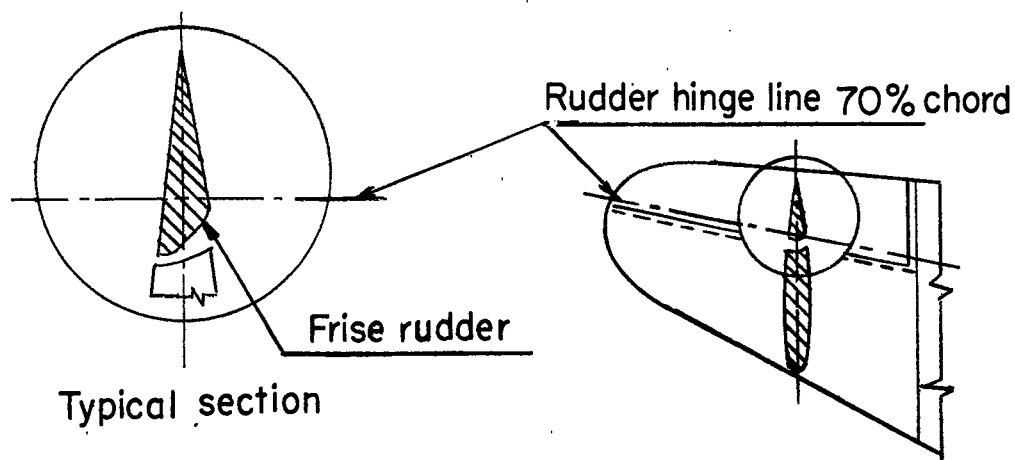
(h) Concluded.

Figure 5.- Concluded.

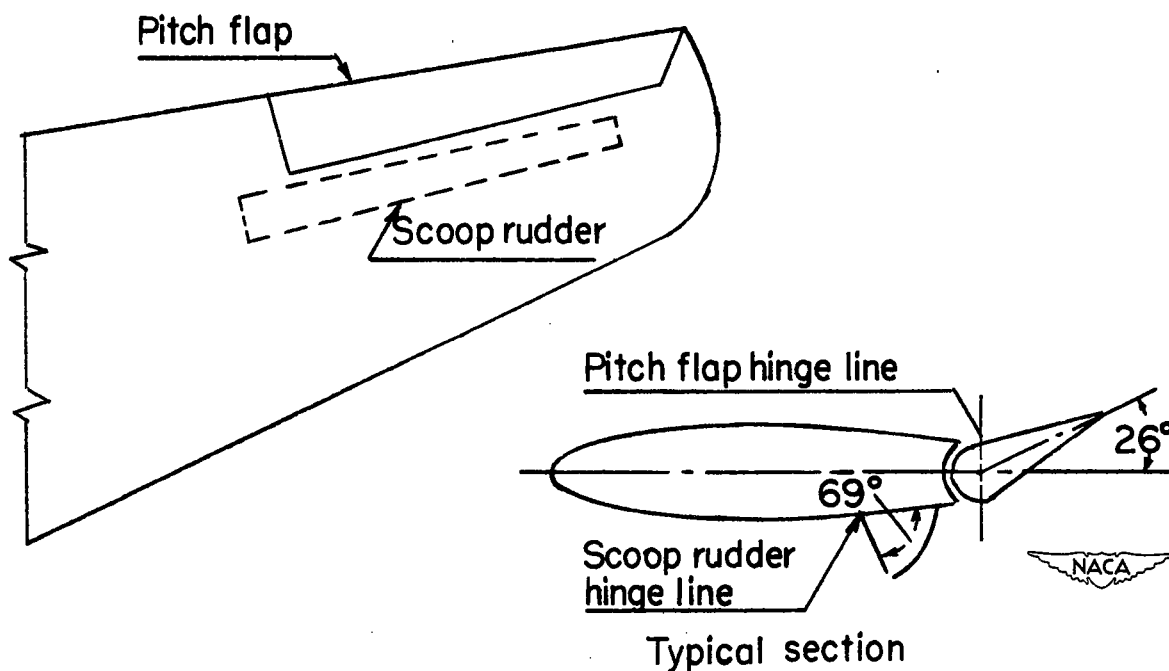
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(a) Rudder detail for model 1.

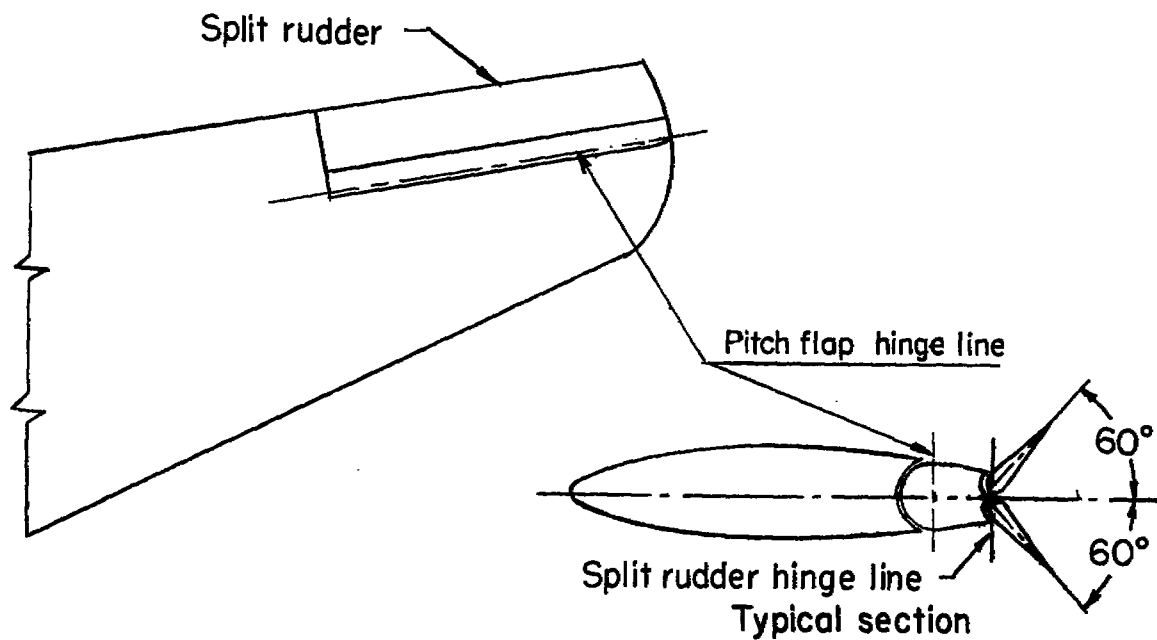


(b) Rudder detail for model 2.

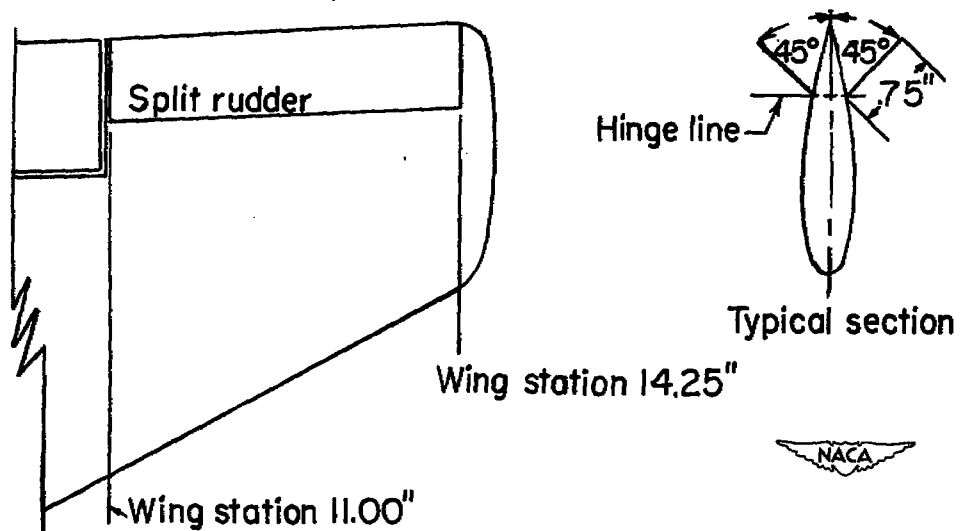
Figure 6.- Details of drag-type rudders used on models 1 to 4.

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(c) Rudder details for model 3.



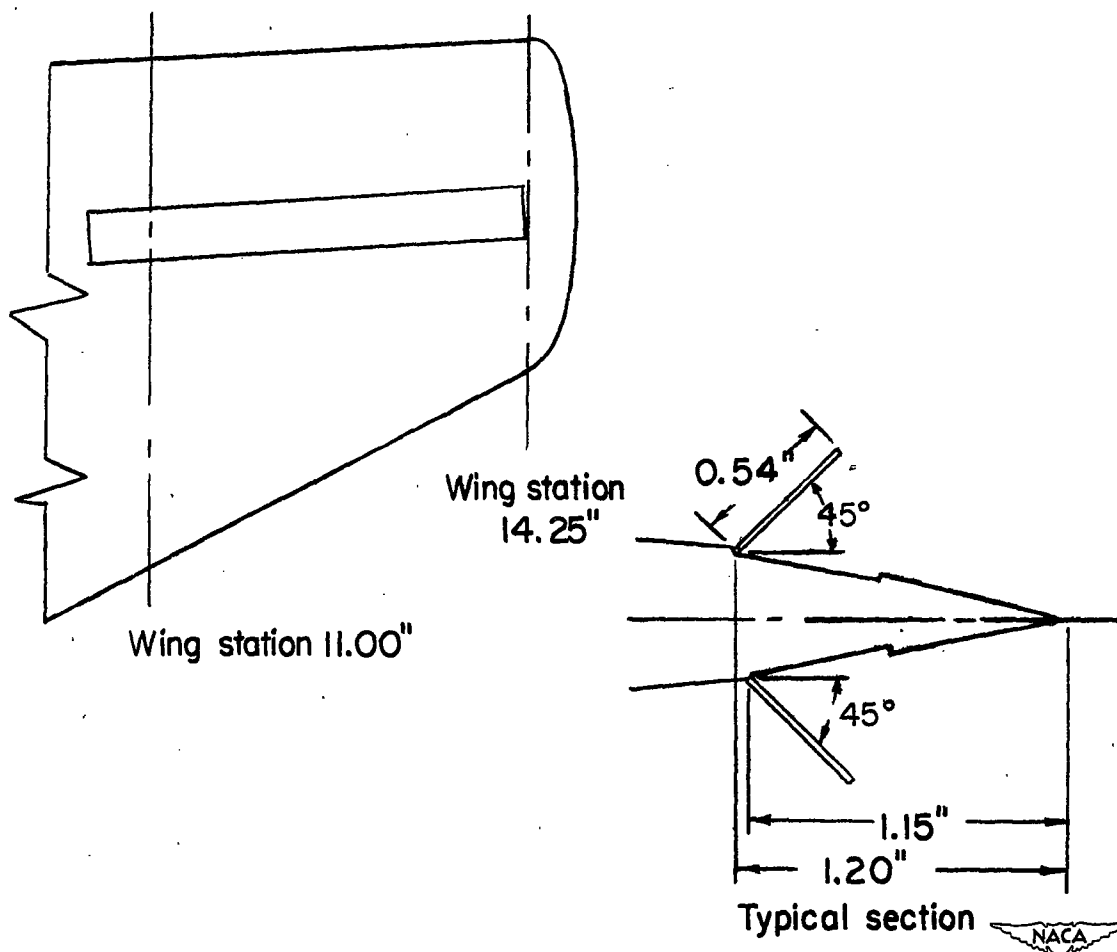
(d) Rudder details for model 4; split-type rudders.

Figure 6.- Continued.

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(e) Rudder detail for model 4; alternate circular-arc type rudder.

Figure 6.- Concluded.

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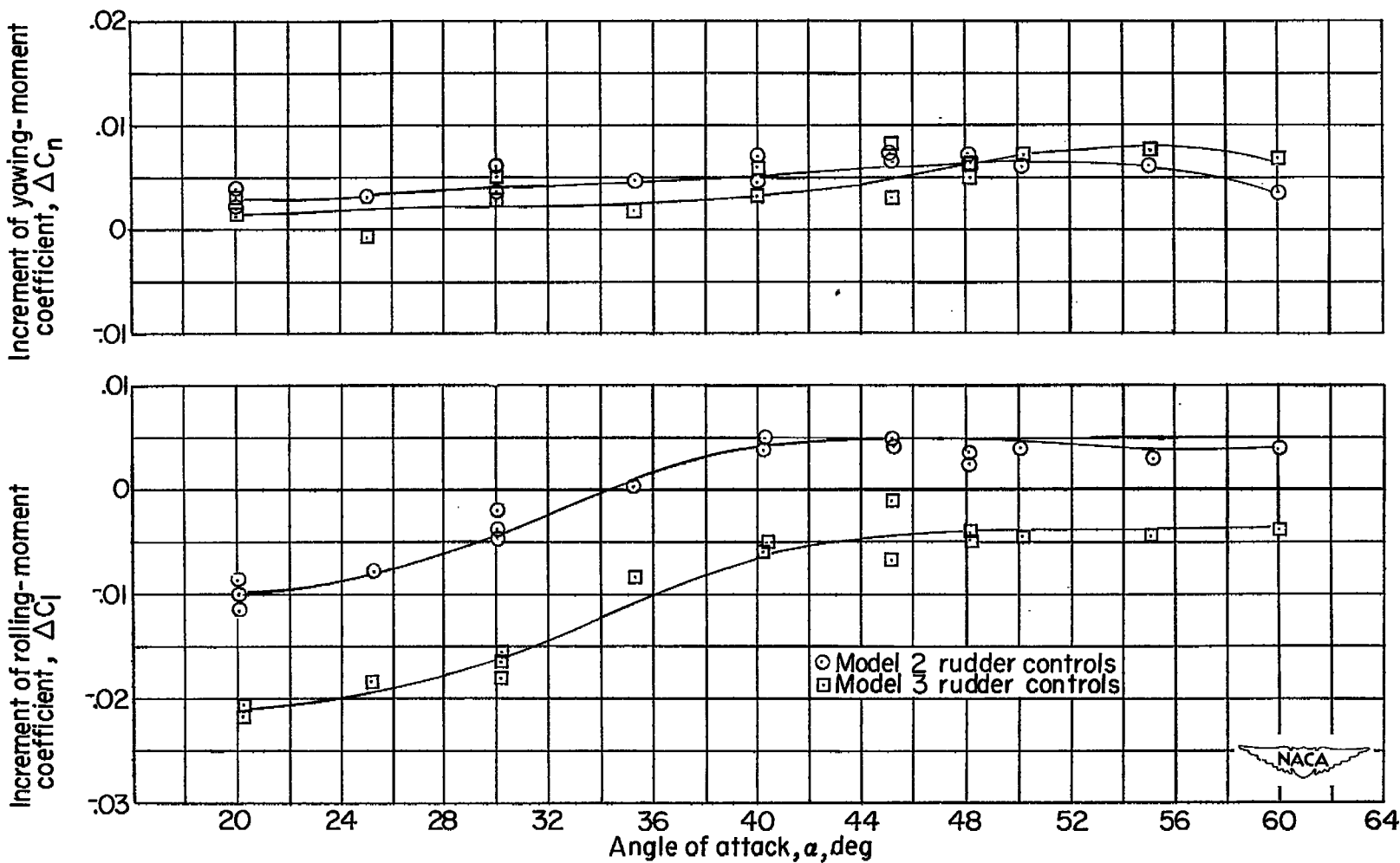


Figure 7.- Increments of yawing- and rolling-moment coefficients contributed by models 2 and 3 rudder controls as a function of angle of attack. Rudder controls on right wing tip fully deflected; rudder controls on left wing tip neutral; $q = 4.274$.

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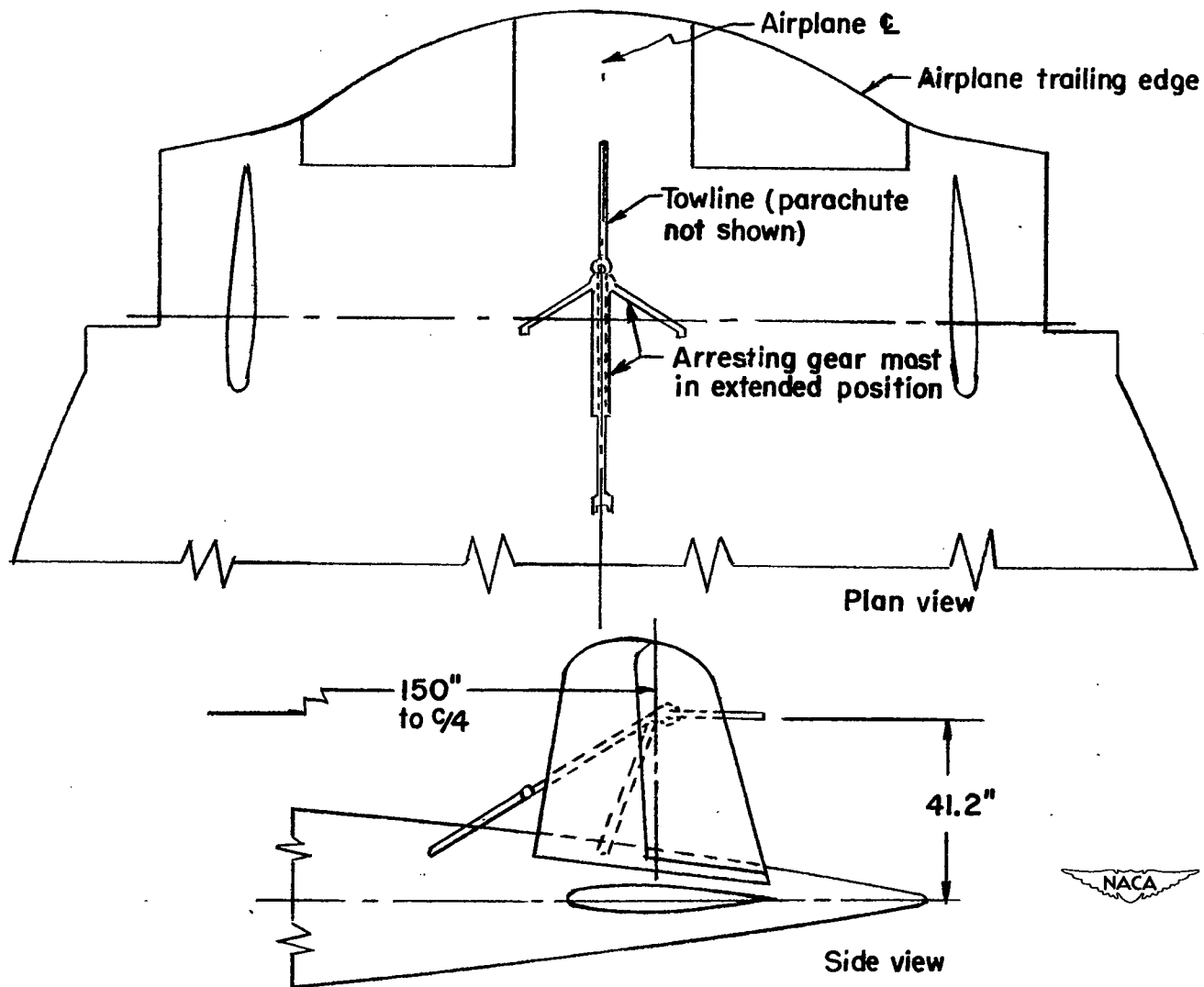


Figure 8.- Arresting gear mast for tail parachute attachment of model 10.

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